

#### HAND DELIVERED TO PADEP SOUTHEAST REGIONAL OFFICE

September 14, 2015

Mr. James Rebarchak
Program Manager – Bureau of Air Quality
Pennsylvania Department of Environmental Protection
Southeast Regional Office
2 East Main Street
Norristown, PA 19401

Subject: Plan Approval Application for Ultra Low Sulfur Gasoline Project

Monroe Energy, LLC, Delaware County, Trainer Borough

Title V Operating Permit No. 23-00003

#### Dear Mr. Rebarchak:

Monroe Energy, LLC (Monroe Energy or Monroe) is pleased to provide the Pennsylvania Department of Environmental Protection (PADEP) with the enclosed three (3) copies of a Plan Approval Application (application) for its petroleum refinery located in Trainer, Delaware County, Pennsylvania (Trainer Refinery or Refinery). This application is being submitted to obtain authorization to make modifications at the Refinery needed to meet gasoline sulfur level requirements of U.S. EPA's Tier 3 Motor Vehicle Emission and Fuel Standards rule which was published at 79 Federal Register (Fed. Reg.) 23414 (April 28, 2014), and amended at 80 Fed. Reg. 9078 (February 19, 2015).

This application is being submitted to fulfill the Pennsylvania air quality permitting requirements for nonexempt stationary sources and provides the necessary information for PADEP review and approval of the proposed project based on Monroe's understanding and interpretation of the rules. All4 Inc. assisted Monroe with preparation of this application.

The application is organized as follows:

- <u>Attachment A</u> Application Narrative, including the following:
  - Project Description Provides a description of the proposed project and a facility location map.
  - o *Emissions Inventory* Provides potential air pollutant emissions estimates for the proposed project.
  - Regulatory Applicability Analysis Summarizes potentially applicable Federal and Commonwealth of Pennsylvania air quality requirements applicable to the proposed project.
- Attachment B PADEP Application Forms, including the following:



Monroe Energy, LLC – Trainer Refinery Ultra Low Sulfur Gasoline Project Plan Approval Application September 11, 2015

- o General Information Form (GIF).
- Application for Plan Approval to Construct, Modify, or Reactivate an Air Contamination Source and/or Install an Air Cleaning Device Application Form (Process and Combustion Forms).
- o Addendum A and Addendum 1.
- o Compliance Review Form (CRF).
- Attachment C Emissions Inventory Tables.
- Attachment D Municipal Notification Letters,
- Attachment E All4 Inc. Quality Seal.

As requested by PADEP, Monroe Energy is also providing one (1) electronic copy of this application to the U.S. Environmental Protection Agency (U.S. EPA) Region 3 Office of Permits and State Programs, via email, to Ms. Gerallyn Duke.

Monroe Energy appreciates PADEP's consideration of these matters. Should you have any questions or require additional information, please contact me at (610) 364-8528, or Mr. Matt Torell, Environmental Leader, at (610) 364-8399.

Sincerely,

MONROE ENERGY, LLC

David Chetkowski, P.E.

Air Program Lead

cc: Gerallyn Duke – U.S. EPA Region 3 (duke.gerallyn@epa.gov)

Neal Lebo - All4 Inc.





#### PROJECT DESCRIPTION

A brief description of the existing operations at the Trainer Refinery and a description of the proposed Ultra Low Sulfur Gasoline Project (ULSG project or project) are provided below.

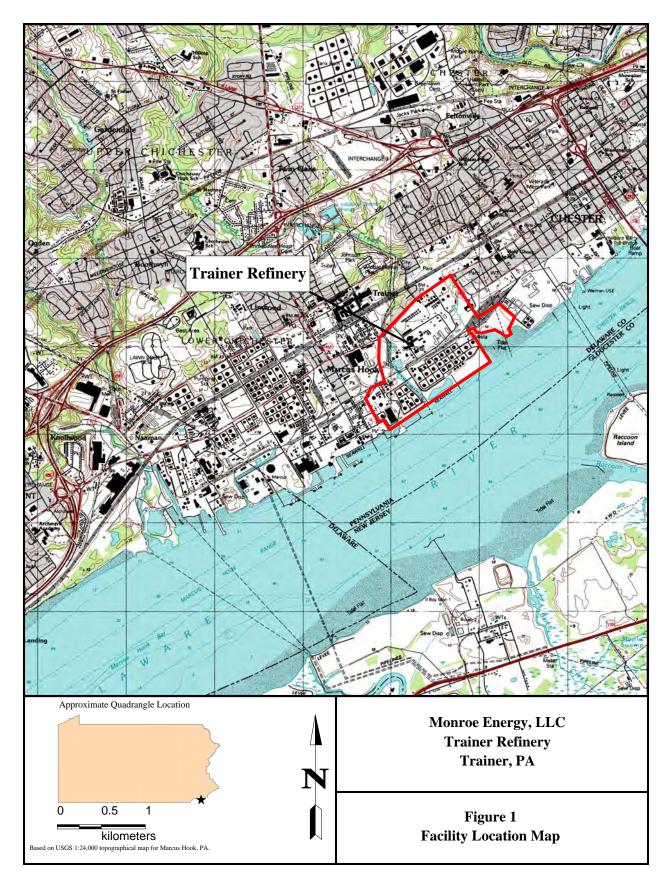
#### **EXISTING FACILITY DESCRIPTION**

Monroe Energy owns and operates a petroleum refinery located on the Delaware River in Trainer, PA, about 10 miles southwest of the Philadelphia International Airport. The Refinery processes mainly light, sweet (low-sulfur) crude oils and primarily produces jet fuel and other transportation fuels, such as gasoline and diesel fuel. Other products include, but are not limited to, sulfur, home heating oil, residual fuel oil, and liquefied petroleum gas (e.g., propane, butane). The Refinery also buys, sells, and trades intermediate streams that can be used as feedstocks or fuel blending components. The Trainer Refinery currently operates under PADEP Title V Operating Permit (TVOP) No. 23-00003.

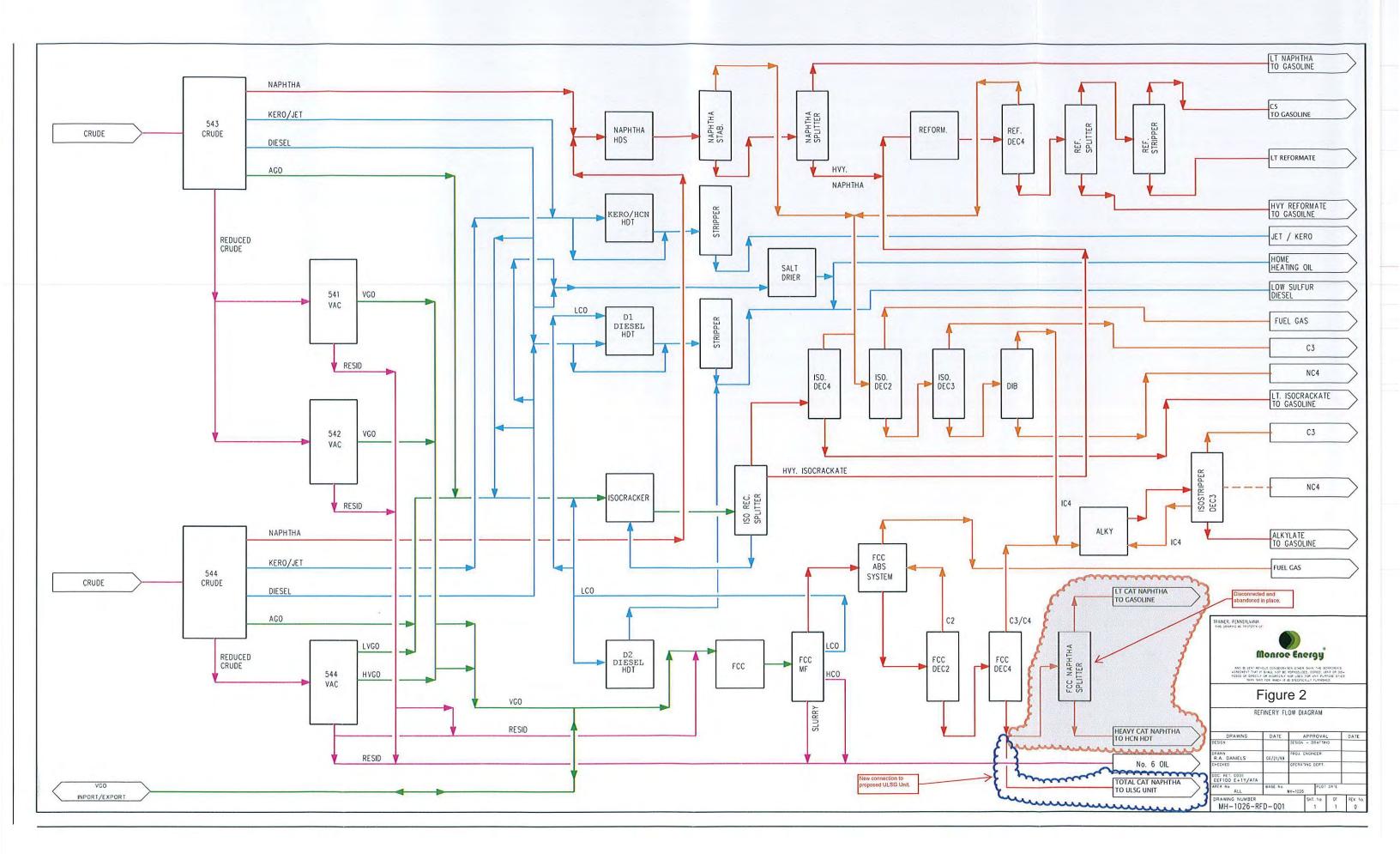
Figure 1 shows the location of the Trainer Refinery.

#### PROPOSED PROJECT DESCRIPTION

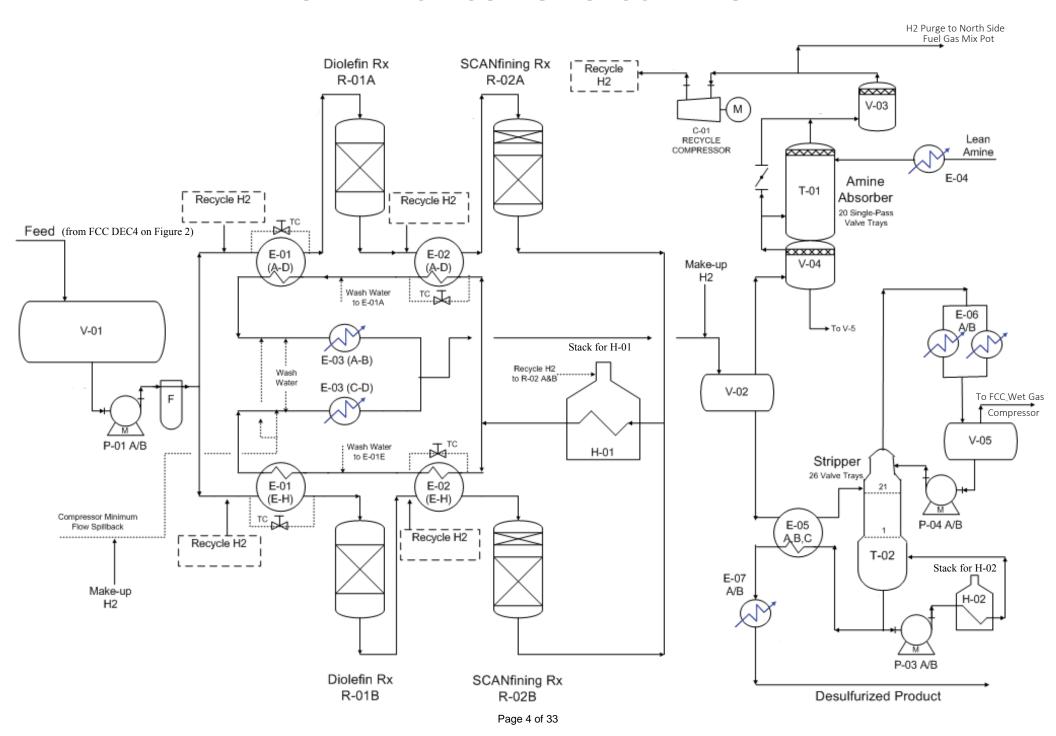
Monroe Energy proposes to purchase and relocate the low sulfur gasoline process unit from the former Sunoco, Marcus Hook Refinery to the Trainer Refinery to meet the U.S. EPA Tier 3 Motor Vehicle Emission and Fuel Standards rule (Tier 3 standards). Exxon Mobil Corporation, the process technology licenser, has reviewed Monroe's proposed feed rates and feed qualities and has verified that the unit can meet the product sulfur levels of the Tier 3 standards. The process will be referred to as the Ultra Low Sulfur Gasoline (ULSG) unit at the Trainer Refinery. Figure 2 represents the general process flow at the Trainer Refinery, and highlights the changes to the existing configuration that will result from the proposed project. Figure 3 provides a diagram of the process flow of the proposed ULSG unit.

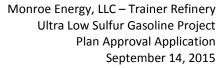


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# Figure 3 - Process Flow ULTRA LOW SULFUR GASOLINE UNIT







At maximum gasoline operation, the Refinery's current configuration allows for the Fluid Catalytic Cracking (FCC) unit (Source ID 101) to nominally produce 34,000 barrels per day (BPD) of total cat naphtha. Currently the cat naphtha stream is split into a light and a heavy stream, with only the heavy cat naphtha stream being desulfurized in the Heavy Cat Naphtha (HCN) hydrotreating unit. The HCN unit also currently processes up to 8,500 BPD of straight run naphtha, however this stream to the HCN unit is not desulfurized in the reactor and is sent to the product stripper for stabilization. To meet the Tier 3 standards, a higher level of desulfurization is needed for all naphtha streams (i.e., straight run naphtha, light cat naptha, and HCN); however, the Refinery cannot meet Tier 3 standards as it is currently configured.

To attain the level of desulfurization required to meet Tier 3 standards, the Refinery proposes to install and operate the new ULSG unit. The ULSG unit will utilize two (2) refinery fuel gas-fired process heaters rated at approximately 99.6 and 44.2 MMBtu/hr. The ULSG unit will be designed for a total naphtha flow rate of 44,000 BPD, comprised of up to 34,000 BPD of total cat naphtha from the FCC unit and up to 10,000 BPD of straight run naphtha from the crude units. Shifting the processing of these streams to the proposed ULSG can result in changes to the short-term crude processing rate and the short-term processing rates of other units at the Trainer Refinery. The annual processing capacity of the refinery is dependent on many variables including, but not limited to, the properties of the crude being processed, catalyst life cycle in units throughout the Refinery, and customer product specifications, and will not be impacted by the project.

The nominal amount of straight run naphtha currently sent to the HCN unit stripper for stabilization is up to 8,500 BPD. The proposed process configuration will divert this stream to the ULSG unit at a nominal design rate of up to 10,000 BPD. Up to 1,500 BPD of excess straight run naphtha will be diverted from the Naphtha Hydrotreater (NHT) unit allowing for short-term flexibility in crude processing rates. Based on the Trainer Refinery's 2014 average crude composition, the naphtha yield was approximately 30%. Therefore, an increase in naphtha processing capability up to 1,500 BPD could allow for a short-term average increase in the overall crude processing rate of up to 5,000 BPD. In turn, the short-term average crude processing rate increase could, under



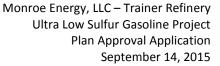
certain operating conditions, influence the short-term feed rates of several existing process units at the Refinery. Specifically, the process units that could see these short-term changes are the D1 and D2 diesel hydrotreaters (Source IDs 736 and 741, respectively), the Isocracker 1<sup>st</sup> Stage Heater (Source ID 739), the Isocracker Splitter Reboiler (Source ID 740), and the sulfur recovery unit (SRU) (Source ID 102). Following implementation of the proposed project, the existing HCN unit will be operated as either a naphtha hydrotreater or a distillate (jet) hydrotreater.

The proposed ULSG unit will require hydrogen to remove the feed sulfur. However, the existing Platformer unit (Source ID 119) that produces the Refinery's hydrogen supply is limited by the availability of heavy naphtha feed. To make hydrogen available for the ULSG unit, an estimated 4,100 BPD of light cycle oil (LCO) will be shifted away from the Isocracker to the D1 and D2 hydrotreaters. This LCO shift from the Isocracker to the D1 and D2 hydrotreater units will decrease the olefin saturation and consume less hydrogen, thereby making hydrogen available for the proposed ULSG unit. The shift will also result in a small increase in ULSD production.

The FCC unit operates to a coke burn limit and will not be able to increase feed rate as a result of the proposed project. However, under the proposed configuration, on average it will consume more residual oil to minimize the production of number 6 oil. In order to process the residual oil while remaining at the FCC unit coke burn limit, some gasoil feed will be shifted to the Isocracker, resulting in a processing rate increase of gasoil at the Isocracker. The net Isocracker feed rate is expected to decrease because more LCO will be shifted away from the Isocracker than vacuum gas oil (VGO) shifted to the Isocracker.

It is important to note that the feed shifts and resulting short-term processing rate changes described herein do not represent new modes of operation, as feed shifts such as those described above regularly occur to ensure that the Refinery produces on-specification products while maximizing profitability.

The potential increase in the short-term crude processing rate and downstream process unit rates could result in process unit heater firing rate increases. Specifically, the process unit heaters which





could see firing rate increases are the FCCU feed heater (Source ID 733), the VCD 541, 542 and 544 vacuum heaters (Source IDs 742, 743 and 746, respectively), the ACD 543 and 544 crude heaters (Source IDs 744 and 745, respectively), the Kero/HCN HTU feed heater (Source ID 735), the naphtha HDS heater (Source ID 737), and the Platformer feed heaters (Source ID 738). The projected future actual process heater firing rates are conservatively assumed to be proportional to the changes in expected short-term feed and product rate changes but are within the normal short-term operating ranges that have been observed historically. In addition to these process unit heater firing rate changes, an increase in short-term steam demand is anticipated to support Refinery operations. The steam is assumed to be produced by existing Boilers 9 and 10 (Source IDs 034 and 035 respectively). No physical modification of the boilers will be made as part of the proposed project and there will be no increase in the hourly maximum steam generating capacity of the boilers. The proposed project could also result in increased short-term product throughput rates of the Refinery's storage tanks for crude, diesel fuel, jet fuel and gasoline blending components.

Finally, the ULSG unit requires trim cooling on the reactor effluent stream and the product cooler. This cooling water demand will be provided by a proposed new cooling tower. The proposed new cooling tower water flow rate is based on the original heat exchanger design. Cooling tower water make-up will be provided by the local municipal water authority. New cooling tower blowdown will be directed to the Trainer Refinery's existing onsite Advanced Wastewater Treatment Plant (AWWTP). No air emissions increase from blowdown to the AWWTP is expected because the Refinery assumes that any trace amounts of organics present in the cooling water return as a result of heat exchanger leaks, will be stripped out by the cooling tower. This assumption conforms with the work practice standards, and reporting requirements for heat exchanger systems found in 40 CFR Part 63, Subpart CC.

There will be no physical modifications to existing air emissions sources at the Refinery as part of the proposed project. A complete list of the new and affected units from the proposed project is provided in the following Emissions Inventory section.



#### **EMISSIONS INVENTORY**

This section presents an inventory of the emissions increases associated with the proposed ULSG project. Tables referenced in this section are found in Attachment C.

The Trainer Refinery is located in an area that is classified as nonattainment with respect to the 2008 1-hour ozone and 2012 annual particulate matter (PM) less than 2.5 microns (PM<sub>2.5</sub>) National Ambient Air Quality Standards (NAAQS). The area is either attainment, or unclassifiable, with respect to all of the other NAAQS. Since the Refinery already qualifies as a major stationary source under both of the major New Source Review (NSR) regulations, the project must be evaluated to determine if it qualifies as a major modification under the PADEP nonattainment NSR (NNSR) rules for ozone and PM<sub>2.5</sub>, and the Federal Prevention of Significant Deterioration (PSD) rules for the other regulated NSR pollutants.

To complete the major NSR applicability assessment, an emissions inventory was developed for the project. The NSR applicability assessment includes the analysis of baseline actual emissions (BAE) rates, projected actual emission (PAE) rates, and could have accommodated (CHA) emission rates for affected units, and potential to emit (PTE) rates for new units. BAE rates are calculated for all existing emission units that are either modified or affected by the proposed project. No existing emissions units will be modified as a result of the proposed project. The affected emissions units for this project are as follows:

- FCC Unit (Source ID 101)
- FCCU Feed Heater (Source ID 733)
- Kerosene/HCN HTU Feed Heater (Source ID 735)
- Diesel HTU Heater (Source ID 736)
- D2/VGO Hydrotreater Feed Heater (Source ID 741)
- Naphtha HDS Heater (Source ID 737)
- Platformer Feed Heater (Source ID 738)
- Isocracker 1<sup>st</sup> Stage Heater (Source ID 739)
- Isocracker Splitter Reboiler (Source ID 740)
- VCD 541 VAC Heater (Source ID 742)
- VCD 542 VAC Heater (Source ID 743)
- VCD 544 VAC Heater (Source ID 746)



- ACD 543 Crude Heater (Source ID 744)
- ACD 544 Crude Heater (Source ID 745)
- Boiler 9 (Source ID 034)
- Boiler 10 (Source ID 035)
- Claus Sulfur Recovery Plant (Source ID 102)
- Main Flare (Source ID 103)
- Tank 93 (Source ID 165)
- Tank 94 (Source ID 166)
- Tank 95 (Source ID 126)
- Tank 96 (Source ID 127)
- Tank 152 (Source ID 137)
- Tank 153 (Source ID 138)
- Tank 155 (Source ID 140)
- Tank 157 (Source ID 142)
- Tank 158 (Source ID 300)
- Tank 159 (Source ID 143)
- Tank 160 (Source ID 194)
- Tank 161 (Source ID 144)
- Tank 162 (Source ID 145)
- Tank 163 (Source ID 146)
- Tank 164 (Source ID 147)
- Tank 165 (Source ID 148)
- Tank 166 (Source ID 149)
- Tank 168 (Source ID 150)
- Tank 170 (Source ID 152)
- Tank 174 (Source ID 155)
- Tank 175 (Source ID 156)
- Tank 178 (Source ID 157)
- Tank 181 (Source ID 160)
- Tank 182 (Source ID 161)
- Tank 185 (Source ID 163)
- Tank 186 (Source ID 164)

#### **Baseline Actual Emission Rates**

The major NSR rules specify that BAE rates be developed using the average rate, in tons per year (tpy), of any historic 24-consecutive month period during the 10 years prior to submission of a completed plan approval application for PSD and five (5) years for NNSR. Monthly emission



rates were developed for the Refinery operating period beginning in September 2005 through July 2015.

For the affected units, BAE for criteria pollutants, with the exception of lead, sulfur dioxide (SO<sub>2</sub>), hydrogen sulfide (H<sub>2</sub>S), total reduced sulfur (TRS), and greenhouse gas (GHG), are determined using historic production data and emission rates consistent with the regulatory definitions of BAE in the NNSR and PSD regulations. For the purposes of this evaluation, the PM emissions shown are representative of the filterable portion of PM only. PM less than 10 microns (PM<sub>10</sub>) and PM<sub>2.5</sub> are representative of both the filterable portion of each respective particle size and condensable PM emissions, where data are available.

Lead emissions have been included in the BAE inventory using the emissions factor for lead from U.S. EPA *AP-42 Compilation of Air Pollutant Emissions Factors*, for lead in natural gas combustion and multiplying by the historic fuel usage of the affected units. SO<sub>2</sub> emissions in the BAE inventory are also determined using historic production data and have been corrected to reflect the 12-month rolling average (calculated monthly) TVOP limits for H<sub>2</sub>S concentration in the north and south side refinery fuel gas supply [50 and 48 parts per million dry volume (ppmvd), respectively] assuming a full conversion of H<sub>2</sub>S to SO<sub>2</sub>. H<sub>2</sub>S and TRS emissions are determined using historic heat input and fuel usage data and emissions factors from U.S. EPA's *Emission Estimation Protocol for Petroleum Refineries*. GHG emissions have been included in the baseline using the appropriate emissions factors listed in 40 CFR Part 98.

On June 23, 2014 the U.S. Supreme Court, in *Utility Air Regulatory Group v. EPA*, struck down portions of the GHG "Tailoring Rule," which modified the GHG major source criteria for inclusion in the PSD and Title V programs. The U.S. EPA August 19, 2015 final rulemaking officially removed the requirements that were struck down in the June 23, 2014 court decision. While the recent U.S. Supreme Court decision on GHG permitting did not remove consideration of GHG PSD permitting when the permitting project already triggers PSD permitting for one of the conventional PSD pollutants (i.e. nitrogen dioxide (NO<sub>2</sub>), volatile organic compounds (VOC), SO<sub>2</sub>, carbon monoxide (CO), etc.), the Supreme Court did determine that the U.S. EPA lacked the



authority to require PSD permitting solely on the basis of the GHG emission levels. This project is not otherwise subject to PSD for non-GHG pollutants, and therefore cannot be subject PSD to permitting solely for GHG emissions.

Since the Refinery is located in a nonattainment area for both the 2008 1-hour ozone and 2012 annual PM<sub>2.5</sub> NAAQS, the proposed project must also be assessed to determine the potential applicability of the Pennsylvania NNSR rules. The Pennsylvania NNSR rules limit the period for determining BAE to any consecutive 24-month period in the five (5) years immediately prior to the date a complete plan approval application is received by PADEP. Nitrogen oxides (NO<sub>X</sub>) and volatile organic compounds (VOC) are precursors to the formation of ozone and must be evaluated for NNSR applicability. When evaluating NNSR for ozone significance, the baseline periods must be the same for VOC and NO<sub>X</sub>. For PM<sub>2.5</sub>, the precursor pollutants that require evaluation along with PM<sub>2.5</sub> are NO<sub>X</sub> and SO<sub>2</sub>. When evaluating for PM<sub>2.5</sub>, the baseline periods for PM<sub>2.5</sub>, SO<sub>2</sub> and NO<sub>X</sub> must be the same.

Tables C-1 and C-2 summarize the BAE selected for PSD and NNSR, respectively. These tables include both the individual emissions unit BAE rates and the total project BAE rates on a pollutant-by-pollutant basis, and also identify the baseline period selected for each PSD and NNSR pollutant.

#### Projected Actual Emissions Rates

Tables C-3 through C-25 detail the PAE rates for emissions units that are affected by proposed project. Where available, continuous emissions monitoring system (CEMS) and stack test data were used to calculate PAE rates for each affected or modified unit. When CEMS or stack test data were not available, emissions were calculated using *AP-42 Compilation of Air Pollutant Emissions Factors* for natural gas combustion. SO<sub>2</sub> emissions were calculated as they were in the baseline (i.e., using the TVOP H<sub>2</sub>S concentration limits in the refinery fuel gas assuming 100 percent conversion to SO<sub>2</sub>). GHG emissions were calculated using the appropriate 40 CFR Part 98 emissions factors.



A plan approval application that affects the SRU was submitted to PADEP on May 18, 2015. With the exception of SO<sub>2</sub>, the PAE rates for all other PSD pollutants for the SRU are calculated consistently with that plan approval application. However, the expected SO<sub>2</sub> emissions increase resulting from the modification proposed in that application have not been incorporated into this analysis. The SO<sub>2</sub> emission increases associated with the modification in that application were approximately 0.04 tons per year (tpy). This emission increase has been accounted for in the contemporaneous emission increases analysis, show in Table C-36 of Attachment C.

Since the future operation of the Main Flare will include the flare gas recovery unit (FGRU) that is currently nearing completion of construction, the flare will primarily only receive gases during upset conditions. The PAE rates for the Main Flare are calculated by first annualizing the average of the three (3) highest emitting months from 2013-2014 and then applying an 80% reduction to reflect the gases that will no longer be combusted in the Main Flare due to their recovery in the FGRU. As discussed previously, operations at the Refinery fluctuate on a monthly basis, making it hard to predict how both the Main Flare and tanks may be affected in the future. Monroe believes that evaluating the average of the three (3) highest emitting months, conservatively captures future fluctuations. Similarly, PAE rates for the affected tanks are calculated by annualizing the average of the three (3) highest emitting months from 2013-2014.

#### Potential to Emit Emissions Rates

Tables C-26 through C-30 detail the PTE rates of the new units associated with the proposed project. The new units include the two (2) new feed heaters, cooling tower, and new fugitive emissions as a result of this proposed project. PTE rates for the new units are calculated using vendor-guaranteed emissions rates, the sulfur content limit of the refinery fuel gas (50 ppmvd H<sub>2</sub>S, annual average), *AP-42 Compilation of Air Pollutant Emissions Factors*, 40 CFR Part 98, design specifications, and engineering estimates.

The cooling tower VOC emissions were calculated using guidance developed by the Texas Commission of Environmental Quality (TCEQ), titled *Air Stripping Method (Modified El Paso* 



Method) for Determination of Volatile Organic Compound Emissions from Water Sources, Sampling Procedures Manual, Appendix P: Cooling Tower Monitoring Guidance (Guidance). The annual emissions rate of 6.02 tons of VOC per year corresponds to an annual average leak rate of 21 ppmv, consistent with the El Paso Method data used in the Guidance. A measurement of 21 ppmv would be approximately one-third of the delay of repair action level specified in 40 CFR §63.654(f)(3). VOC emissions from the proposed cooling tower will be the direct result of hydrocarbons leaks from water-cooled heat exchangers associated with the ULSG unit. The frequency and extent of future leaks is unpredictable, therefore Monroe believes that this assumption represents the maximum worst-case PTE rate on an annual basis for the ULSG heat exchangers that will be serviced by the proposed new cooling tower.

VOC emissions from fugitive sources were calculated using U.S. EPA's *Protocol for Equipment Leak Emission Estimates*.

Table C-31 summarizes total emissions from the new and affected units as a result of the project (i.e., PTE and PAE). This table includes both the individual emissions units' PAE or PTE rates and the total projected emissions rates on a pollutant-by-pollutant basis.

#### Could Have Accommodated Emissions Rates

Tables C-32 and C-33 detail the excludable emissions analysis, or emissions that "could have been accommodated" during the baseline period. The applicable NSR regulations establish that the source may exclude that portion of the emissions that the unit CHA during the baseline period and that are unrelated to the project, including increase utilization due to demand growth as per 25 Pa. Code §127.203a(a)(5)(i)(c) and 40 CFR §52.21(b)(41).

Monroe determined CHA emissions by annualizing the highest monthly emissions for each affected unit and pollutant within the selected baseline period for that pollutant. This approach represents a reasonable estimation of what the source was capable of emitting at a sustained level during the baseline period. CHA emissions were then evaluated as part of the process detailed in



Table C-33, where the CHA emissions are factored into the determination of the total project increases.

PSD and NNSR applicability is assessed in the Regulatory Analysis section of this application.

#### **REGULATORY ANALYSIS**

Monroe has reviewed the Federal and Commonwealth of Pennsylvania air quality regulations to determine which regulations potentially apply to the proposed project. A summary of potentially applicable air quality requirements follows.

#### FEDERAL REGULATIONS

For the purpose of this application, potentially applicable Federal regulations are defined as:

- Standards of Performance for New Stationary Sources (NSPS)
- National Emission Standards for Hazardous Air Pollutants (NESHAP)
- New Source Review (NSR)

A discussion of each specific Federal requirement is provided in the following subsections.

#### **Standards of Performance for New Stationary Sources**

U.S. EPA has promulgated standards of performance for new, modified, or reconstructed sources [i.e., New Source Performance Standards (NSPS)] of air pollution at 40 CFR Part 60. The following NSPS are potentially applicable to the proposed Ultra Low Sulfur Gasoline (ULSG) project:

- 40 CFR Part 60, Subpart A General Provisions
- 40 CFR Part 60, Subpart Ja Standards of Performance for Petroleum Refineries for Which Construction, Reconstruction, or Modification Commenced After May 14, 2007
- 40 CFR Part 60, Subpart GGGa Standards of Performance for Equipment Leaks of VOC in Petroleum Refineries for Which Construction, Reconstruction, or Modification Commenced After November 7, 2006



• 40 CFR Part 60, Subpart QQQ – Standards of Performance for VOC Emissions from Petroleum Refinery Wastewater Systems

#### 40 CFR Part 60, Subpart A – General Provisions

The provisions of 40 CFR Part 60, Subpart A apply to the owner or operator of any stationary source subject to a NSPS under 40 CFR Part 60. Because the proposed project is subject to other subparts of 40 CFR Part 60, the requirements of Subpart A will also apply. Monroe will comply with each applicable section of 40 CFR Part 60, Subpart A.

# 40 CFR Part 60, Subpart Ja – Standards of Performance for Petroleum Refineries for Which Construction, Reconstruction, or Modification Commenced After May 14, 2007

Standards of Performance for Petroleum Refineries for Which Construction, Reconstruction, or Modification Commenced After May 14, 2007, have been codified in 40 CFR Part 60, Subpart Ja. Applicability to Subpart Ja is established in §60.100a(b) wherein owners and operators are deemed affected if a fuel gas combustion device (including process heaters) is constructed after May 14, 2007. The two (2) ULSG unit process heaters will be subject to 40 CFR Part 60, Subpart Ja. In accordance with §60.102a(g)(1)(ii), fuel gas combustion units may not burn fuel gas that contains H<sub>2</sub>S in excess of 162 ppmv on a 3-hr rolling average basis and in excess of 60 ppmv daily on a 365-day rolling average basis. The Refinery's North Side fuel gas system supplies fuel gas that contains H<sub>2</sub>S at concentrations lower than 60 ppmv, as it is currently required to meet a lower H<sub>2</sub>S limit of 50 ppmv for Boilers 9 and 10 (Source IDs 034 and 035). Fuel gas supplied to the ULSG unit process heaters will continue to meet these existing lower H<sub>2</sub>S concentration requirements. Pursuant to §60.107a(a)(2), Monroe is required to install, operate, calibrate, and maintain an instrument for continuous monitoring and recording of the concentration of H<sub>2</sub>S before the fuel gas is burned. Monroe currently monitors the H<sub>2</sub>S concentration in its refinery fuel gas using an approved continuous H<sub>2</sub>S monitor. By complying with the fuel gas H<sub>2</sub>S limit in §60.102a(g)(1)(ii), the proposed ULSG unit process heaters will not be subject to the SO<sub>2</sub> concentration limits of 40 CFR Part 60, Subpart Ja. 40 CFR Part 60, Subpart Ja does not require fuel gas combustion devices to comply with specific PM emission standards.



In accordance with §60.102a(g)(2)(i)(B), emissions of NO<sub>X</sub> for natural draft process heaters firing refinery fuel gas are limited to 0.040 pounds per MMBtu (lb/MMBtu) higher heating value basis determined daily on a 30-day rolling average. Monroe proposes to meet this requirement by utilizing low NO<sub>X</sub> burners to control the NO<sub>X</sub> emissions from the proposed ULSG unit process heaters. Compliance will be assured by monitoring the type of fuel being fired, the fuel firing rate, fuel gas heating value (Btu/scf), and NO<sub>X</sub> emissions by a continuous emission monitoring system (CEMS). Monroe will install and operate NO<sub>X</sub> and O<sub>2</sub> CEMS on the proposed ULSG unit process heater stacks in accordance with §60.107a. In addition, the NO<sub>X</sub> and O<sub>2</sub> CEMS on the proposed ULSG unit process heater stacks will be certified and operated pursuant to Revision 8 of PADEP's Continuous Source Monitoring Manual.

Pursuant to §60.103a(c)(2), Monroe will be required to conduct a root cause analysis and a corrective action analysis for the ULSG process heaters, for each instance that the SO<sub>2</sub> discharge to the atmosphere is 227 kilograms (500 pounds) greater than the amount that would have been emitted if the emission limit in §60.102a(g)(1)(ii) had been met during one (1) or more consecutive periods of excess emissions or any 24-hour period, whichever is shorter. Pursuant to §60.103a(d), the root cause analysis and corrective action analysis must be completed as soon as possible, but no later than 45 days after a discharge meeting the aforementioned condition.

In accordance with \$60.104a(a), Monroe must conduct a NO<sub>X</sub> performance test of the new ULSG unit process heaters no later than 60 days after achieving the maximum production rate or 180 days after initial startup, whichever comes first. The NO<sub>X</sub> performance test must be conducted in accordance with \$60.104a(i).

The notification, recordkeeping, and reporting requirements of §60.108a will apply to the ULSG unit process heaters subsequent to the project. Specifically, Monroe will meet the notification requirements of §60.108a(b), the applicable records maintenance requirements of §60.108a(c), the excess emissions reporting requirements of §60.108a(d), and all other applicable notification, recordkeeping or reporting requirements found in §60.7.



# 40 CFR Part 60, Subpart GGGa – Standards of Performance for Equipment Leaks of VOC in Petroleum Refineries for Which Construction, Reconstruction, or Modification Commenced After November 7, 2006

The proposed ULSG unit is also potentially subject to 40 CFR Part 60, Subpart GGGa - Standards of Performance for Equipment Leaks of VOC in Petroleum Refineries for Which Construction, Reconstruction, or Modification Commenced After November 7, 2006, which establishes standards for equipment leaks of VOC. Pursuant to §60.590a(a), affected facilities are compressors or the group of equipment within a process unit. §60.591a defines a process unit as follows:

"Process unit means the components assembled and connected by pipes or ducts to process raw materials and to produce intermediate or final products from petroleum, unfinished petroleum derivatives, or other intermediates. A process unit can operate independently if supplied with sufficient feed or raw materials and sufficient storage facilities for the product. For the purpose of this subpart, process unit includes any feed, intermediate and final product storage vessels (except as specified in §60.482-1a(g)), product transfer racks, and connected ducts and piping. A process unit includes all equipment as defined in this subpart."

All of the valves, flanges, pumps, etc. associated with the proposed ULSG unit will be subject to this NSPS. The Refinery already has a number of existing components that are subject to Subpart GGGa, and the addition of the components associated with the ULSG unit will not change the existing Subpart GGGa requirements. Monroe will continue to comply with the applicable Subpart GGGa requirements.

## 40 CFR Part 60, Subpart QQQ – Standards of Performance for VOC Emissions from Petroleum Wastewater Systems

Standards of Performance for VOC Emissions from Petroleum Refinery Wastewater Systems have been codified in 40 CFR Part 60, Subpart QQQ, which addresses VOC emissions from individual



and aggregate drain systems, and oil-water separators, receiving oily wastewater from petroleum refinery process units. The blowdown from the proposed new cooling tower will be introduced into the existing onsite wastewater system and directed to the Trainer Refinery's existing onsite AWWTP. However, the cooling tower blowdown is not oily wastewater from a refinery process unit and thus installation of the cooling tower and associated blowdown drain piping will not be subject to Subpart QQQ. The proposed ULSG unit will not be subject to Subpart QQQ because the proposed unit will not include new drain systems to the AWWTP.

#### **National Emission Standards for Hazardous Air Pollutants**

U.S. EPA has promulgated National Emission Standards for Hazardous Air Pollutants (NESHAPs) at 40 CFR Parts 61 and 63. NESHAPs promulgated prior to the Clean Air Act Amendments (CAAA) of 1990, found in 40 CFR Part 61, apply to specific compounds emitted from specific processes. Pursuant to the CAAA of 1990, process-specific NESHAPs are promulgated in 40 CFR Part 63. NESHAPs rules promulgated under 40 CFR Part 63, commonly referred to as MACT standards, apply to source categories that are considered area sources or major sources of hazardous air pollutants (HAPs).

Under the MACT rules, a major source of HAP is defined as a source with the facility-wide potential to emit (PTE) of any single HAP of 10 tons per year or more, or with a facility-wide PTE for total HAP of 25 tons per year or more. The Refinery is classified as a major source of HAP emissions; therefore, the following NESHAPs are potentially applicable to the proposed ULSG project:

- 40 CFR Part 61, Subpart A General Provisions
- 40 CFR Part 61, Subpart FF National Emission Standard for Benzene Waste Operations
- 40 CFR Part 63, Subpart A General Provisions
- 40 CFR Part 63 Subpart Q National Emission Standards for Hazardous Air Pollutants for Industrial Process Cooling Towers



- 40 CFR Part 63, Subpart CC National Emission Standards for Hazardous Air Pollutants from Petroleum Refineries
- 40 CFR Part 63, Subpart UUU National Emission Standards for Hazardous Air Pollutants for Petroleum Refineries: Catalytic Cracking Units, Catalytic Reforming Units, and Sulfur Recovery Units
- 40 CFR Part 63, Subpart DDDDD National Emission Standards for Hazardous Air Pollutants for Major Sources: Industrial, Commercial, and Institutional Boilers and Process Heaters

#### 40 CFR Part 61, Subpart A – General Provisions

The provisions of 40 CFR Part 61, Subpart A apply to the owner or operator of any stationary source subject to a NESHAP under 40 CFR Part 61. Because the project is subject to other subparts of 40 CFR Part 61, the requirements of Subpart A will also apply. Monroe will comply with each applicable section of 40 CFR Part 61, Subpart A.

#### 40 CFR Part 61, Subpart FF – National Emission Standard for Benzene Waste Operations

The National Emission Standard for Benzene Waste Operations (BWON) is codified in 40 CFR Part 61, Subpart FF and applies to petroleum refineries with benzene-containing hazardous waste. The proposed new cooling tower will direct blowdown to the existing AWWTP at the Refinery. Monroe samples and analyzes the influent to the AWWTP for benzene and other HAPs as part of the Refinery's existing BWON program, and will continue to do so following the project.

#### 40 CFR Part 63, Subpart A – General Provisions

The provisions of 40 CFR Part 63, Subpart A apply to the owner or operator of any stationary source subject to a NESHAP under 40 CFR Part 63. Because the project is subject to other subparts of 40 CFR Part 63, the requirements of Subpart A will also apply. Monroe will comply with each applicable section of 40 CFR Part 63, Subpart A.



## 40 CFR Part 63, Subpart Q – National Emission Standards for Hazardous Air Pollutants for Industrial Process Cooling Towers

The NESHAPs for Industrial Process Cooling Towers have been codified at 40 CFR Part 63, Subpart Q. Subpart Q affects all new industrial process cooling towers that are operated with the use of chromium-based water treatment chemicals and that are integral parts of a facility that is a major source. The Trainer Refinery is a major source of HAP emissions and therefore, the proposed cooling tower is potentially subject to Subpart Q. The Refinery has no plans to use chromium-based chemicals in the new cooling tower and requests that PADEP include a requirement in the plan approval for the proposed cooling tower that prohibits the use of chromium-based chemicals to avoid triggering Subpart Q. A similar condition exists in the Refinery's current TVOP for the existing cooling towers (Source ID 111). Therefore, Subpart Q will not apply.

### <u>40 CFR Part 63, Subpart CC – National Emission Standards for Hazardous Air Pollutants</u> <u>from Petroleum Refineries</u>

The NESHAPs for Petroleum Refineries have been codified in 40 CFR Part 63, Subpart CC and includes provisions that apply to all heat exchange systems in HAP service at petroleum refineries. The proposed cooling tower and all petroleum refinery process unit heat exchangers that are in organic HAP service (as defined in §63.641), and serviced by the cooling tower, and all water lines to and from these petroleum refinery process unit heat exchangers, are considered a heat exchange system and are subject to Subpart CC, specifically §63.654. Monroe will follow the monitoring plan requirements of §63.654(c)(1) for closed-loop recirculation heat exchange systems and the applicable reporting and recordkeeping requirements outlined in §63.655. Compliance is required upon startup.

The "affected source" under 40 CFR Part 63, Subpart CC is defined as "...the collection of emission points to which this subpart applies as determined by the criteria in §63.640". The addition of the proposed cooling tower is not considered "reconstruction" of the existing affected



source pursuant to 40 CFR Part 63, Subpart A (§63.2 – Definitions), because the fixed capital cost of the proposed cooling tower does not exceed 50 percent of the fixed capital cost that would be required to construct a comparable new source. Therefore, the affected source under 40 CFR Part 63, Subpart CC at the Refinery will remain an existing source, and for equipment in HAP service compliance with the provisions of 40 CFR Part 60, Subpart VV - Standards of Performance for Equipment Leaks of VOC in the Synthetic Organic Chemicals Manufacturing Industry for which Construction, Reconstruction, or Modification Commenced After January 5, 1981, and on or Before November 7, 2006 is specified under 40 CFR Part 63, Subpart CC (§63.648(a)(1)). As previously stated, the fugitive components associated with the proposed ULSG unit will be subject to fugitive emission monitoring pursuant to Subpart GGGa. Because the monitoring requirements are more stringent than the monitoring requirements of Subpart VV, the Refinery's compliance with Subpart GGGa will ensure compliance with Subpart CC.

40 CFR Part 63, Subpart CC also includes standards for storage vessels and wastewater streams, at §63.646 and §63.647, respectively. Monroe has previously established monitoring, recordkeeping, and reporting systems for existing affected sources in accordance with the provisions of §63.653 and §63.644. Monroe will integrate newly affected sources and processes into the existing monitoring, recordkeeping, an reporting systems, as applicable.

## <u>40 CFR Part 63, Subpart UUU – National Emission Standards for Hazardous Air Pollutants</u> <u>for Petroleum Refineries: Catalytic Cracking Units, Catalytic Reforming Units, and Sulfur</u> Recovery Units

40 CFR Part 63, Subpart UUU – National Emission Standards for Hazardous Air Pollutants for Petroleum Refineries: Catalytic Cracking Units, Catalytic Reforming Units, and Sulfur Recovery Units, which applies to process vents or bypass lines on catalytic cracking units, catalytic reforming units, and sulfur recovery plant units at petroleum refineries. The proposed ULSG unit will not be subject to Subpart UUU; however, the proposed project will result in a nominal increase of crude throughput at the Refinery of 5,000 barrels per day which will in turn affect the Refinery's



units that are subject to Subpart UUU (i.e., the Platformer, FCC Unit, and SRU). The increase in crude throughput will not require the reconstruction of any Subpart UUU affected sources at the Refinery; therefore, no new requirements of Subpart UUU will be triggered as a result of the project and the Refinery will continue to comply with the applicable provisions of Subpart UUU following the proposed project.

# 40 CFR Part 63, Subpart DDDDD – National Emission Standards for Industrial, Commercial, and Institutional Boilers and Process Heaters

The NESHAPs for Industrial, Commercial, and Institutional Boilers and Process Heaters have been codified in 40 CFR Part 63, Subpart DDDDD (Boiler MACT), and will be applicable to the proposed H-01 and H-02 process heaters that are associated with the proposed ULSG process. The process heaters and ULSG processing unit are approximately ten years old and are being purchased by Monroe from an existing nearby refinery which ceased operations in 2010. Because the heaters are not new and are not being reconstructed, they are considered existing sources under Subpart DDDDD in accordance with §63.7490(d). As existing process heaters, compliance must be achieved by January 31, 2016, or upon start-up. The proposed USLG process and associated processes will not start-up prior to January 31, 2016, therefore, compliance with the applicable Boiler MACT provisions will be demonstrated upon start-up.

The proposed H-01 and H-02 process heaters will combust only refinery gas, which meets the Boiler MACT definition of a gas 1 fuel. Pursuant to \$63.7500(e), units designed to combust gas 1 fuels are not subject to the emissions limits in Subpart DDDDD when combusting only gas 1 fuels. Boilers and process heaters that combust only gas 1 fuels (e.g., natural gas and refinery gas), are subject only to the work practice standards codified in Subpart DDDDD. This includes the annual tune-up requirements specified at \$63.7540(a)(10) and a one-time energy assessment specified at \$63.7510(j). Monroe will comply with the applicable portions of the Boiler MACT provisions upon startup of the proposed H-01 and H-02 process heaters.



#### New Source Review (NSR)

The Trainer Refinery is located in Delaware County. Delaware County is classified as in attainment or unclassifiable for the NAAQS for all NSR-regulated pollutants except PM<sub>2.5</sub> and ozone. Therefore, the Refinery must evaluate applicability of both the NNSR and PSD regulations.

#### Nonattainment New Source Review (NNSR)

U.S. EPA has approved PADEP's NNSR regulations through their incorporation into Pennsylvania's State Implementation Plan (SIP). These state-specific NNSR regulations are codified in Title 25 – Environmental Protection of the Pennsylvania Code (Pa. Code) Chapter 127, Subchapter E. NNSR applicability is addressed under the Commonwealth of Pennsylvania regulatory review section of this application.

#### Prevention of Significant Deterioration (PSD)

Pennsylvania has adopted the Federal PSD regulations cited at 40 CFR §52.21 in their entirety in Subchapter D of Chapter 127 of the state air regulations. The Trainer Refinery meets the definition of a major stationary source with respect to the Federal PSD rules. Therefore, the proposed project emissions must be evaluated to determine if the project qualifies as a major modification under the PSD regulations. In order to determine whether a proposed project at an existing major source is subject to regulation under the PSD rules, a two (2)-step applicability test is required. In Step 1, the emissions increases from the new, modified, and affected emissions units comprising the project are summed and compared to the PSD significant emission increase thresholds for each regulated NSR pollutant emitted. If the project emissions increases exceed the significance levels for any of the regulated NSR pollutants, a Step 2 analysis that evaluates net facility-wide emissions increases is required. If no PSD significant increases are determined under the Step 1 assessment, the Step 2 analysis is not required. Table C-34 in Attachment C presents the PSD applicability assessment for the proposed project. As demonstrated by the data presented in the table, the emissions increases for the regulated NSR pollutants emitted for the project emissions units are



below the PSD significance levels for Step 1. As a result, no further assessment is required and the proposed project is not subject to the PSD permitting requirements.

#### COMMONWEALTH OF PENNSYLVANIA REGULATIONS

The proposed project is potentially subject to the following Pennsylvania air quality regulations which are codified in Title 25 – Environmental Protection of the Pennsylvania Code (Pa. Code):

- Chapter 122 National Standards of Performance for New Stationary Sources
- Chapter 123 Standards for Contaminants
- Chapter 124 National Emission Standards for Hazardous Air Pollutants
- Chapter 127 Construction, Modification, Reactivation, and Operation of Sources
- Chapter 129 Standards for Sources

A discussion of each specific Commonwealth requirement is provided in the following subsections.

#### Chapter 122 – National Standards of Performance for New Stationary Sources

The Federal NSPS are adopted in their entirety by reference at 25 Pa. Code §122.3 and are discussed in detail in the preceding section regarding Federal requirements.

#### **Chapter 123 – Standards for Contaminants**

The following sections of 25 Pa. Code Chapter 123 are applicable to the two (2) proposed process heaters:

#### Fugitive Dust Standards (25 Pa. Code §§123.1 & 123.2)

Fugitive dust emissions are prohibited from sources except those listed in 25 Pa. Code §123.1(a), for which reasonable actions shall be taken to minimize fugitive dust. The Refinery currently complies with the provisions of §§123.1 and 123.2 by employing good operating practices such as locating operations inside buildings, paved roadways, and prompt cleanup of any material spills.



Regulations that the Refinery has determined are generally applicable, such as §123.1 and §123.2, are not further identified or discussed as these provisions apply facility-wide.

#### Particulate Matter Standards (25 Pa. Code §§123.11 & 123.13)

25 Pa. Code §123.11 is applicable to combustion sources with heat inputs greater than 2.5 MMBtu/hr. The proposed ULSG unit process heaters, designated as H-02, has a heat input rating of 44.2 MMBtu/hr; therefore, pursuant to §123.11(a)(1), the allowable filterable PM emission limit for the H-02 process heater is 0.40 lb/MMBtu. The other proposed ULSG unit process heater, designated as H-01, is rated at 99.6 MMBtu/hr; therefore, pursuant to §123.11(a)(2) the following formula must be employed to determine the allowable emissions rate:

$$A = 3.6E^{-0.56}$$

where:

A = Allowable emissions in pounds per million British thermal units (MMBtu) of heat input, and

E = Heat input to the combustion unit in MMBtu/hr.

The allowable filterable PM emission limit for the H-02 process heater is 0.27 lb/MMBtu when operating at its rated capacity. Compliance with the filterable PM emission limits for both process heaters will be assured by firing only refinery fuel gas and by operation of the proposed two (2) heater according to the applicable Boiler MACT work practice standards.

#### Sulfur Compound Standards (25 Pa. Code §§123.21 & 123.22)

As combustion sources, the proposed ULSG unit process heaters will be subject to 25 Pa. Code \$123.22 (Combustion Units), which limits SO<sub>2</sub> emissions to 1.0 lb/MMBtu for facilities located in the inner Southeast Pennsylvania air basin. Compliance with this requirement will be assured through compliance with 40 CFR Part 60, Subpart Ja for fuel combustion devices.



#### Visible Emissions Standards (25 Pa. Code §§123.41 & 123.42)

The proposed ULSG unit process heaters will be subject to 25 Pa. Code §123.41 which limits visible emissions from stack sources to (1) equal to or greater than 20% for a period or periods aggregating more than 3 minutes in any 1 hour, and (2) equal to or greater than 60% at any time, except as noted in §123.42. Compliance with this standard will be ensured by combusting gaseous fuels and employing good air pollution control practices.

The following sections of 25 Pa. Code Chapter 123 are applicable to the proposed ULSG unit cooling tower:

#### Particulate Matter Standards (25 Pa. Code §§123.11 & 123.13)

The proposed cooling tower is classified as process sources under the Pennsylvania air quality regulations and are therefore subject to the 25 Pa. Code §123.13 – Processes requirements. Under §123.13(c)(1)(iii), a cooling tower with a effluent gas volume greater than 300,000 actual cubic feet per minute (acfm), may not emit filterable PM from in excess of 0.02 grains per dry standard cubic foot (gr/dscf). The proposed cooling tower will have an approximate effluent gas volume greater than 300,000 acfm, and therefore is subject to §123.13(c)(1)(iii). Installation, operation and maintenance of drift eliminators in accordance with the manufacturer's specifications will help ensure compliance with this standard.

#### **Chapter 124 – National Emission Standards for Hazardous Air Pollutants**

The Federal NESHAP are adopted in their entirety by reference at 25 Pa. Code §124.3 and are discussed in detail in the preceding section regarding Federal requirements.

#### Chapter 127 – Construction, Modification, and Reactivation of Sources

#### **Subchapter B – Plan Approval Requirements**

The proposed project is subject to the requirements of 25 Pa. Code Chapter 127 Subchapter B, which established Plan Approval requirements. 25 Pa. Code §127.11 requires PADEP approval



to construct, modify, reactivate, or install an air contamination source. Monroe is submitting this application in accordance with 25 Pa. Code §127.12, Application Contents. 25 Pa. Code §127.12(a)(5) also requires that Plan Approval Applications show that the emissions from a new source be the minimum attainable through the use of best available technology (BAT). A BAT analysis is included in a subsequent section of this submittal.

#### Subchapter D – Prevention of Significant Deterioration of Air Quality

Pennsylvania incorporates the Federal PSD regulations by reference at 25 Pa. Code §127.83. A discussion of PSD applicability with respect to the proposed project is included under the Federal requirements.

#### <u>Subchapter E – Nonattainment New Source Review (NNSR)</u>

Delaware County is currently classified as nonattainment with respect to the 2012 annual PM<sub>2.5</sub> NAAQS, and is managed as a severe nonattainment area with respect to the ozone eight (8)-hour NAAQS for permitting applicability purposes. Similar to the Federal PSD rules, under PADEP's NNSR rules a project must have both a significant emissions increase and a significant net emissions increase of the nonattainment pollutant or precursor pollutants to be a major modification. Table C-35 in Attachment C presents the results of the PADEP NNSR permitting applicability evaluation for ozone and PM<sub>2.5</sub>. The project related emissions increases are below the NNSR significance levels for nonattainment pollutants and precursors as determined in accordance with 25 Pa. Code §127.203a requirements. As a result, no further assessment is required.

Because the project results in a de minimis emission increase, Monroe must evaluate the proposed VOC and NO<sub>X</sub> emissions increases from the project and aggregate the project-related emissions increases with other increases and decreases of VOC and NO<sub>X</sub> which occurred within 10 years prior to the date of submission of a complete application. If the aggregated emissions increase meets or exceeds the emissions rate that is significant, only the emissions offset requirements in §127.205(3) (relating to special permit requirements) apply to the aggregated emissions increases.



Table C-36, in Attachment C, summarizes projects that have occurred at the refinery during the 10-year aggregation periods specified under 25 Pa. Code §127.203a that have resulted in net emissions increases in NO<sub>X</sub> and VOC. The net increases have been summed with the proposed ULSG project emissions in Table C-36 and the results demonstrate that the 10-year emission offset requirements of §127.205(3) for ozone NNSR requirements apply to the installation of the proposed ULSG project for NO<sub>X</sub>. Therefore, Monroe Energy intends to purchase 48 tpy of NO<sub>X</sub> emission reduction credits (which is an emission offset of 1.3 to 1 for the 10-year net emission increase of 36.62 tpy of NO<sub>X</sub>, rounded to a whole number) in order to comply with the applicable ozone NNSR regulations.

#### <u>Subchapter I – Plan Approval and Operating Permit Fees</u>

25 Pa. Code §127.702 specifies the fee required to submit an operating permit application for facilities. The proposed project will be subject to 25 Pa. Code Subchapter E (i.e., NSR) and Chapter 122 requirements (i.e., NSPS); therefore, a check for \$7,000.00 payable to the "Commonwealth of Pennsylvania - Clean Air Fund" has been provided to PADEP as part of this application.

#### **Chapter 129 – Standards for Sources**

VOC emission control standards for specific sources at petroleum refineries are addressed in 25 Pa. Code §129.55. The specific sources subject to §129.55 include wastewater separators, pumps and compressors, vacuum-producing systems and process units during turnarounds. The proposed fugitive equipment to be installed as part of the project will include pumps and compressors handling VOC with a vapor pressure greater than 1.5 psia at actual conditions. The proposed pumps and compressors that will be installed as part of the project will comply with applicable provisions of §129.55.

Standards for monitoring and repairing certain refinery components that have the potential to leak VOC are addressed in 25 Pa. Code §129.58. The proposed ULSG unit and cooling tower are not refinery components as defined in §121.1. Therefore these units will not be subject to §129.58.



Pursuant to §129.58, petroleum refineries must develop a monitoring plan for certain components with the potential to leak VOC emissions. Certain components of the ULSG unit will be subject to the requirements of a PADEP-approved monitoring plan. Compliance with 40 CFR Part 60, Subpart GGGa serves as compliance for §129.58. The new potential VOC fugitive emissions components will be incorporated in the Refinery's existing alternative monitoring plan and the Refinery will remain in compliance with applicable requirements of Subpart GGGa and §129.58.

The 2014 Proposed Additional RACT Requirements for Major Stationary Sources of NO<sub>X</sub> and VOC (RACT 2) will apply to various sources at the Monroe Refinery, including the proposed process heaters (H-01 and H-02) and the proposed new cooling tower when and if the rule is finalized. The proposed rule defines specific reasonably available control technology (RACT) limits for many types of emissions units (including process heaters) and specifies "presumptive" limits for others. It also includes provisions for "case-by-case" RACT analyses to be conducted in accordance with the existing RACT rules at §\$129.91 -129.95. Under the currently proposed RACT 2 rule, process heater H-01 (99.6 MMBtu/hr) would be subject to a NO<sub>X</sub> RACT standard of 0.25 lb NO<sub>X</sub>/MMBtu in accordance with proposed \$129.97(g)(1)(iv). Process heater H-02 (44.0 MMBtu/hr) would be subject to a "case-by-case" RACT analyses in accordance with proposed \$129.99(b). Both of the process heaters would be subject to the presumptive VOC RACT standard for combustion units or other combustion sources at proposed \$129.97(d). The proposed new cooling tower would be subject to a "case-by-case" RACT analyses in accordance with proposed \$129.99(c). Monroe will comply with the applicable portions of the RACT 2 rule when the proposed rule is finalized.

#### **Best Available Technology**

Pursuant to 25 Pa. Code §127.12(5), an application submitted for PADEP approval shall show that emissions from a new source, or a source which was constructed and commences operation on or after July 1, 1972, will be the minimum attainable through the use of best available technology (BAT).



#### **Proposed ULSG Unit Process Heaters**

#### NO<sub>X</sub> BAT

Monroe evaluated the following potential NO<sub>X</sub> control technologies:

#### • Flue Gas Recirculation (FGR)

FGR is the recirculation of cooled flue gas which acts as a heat sink and absorbs heat from the flame to reduce peak flame temperatures. When mixed with combustion air, the recirculated flue gas dilutes the oxygen content of combustion air and therefore reduces the formation of thermal NO<sub>X</sub>. Success with FGR on boilers demonstrates the capability of the technique. However, combustion air is supplied to the proposed ULSG unit process heaters by natural draft, and thus recirculation of flue gas is not technically feasible.

#### • Low NO<sub>X</sub> Burners (LNB)

LNB are front-end combustion controls for process heaters and boilers. LNB reduce emissions of thermal  $NO_X$  by lowering peak flame temperatures. LNB technology is feasible and the proposed new heaters will be equipped with Callidus LNB that are guaranteed no to exceed an emission rate of 0.035 lb/MMBtu on a 30-day rolling average basis.

#### • <u>Selective Non-Catalytic Reduction (SNCR)</u>

SNCR reduces NO<sub>X</sub> by reactions with ammonia. SNCR is only effective in a temperature window in the 1,600 °F to 1,800 °F range when adequate gas residence time is available. Monroe contacted the following SNCR vendors and provided them with the physical dimensions and operating conditions of the proposed ULSG unit process heaters: Fuel Tech, Inc., HAMON Corporation, and De-NO<sub>X</sub> Technologies, LLC. These vendors have advised Monroe that installation of SNCR on the proposed ULSG unit process heaters



would not be technically feasible due to inadequate temperature and residence time for NO<sub>X</sub> reduction by ammonia.

#### • <u>Selective Catalytic Reduction (SCR)</u>

SCR uses ammonia as a reagent and a catalyst to reduce  $NO_X$  emissions at an operating temperature near  $600^{\circ}F$ . SCR catalysts are composed of active metals or ceramics with a highly porous structure containing activated sites where the reduction reaction occurs. SCR requires a forced draft air flow to overcome the pressure drop imposed on the exhaust flow by the catalyst bed(s). As previously stated, the proposed new heaters are natural draft; therefore, the installation and operation of SCR is not technically feasible.

Monroe considers compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), the application of LNB and the proposed  $NO_X$  emission limit of 0.035 lb/MMBtu as BAT for  $NO_X$  emissions from the two (2) proposed ULSG unit process heaters.

#### Carbon Monoxide BAT

Monroe evaluated CO catalyst technology, use of FGR, proper operation, and good combustion and engineering practices, as potential CO control technologies. For the reasons stated above, FGR and catalyst technology are not technically feasible for the proposed ULSG unit process heaters. Monroe therefore considers compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), proper operation and good combustion and engineering practices as BAT for CO emissions from the two (2) proposed ULSG unit process heaters.

#### Volatile Organic Compounds BAT

Monroe evaluated VOC catalyst technology, use of FGR, proper operation, and good combustion and engineering practices, as potential VOC control technologies. As discussed above, Monroe considers the use of catalyst technology and FGR, to be technically infeasible for the two (2)



proposed process heaters. Monroe therefore considers BAT for VOC to be compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), proper design, operation and good combustion and engineering practices.

#### PM BAT

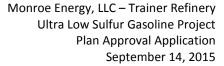
PM emissions associated with the use of gaseous fuels are primarily a result of incomplete fuel combustion. By carefully controlling the combustion process, PM emissions can be minimized. Monroe considers BAT for PM for the two (2) proposed process heaters to be compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), proper design, operation, and good combustion and engineering practices.

#### SO<sub>2</sub> BAT

During fuel combustion, SO<sub>2</sub> emissions result from the oxidation of sulfur contained in the fuels. Monroe will fire only refinery fuel gas in the proposed ULSG unit process heaters. Monroe considers BAT for SO<sub>2</sub> for the two (2) proposed process heaters to be compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning) and the firing of refinery fuel gas that meets the requirements of 40 CFR Part 60, Subpart Ja.

#### **Proposed Cooling Tower**

BAT for the proposed cooling tower was considered for both PM<sub>2.5</sub> and VOC. For PM<sub>2.5</sub>, the best available cooling tower control method that Monroe is aware of is high efficiency drift eliminator with a drift rate of 0.0005%. For VOC, monthly monitoring for leaks from heat exchangers is available. Monroe contacted the Louisiana Department of Environmental Quality (LDEQ) and the Texas Commission of Environmental Quality (TCEQ), two (2) states which have a large population of oil refineries, and confirmed that no other compliance methods have been used in these states. Monroe therefore considers a guaranteed drift rate of 0.0005% and leak monitoring to represent BAT for the proposed cooling tower. Monroe Energy proposes to install the cooling tower with a manufacturer guaranteed drift rate of 0.0005% and operate the cooling tower in





accordance with the manufacturer's specifications to minimize PM emissions. Monroe will also monitor the cooling tower monthly in accordance with 40 CFR Part 63, Subpart CC, and calculate monthly emissions using the methodology in the guidance developed by the Texas Commission of Environmental Quality (TCEQ), titled *Air Stripping Method (Modified El Paso Method) for Determination of Volatile Organic Compound Emissions from Water Sources*, Sampling Procedures Manual, Appendix P: Cooling Tower Monitoring Guidance.





## COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION

### **GENERAL INFORMATION FORM – AUTHORIZATION APPLICATION**

Before completing this General Information Form (GIF), read the step-by-step instructions provided in this application package. This version of the General Information Form (GIF) must be completed and returned with any program-specific application being submitted to the Department.

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	@monroe-energ	y.com								
	J		SITE	INFO	RMATI	ON				
DEP Site ID#	Site Name									
270501	Trainer Re	finerv								
	110046121807		d Nun	nber of	Employ	ees to be F	Present at	Site	~450	
Description of				<b></b>		,				
Petroleum Re										
County Name	•	Municipality					City	Boro	Twp	State
Delaware		Trainer								
<b>County Name</b>		Municipality					City	Boro	Twp	State
Site Location	Line 1			,	Site Loc	ation Line 2	2			
Trainer Refine	,									
	Last Line – City				State	ZIP+4			_	
Trainer					PA	19061				
	en Directions to		_	_			_			
	Coute 452 (Marke									
•	le to the Trainer	•	er @ V	/isitor's	s Entran	ce on Post	Road. Re	quest es	cort by	<i>'</i>
	l Dept. personn									
Site Contact L	ast Name			Name			MI		Su	ıffix
Torell			Matt							
Site Contact T				•	Site Con	tact Firm			_	
Environmenta										
Mailing Addre					_	Address Lir	ne 2			
Trainer Refine	erv				4101 Po	st Road				

Maili	ng Address Last Line – City		State	ZIP+4			
Trair	-		PA	19061			
Phor	ne Ext F	AX	Email A	Address			
		10-364-8614		rell@monro			
	S Codes (Two- & Three-Digit Codes -	List All That A	pply)		-Digit Code	(Optional)	
324				3	24110		
Clier OW/	t to Site Relationship						
OVVI	IOP	FACILITY	/ INICODM	IATION			
NA - 1	Continue Continue Footble	FACILIT	/ INFORM	IATION			<b>N</b> 1 -
	fication of Existing Facility	na facility o	votom or o	-4iv:i4v:2		Yes	No
1. 2.	Will this project modify an existi Will this project involve an addit	ng facility, s	ystem, or ac	ctivity?	r ootivity?		님
۷.	If "Yes", check all relevant facility t						
	Facility Type	DEP Fac II		acility Type	ation number	S Delow.	DEP Fac ID#
$\boxtimes$	Air Emission Plant	293037		ndustrial Mineral	s Mining Opera	tion	DLI TACID#
	Beneficial Use (water)	273037		aboratory Locat		-	
Ħ	Blasting Operation			and Recycling C		n _	
Ħ	Captive Hazardous Waste Operation			/lineDrainageTrr			
Ħ	Coal Ash Beneficial Use Operation	-		1unicipal Waste		-	
	Coal Mining Operation		<u> </u>	oil & Gas Encroa	chment Locatio	n _	
	Coal Pillar Location		<u> </u>	il & Gas Locatio	on	_	
	Commercial Hazardous Waste Operation		🗆 o	il & Gas Water	Poll Control Fac	cility	
	Dam Location			ublic Water Sup		<u>_</u>	
	Deep Mine Safety Operation -Anthracite			adiation Facility		_	
	Deep Mine Safety Operation -Bituminous			Residual Waste (	•	=	
님	Deep Mine Safety Operation -Ind Minerals			torage Tank Lo		_	
님	Encroachment Location (water, wetland)			Vater Pollution C	control Facility	-	
H	Erosion & Sediment Control Facility			Vater Resource Other:		=	
	Explosive Storage Location  Latitude/Longitude	1	Latitude	Milei.		Longitud	<u> </u>
	Latitude/Longitude		Lanuue			Longitud	e
	Point of Origin	Dograce	Minutos	Sacanda	Dograce	Minutos	Secondo
NDD	Point of Origin	Degrees	Minutes	Seconds	Degrees	Minutes	Seconds
	ES Discharge Point	39	Minutes 49	1	75	24	59
Horiz	ES Discharge Point contal Accuracy Measure	<b>39</b> Feet	49	1 or	<b>75</b> Me		59
Horiz	ES Discharge Point	Feet Nortl	49 n American I	<i>1</i> or Datum of 192	<b>75</b> Me	24	59
Horiz	ES Discharge Point contal Accuracy Measure	Feet North	n American I	or Datum of 192 Datum of 198	<b>75</b> Me 27 33	24	59
Horiz Horiz	ES Discharge Point zontal Accuracy Measure zontal Reference Datum Code	Feet Nortl Nortl Worl	n American I	<i>1</i> or Datum of 192	<b>75</b> Me 27 33	24	59
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Mailing Address Line 1 2393 Kimberton Road	I		Mailing Address Line 2 PO Box 299				
Address Last Line – C	tv		State	ZIP+4			
Kimberton	-,		PA		2-0299		
Phone	Ext	FAX	Email Address				
610-933-5246	113	610-933-5127	nlebo@all4inc.com				
Time Schedules	Project M	ilestone (Optional)					
	<del> </del>						
1. Have you info	med the	surrounding comm	unity and addressed a	nv 🖂	Yes	$\neg \neg$	No
		g the application to		iiy 🖂	103	Ш	140
		ate or federal grants			Yes		No
			ated to the grant and provide th	e grant so	ource, coi		erson
	expiration date						
	Project Relate	ed to Grant					
Grant Sou							
	ration Date:	authorization on Ar	pendix A of the Land U	so 🗆	Yes	$\boxtimes$	No
			A of the Land Use Poli		163		INO
attached to GIF i			A of the Land Ose Follows	o y			
		,	ect to the Land Use Policy.				
If "Yes" to	Question 3, th	ne application is subject	to this policy and the Applicant	should ar	swer the	additio	nal
questions	n the Land U	se Information section	<u>.                                      </u>				
		LAND USE I	NFORMATION				
Note: Applicants are el	ncouraged to	submit copies of loc	cal land use approvals or ot	her evide	ence of a	complia	ance with
local comprehensive pla							
		or multi-county com			Yes	$\boxtimes$	No
			al comprehensive plan?		Yes		No
			dinance, municipal zonir	ng 📙	Yes	$\boxtimes$	No
		I zoning ordinance?		54.45	_	. "	
Note: If the Application	cant answers	s "No" to either Questior leed to respond to ques	ns 1, 2 <u>or</u> 3, <u>the provisions of the trans 4 and 5 below</u>	ne PA MP	<u>∪ are no</u>	t applic	able and
			and 3, the Applicant should res	spond to a	uestions	4 and 5	below.
			of the zoning ordinance		Yes		No
			al? If zoning approval has be		-	_	
received, attach do	cumentation.		<b>.</b>				
5. Have you attach	ed Municipa	al and County Land	Use Letters for the project	?	Yes		No

#### **COORDINATION INFORMATION**

<u>Note</u>: The PA Historical and Museum Commission must be notified of proposed projects in accordance with DEP Technical Guidance Document 012-0700-001 and the accompanying Cultural Resource Notice Form.

If the activity will be a mining project (i.e., mining of coal or industrial minerals, coal refuse disposal and/or the operation of a coal or industrial minerals preparation/processing facility), respond to questions 1.0 through 2.5 below.

If the activity will not be a mining project, skip questions 1.0 through 2.5 and begin with question 3.0. Is this a coal mining project? If "Yes", respond to 1.1-1.6. If "No", skip to  $\boxtimes$ No Question 2.0. 1.1 Will this coal mining project involve coal preparation/ processing Yes П No activities in which the total amount of coal prepared/processed will be equal to or greater than 200 tons/day? Will this coal mining project involve coal preparation/ processing 1.2 Yes П No activities in which the total amount of coal prepared/processed will be greater than 50,000 tons/year? Will this coal mining project involve coal preparation/ processing 1.3 Yes No activities in which thermal coal dryers or pneumatic coal cleaners will be used? 1.4 For this coal mining project, will sewage treatment facilities be Yes No constructed and treated waste water discharged to surface waters? 1.5 Will this coal mining project involve the construction of a permanent Yes No impoundment meeting one or more of the following criteria: (1) a contributory drainage area exceeding 100 acres; (2) a depth of water measured by the upstream toe of the dam at maximum storage elevation exceeding 15 feet; (3) an impounding capacity at maximum storage elevation exceeding 50 acre-feet? Will this coal mining project involve underground coal mining to be 1.6 Yes П No conducted within 500 feet of an oil or gas well? Is this a non-coal (industrial minerals) mining project? If "Yes", respond 2.0 Yes  $\boxtimes$ No to 2.1-2.6. If "No", skip to Question 3.0. Will this non-coal (industrial minerals) mining project involve the 2.1 Yes No crushing and screening of non-coal minerals other than sand and gravel? 2.2 Will this non-coal (industrial minerals) mining project involve the Yes No crushing and/or screening of sand and gravel with the exception of wet sand and gravel operations (screening only) and dry sand and gravel operations with a capacity of less than 150 tons/hour of unconsolidated materials? 2.3 Will this non-coal (industrial minerals) mining project involve the Yes No construction, operation and/or modification of a portable non-metallic (i.e., non-coal) minerals processing plant under the authority of the General Permit for Portable Non-metallic Mineral Processing Plants (i.e., BAQ-PGPA/GP-3)? Yes 2.4 For this non-coal (industrial minerals) mining project, will sewage П No treatment facilities be constructed and treated waste water discharged to surface waters? 2.5 Will this non-coal (industrial minerals) mining project involve the Yes No construction of a permanent impoundment meeting one or more of the following criteria: (1) a contributory drainage area exceeding 100 acres; (2) a depth of water measured by the upstream toe of the dam at maximum storage elevation exceeding 15 feet; (3) an impounding capacity at maximum storage elevation exceeding 50 acre-feet? 3.0 Will your project, activity, or authorization have anything to do with a Yes  $\bowtie$ No well related to oil or gas production, have construction within 200 feet of, affect an oil or gas well, involve the waste from such a well, or string power lines above an oil or gas well? If "Yes", respond to 3.1-3.3. If "No", skip to Question 4.0.

3.1	Does the oil- or gas-related project involve any of the following: placement of fill, excavation within or placement of a structure, located in, along, across or projecting into a watercourse, floodway or body of water (including wetlands)?	Yes		No
3.2	Will the oil- or gas-related project involve discharge of industrial wastewater or stormwater to a dry swale, surface water, ground water or an existing sanitary sewer system or storm water system? If "Yes", discuss in <i>Project Description</i> .	Yes		No
3.3	Will the oil- or gas-related project involve the construction and operation of industrial waste treatment facilities?	Yes		No
4.0	Will the project involve a construction activity that results in earth disturbance? If "Yes", specify the total disturbed acreage.  4.0.1 Total Disturbed Acreage ~1.4 acres	Yes		No
5.0	Does the project involve any of the following? If "Yes", respond to 5.1-5.3. If "No", skip to Question 6.0.	Yes	$\boxtimes$	No
5.1	Water Obstruction and Encroachment Projects – Does the project involve any of the following: placement of fill, excavation within or placement of a structure, located in, along, across or projecting into a watercourse, floodway or body of water?	Yes		No
5.2	Wetland Impacts – Does the project involve any of the following: placement of fill, excavation within or placement of a structure, located in, along, across or projecting into a wetland?	Yes		No
5.3	Floodplain Projects by the commonwealth, a Political Subdivision of the commonwealth or a Public Utility – Does the project involve any of the following: placement of fill, excavation within or placement of a structure, located in, along, across or projecting into a floodplain?	Yes		No
6.0	Will the project involve discharge of stormwater or wastewater from an industrial activity to a dry swale, surface water, ground water or an existing sanitary sewer system or separate storm water system?	Yes		No
7.0	Will the project involve the construction and operation of industrial waste treatment facilities?	Yes		No
8.0	Will the project involve construction of sewage treatment facilities, sanitary sewers, or sewage pumping stations? If "Yes", indicate estimated proposed flow (gal/day). Also, discuss the sanitary sewer pipe sizes and the number of pumping stations/treatment facilities/name of downstream sewage facilities in the <i>Project Description</i> , where applicable.  8.0.1 Estimated Proposed Flow (gal/day)	Yes		No
9.0	Will the project involve the subdivision of land, or the generation of 800 gpd or more of sewage on an existing parcel of land or the generation of an additional 400 gpd of sewage on an already-developed parcel, or the generation of 800 gpd or more of industrial wastewater that would be discharged to an existing sanitary sewer system?	Yes		No
	9.0.1 Was Act 537 sewage facilities planning submitted and approved by DEP? If "Yes" attach the approval letter. Approval required prior to 105/NPDES approval.	Yes		No
10.0	Is this project for the beneficial use of biosolids for land application within Pennsylvania? If "Yes" indicate how much (i.e. gallons or dry tons per year).  10.0.1 Gallons Per Year (residential septage)  10.0.2 Dry Tons Per Year (biosolids)	Yes		No
11.0	Does the project involve construction, modification or removal of a dam?  If "Yes", identify the dam.  11.0.1 Dam Name	Yes		No
12.0	Will the project interfere with the flow from, or otherwise impact, a dam? If "Yes", identify the dam.  12.0.1 Dam Name	Yes		No

13.0	Will the project involve operations (excluding during the construction ☐ Yes ☐ No period) that produce air emissions (i.e., NOX, VOC, etc.)? If "Yes", identify each type of emission followed by the amount of that emission.  13.0.1 Enter all types & amounts Please refer to the Plan Approval Application letter of emissions; separate accompanying this submittal. each set with semicolons.							
14.0	Does the project include the construction or modification of a drinking water supply to serve 15 or more connections or 25 or more people, at least 60 days out of the year? If "Yes", check all proposed sub-facilities.  14.0.1 Number of Persons Served		Yes		No			
	14.0.2 Number of Employee/Guests							
	14.0.3 Number of Connections							
	14.0.4 Sub-Fac: Distribution System		Yes		No			
	14.0.5 Sub-Fac: Water Treatment Plant		Yes		No			
	14.0.6 Sub-Fac: Source		Yes		No			
	14.0.7 Sub-Fac: Pump Station		Yes		No			
	14.0.8 Sub Fac: Transmission Main		Yes		No			
	14.0.9 Sub-Fac: Storage Facility	<u> </u>	Yes		No			
15.0	Will your project include infiltration of storm water or waste water to ground water within one-half mile of a public water supply well, spring or infiltration gallery?	Ш	Yes		No			
16.0	Is your project to be served by an existing public water supply? If "Yes", indicate name of supplier and attach letter from supplier stating that it will serve the project.		Yes		No			
	16.0.1 Supplier's Name Chester Water Authority							
	16.0.2 Letter of Approval from Supplier is Attached	$\boxtimes$	Yes		No			
17.0	Will this project involve a new or increased drinking water withdrawal from a stream or other water body? If "Yes", should reference both Water		Yes		No			
	Supply and Watershed Management.  17.0.1 Stream Name							
18.0	Will the construction or operation of this project involve treatment, storage, reuse, or disposal of waste? If "Yes", indicate what type (i.e.,		Yes		No			
	hazardous, municipal (including infectious & chemotherapeutic), residual) and the amount to be treated, stored, re-used or disposed.  18.0.1 Type & Amount							
19.0	Will your project involve the removal of coal, minerals, etc. as part of any earth disturbance activities?		Yes		No			
20.0	Does your project involve installation of a field constructed underground		Yes	$\boxtimes$	No			
	storage tank? If "Yes", list each Substance & its Capacity. Note: Applicant							
	may need a Storage Tank Site Specific Installation Permit.							
	20.0.1 Enter all substances &							
	capacity of each; separate each set with semicolons.							
21.0	Does your project involve installation of an aboveground storage tank	П	Yes	$\boxtimes$	No			
	greater than 21,000 gallons capacity at an existing facility? If "Yes", list			_				
	each Substance & its Capacity. Note: Applicant may need a Storage Tank							
	Site Specific Installation Permit.							
	21.0.1 Enter all substances &							
	capacity of each; separate							
22.0	each set with semicolons.		Yes	$\boxtimes$	No			
22.0	Does your project involve installation of a tank greater than 1,100 gallons which will contain a highly hazardous substance as defined in DEP's Regulated Substances List, 2570-BK-DEP2724? If "Yes", list each Substance & its Capacity. Note: Applicant may need a Storage Tank Site Specific Installation Permit.		res		INO			
	22.0.1 Enter all substances &							
	capacity of each; separate each set with semicolons.							

23.0 Does your project involve installation of a storage tank at a new facility Yes  $\boxtimes$ No with a total AST capacity greater than 21,000 gallons? If "Yes", list each Substance & its Capacity. Note: Applicant may need a Storage Tank Site Specific Installation Permit. 23.0.1 Enter all substances & capacity of each; separate each set with semicolons. 24.0 Will the intended activity involve the use of a radiation source? Yes  $\boxtimes$ No CERTIFICATION I certify that I have the authority to submit this application on behalf of the applicant named herein and that the information provided in this application is true and correct to the best of my knowledge and information. Type or Print Name Jeffrey K. Warmann CEO and President Signatu Title

1300-PM-BIT0001 5/2012

#### Chetkowski, David

Subject:FW: City Water Use at Monroe EnergyAttachments:Meters - addl cooling towers june\_2014.xlsx

From: Brian P. Mac Ewen [mailto:bpmacewen@chesterwater.com]

Sent: Wednesday, June 11, 2014 9:53 AM

To: Kofeldt, Frank; Edwards, David

**Cc:** Thomas A. Zetusky, Sr.; Thomas Moore **Subject:** RE: City Water Use at Monroe Energy

Frank – we have reviewed the current meters at the four locations nearest the proposed cooling towers and we offer the following for your information.

Each of the four meters has available additional capacity that in combination can supply the additional 3.815 MGD of use for the proposed three cooling towers. You will have to determine if your internal distribution piping can handle the additional flows.

The attached spreadsheet summarizes the four meter locations and also lists the 2014 average daily consumption (ADC) – these ADC values are in-line with the figures you provided from the October 2012 to October 2013 period.

For example, the C-3 Gate meter (#N62708266) has a continuous operating range of 30 - 2000 GPM, with intermittent max flows up to 2,500 GPM. The 2014 ADC for this site has been 673,000 GPD, which equates to an <u>average</u> usage of 467 GPM. Depending on your internal piping arrangement, I'm assuming this C-3 Gate meter would primarily feed the Cooling Tower #3 demand of 1.8 MGD (1,260 GPM). So the 2014 average usage of 467 GPM <u>plus</u> the average cooling tower usage of 1,260 GPM equals 1,727 GPM, which is within the existing meter's operating range. As long as your maximum instantaneous flows are within each meter's capability, it shouldn't be an issue.

The same analysis can be done for the other three meter sites as I'm assuming your internal piping layout would allow for a combined feed from these three meters to the proposed cooling towers #1 and #2.

If you would like to meet to review this meter capacity info in detail, let me know. There would be <u>no</u> additional capacity fees due as long as the meter sizes are not changed – just the additional usage fees at our standard rates.

Also, the CWA is considering a modernization program to change out these meters to our current meters (same size) that have a slightly larger flow capacity and more data logging capability (min, max flows, etc). Our Business Office will be in contact regarding this possible meter change out program.

If you have any questions, let me know.

Brian P. MacEwen, P.E. Director of Engineering Chester Water Authority P.O. Box 467

Chester, PA 19016-0467 610-876-8185 x-1218 610-499-5993 (fax) bpmacewen@chesterwater.com

From: Kofeldt, Frank [mailto:frank.kofeldt@monroe-energy.com]

**Sent:** Tuesday, June 03, 2014 2:18 PM **To:** Brian P. Mac Ewen; Edwards, David **Cc:** Steven C. Farney; Keith M. Johnston

Subject: RE: City Water Use at Monroe Energy

Brian,

#### Thanks for the feedback.

From: Brian P. Mac Ewen [mailto:bpmacewen@chesterwater.com]

Sent: Tuesday, June 03, 2014 1:34 PM
To: Kofeldt, Frank; Edwards, David
Cc: Steven C. Farney; Keith M. Johnston
Subject: RE: City Water Use at Monroe Energy

FYI- Patrick Martin is no longer with CWA, but we will respond to your request shortly.

Brian P. MacEwen, P.E. Director of Engineering Chester Water Authority P.O. Box 467 Chester, PA 19016-0467 610-876-8185 x-1218 610-499-5993 (fax) bpmacewen@chesterwater.com

**From:** Kofeldt, Frank [mailto:frank.kofeldt@monroe-energy.com]

Sent: Monday, June 02, 2014 8:53 AM

**To:** Engineer **Cc:** Edwards, David

Subject: City Water Use at Monroe Energy

Patrick,

Would it be possible to send an email or letter to confirm that Chester Water Authority will be able to supply the refinery with the additional water we discussed previously. I attached the email Jagwinder Singh sent you. The additional use would be 3,815,000 per day (2649 gpm). We need the confirmation to proceed with our environmental permit.

The meter changes you suggested will be done as a part of the project.

Thanks,

Frank Kofeldt Monroe Energy Trainer Refinery 610-364-8072

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3



#### COMMONWEALTH OF PENNSYLVANIA DEPARTMENT OF ENVIRONMENTAL PROTECTION BUREAU OF AIR QUALITY

## **PROCESSES**

# Application for Plan Approval to Construct, Modify or Reactivate an Air Contamination Source and/or Install an Air Cleaning Device

This application must be submitted with the General Information Form (GIF).

Before completing this form, read the instructions provided for the form.

Section A	- Facility Name, Checklis	t And Certification
Organization Name or Registered Fictiti	ous Name/Facility Name: Monro	pe Energy, LLC – Trainer Refinery
DEP Client ID# (if known): 296139	P. Dan John Jan S. S. Salas J.	and the second second
Type of Review required and Fees:		
	NSPS, NESHAPs, MACT, NSR	
Source requiring approval under	er NSPS or NESHAPS or both:	\$ <u>1,700</u>
Source requiring approval under	nent of a MACT limitation:	\$ <u>5,300</u>
Source requiring approval under	er PSD:	\$
	Applicant's Checkl	ist
Check the following li	st to make sure that all the rec	quired documents are included.
⊠ General Information Form (	GIF)	
Processes Plan Approval A	pplication	
Compliance Review Form facilities submitting on a perior	or provide reference of most odic basis: <u>5/14/2015</u>	recently submitted compliance review form for
	and Municipal Notifications	
□ Permit Fees		MARKET AND THE
Addendum A: Source Appli	cable Requirements (only applic	able to existing Title V facility)
Certification of Truth.	Accuracy and Completer	ness by a Responsible Official
or modern or reading	Accuracy and complete.	less by a responsible Official
I, Jeffrey K. Warmann	. certify under penalty	of law in 18 Pa. C. S. A. §4904, and
35 P.S. §4009(b) (2) that based on info	rmation and belief formed after r	easonable inquiry, the statements and information
in this application are true applicate and	complete.	1 1
/////		9/14/2015
(Signature):	Date:	
Name (Print): <u>Jeffrey K. Warmann</u>	Title: <u>C</u>	CEO and President
1.9	OFFICIAL USE ONLY	
Application No.	Unit ID	Site ID AUTH, ID
DEP Client ID #:	APS. ID	AUTH. ID
Date Received	Date Assigned	Reviewed By
Date of 1st Technical Deficiency Comments:		of 2 <sup>nd</sup> Technical Deficiency
Comments.		

#### **Section B - Processes Information**

#### 1. Source Information

Source Description (give type, use, raw materials, product, etc). Attach additional sheets as necessary.

Cooling Tower with two (2) cells for cooling of reactor effluent stream and the ULSG product cooler.

Manufacturer Cooling Tower Depot	Model No. N/A	Number of Sources 1
Source Designation	Maximum Capacity	Rated Capacity
ULSG Cooling Tower	10,200 gpm	10,200 gpm

Type of Material Processed

Cooling water

#### **Maximum Operating Schedule**

Hours/Day	Days/Week	Days/Year	Hours/Year
24	7	365	8,760

Operational restrictions existing or requested, if any (e.g., bottlenecks or voluntary restrictions to limit PTE)

Capacity (specify units)

Per Hour Per Day Per Week Per Year

**Operating Schedule** 

Hours/Day Days/Week Days/Year Hours/Year **24** 7 **365 8,760**Seasonal variations (Months) From **N/A** to

If variations exist, describe them

N/A

2. Fuel – N/A					
Туре	Quantity Hourly	Annually	Sulfur	% Ash (Weight)	BTU Content
Oil Number	GPH @ 60°F	X 10 <sup>3</sup> Gal	% by wt		Btu/Gal. & Lbs./Gal. @ 60 °F
Oil Number	GPH @ 60°F	X 10 <sup>3</sup> Gal	% by wt		Btu/Gal. & Lbs./Gal. @ 60 °F
Natural Gas	SCFH	X 10 <sup>6</sup> SCF	grain/100 SCF		Btu/SCF
Gas (other)	SCFH	X 10 <sup>6</sup> SCF	grain/100 SCF		Btu/SCF
Coal	TPH	Tons	% by wt		Btu/lb
Other *					
*Note: Describe ar	nd furnish information	separately for oth	er fuels in Addendur	n B.	

Section B - Processes Information (Continued)						
3. Burner – N/A						
Manufacturer	Type and N	lodel No.			Number of Burners	
Description:	I			l		
Rated Capacity		Maximum C	apacity			
4. Process Storage Vessels – N/A						
A. For Liquids:						
Name of material stored						
Tank I.D. No.	Manufacturer			Date Instal	led	
Maximum Pressure		Capacity	(gallons/M	eter³)		
Type of relief device (pressure set vent/ce	onservation vent/	emergency v	ent/open ve	ent)		
Relief valve/vent set pressure (psig)		Vapor pr	Vapor press. of liquid at storage temp. (psia/kPa)			
Type of Roof: Describe:						
Total Throughput Per Year		Number of fills per day (fill/day): Filling Rate (gal./min.): Duration of fill hr./fill):				
B. For Solids – N/A				,		
Type: Silo Storage Bin Other	, Describe	Name of	Material St	ored		
Silo/Storage Bin I.D. No.	Manufacturer	·		Date Instal	led	
State whether the material will be stored	in loose or bags i	n silos	Capacity	(Tons)		
Turn over per year in tons		Turn over per day in tons				
Describe fugitive dust control system for	loading and hand	lling operation	ns			
Describe material handling system						
5. Request for Confidentiality						
Do you request any information on this ap					∕es ⊠ No ed "confidential".	

## **Section B - Processes Information (Continued)**

#### **Miscellaneous Information**

Attach flow diagram of process giving all (gaseous, liquid and solid) flow rates. Also, list all raw materials charged to

process equipment, and the amounts charged (tons/hour, etc.) at rated capacit charges describing fully expected variations in production rates). Indicate (on dicontrolled (location of water sprays, collection hoods, or other pickup points, edesign, airflow and capture efficiency. Describe any restriction requested and how the approach of the approa	agram) all points where contaminants are etc.). Describe collection hoods location,
Describe fully the facilities provided to monitor and to record process operating of air contaminants. Show that they are reasonable and adequate.  See Attachment B, Addendum A and Addendum 1.	conditions, which may affect the emission
Describe each proposed modification to an existing source.  N/A	
Identify and describe all fugitive emission points, all relief and emergency valves at N/A	nd any by-pass stacks.
Describe how emissions will be minimized especially during start up, shut down, properties of the design of each cooling tower of drift droplets formed within the cooling tower system.	· · · · · · · · · · · · · · · · · · ·
Anticipated Milestones:  i. Expected commencement date of construction/reconstruction/installation:  ii. Expected completion date of construction/reconstruction/installation:  iii. Anticipated date of start-up:	2Q2016 2Q2017 2Q2017

	S	ection C - Air (	Cleaning Device					
1. Precontrol Emis	sions* – <i>Not Availa</i>	ble						
		Calculation/						
Pollutant	Specify Units	Pounds/Hou	r Hours/Year	Tons/Year	Estimation Method			
PM	Opcony onits	1 Garas/11Gar	Tiodis/Todi	10113/1Cui	Metriou			
PM <sub>10</sub>								
SO <sub>x</sub>								
CO								
NOx								
VOC								
Others: (e.g., HAPs)								
* These emissions mu schedule for maximu values were determir	ım limits or restricted	d hours of operati	sted operating schedul on and/or restricted the					
2. Gas Cooling – N	I/A							
Water quenching	Yes 🗌 No	Water injection ra	ate	GPM				
Radiation and convection	on cooling		Air dilution	Yes 🗌 No				
☐ Yes ☐ No			If yes,CFM					
Forced Draft  Yes	s □ No		Water cooled duct wo	ork 🗌 Yes 🗀	] No			
Other								
Interest of the second	AOEN4		O that Male are	AOEN4				
Inlet Volume			Outlet Volume					
@°F	% Moisture		@°F	% Moisture				
Describe the system in	detail.							

Section C - Air Cleaning Device (Continued)								
3. Settling Chambers – A	/A							
Manufacturer		Volume of gas handledACF		Gas velocity	Gas velocity (ft/sec.)			
Length of chamber (ft.)	Width	of chamber (ft.)	Height of chamb	er (ft.)	Number of trays			
Water injection	No		Water injection r	ate (GPM)				
<b>Emissions Data</b>		,						
Inlet		Ou	tlet	R	Removal Efficiency (%)			
4. Inertial and Cyclone C	ollectors	s – <i>N/A</i>						
Manufacturer		Туре		Model N	0.			
Pressure drop (in. of water)		Inlet volume			Outlet volumeACFM @°F			
Number of individual cyclone(		Outlet straightening vanes used?  ☐ Yes ☐ No		ed?				
Length of Cyclone(s) Cylinder	(ft.)	Diameter of Cyclon	Diameter of Cyclone(s) Cylinder (ft.)		of Cyclone(s) cone (ft.)			
Inlet Diameter (ft.) or duct area	a (ft.²) of	cyclone(s)	clone(s) Outlet Diameter (ft.) or duct area (ft.²) of cyclone(s)					
If a multi-clone or multi-tube u	nit is inst	talled, will any of the ind	lividual cyclones o	r cyclone tub	es be blanked or blocked off?			
Describe any exhaust gas rec	irculation	n loop to be employed.						
Attach particle size efficiency curve								
<b>Emissions Data</b>								
Inlet		Ou	tlet	R	Removal Efficiency (%)			

Section C - Air Cleaning Device (Continued)									
5. Fabric Collector – N/A									
Equipment Specifications									
Manufacturer		Мо	del No.		Pressurized Design Suction Design				
Number of Compartments	N	Number of Filters Per Compartment   Is Baghouse Insulated?   Yes   No							
Can each compartment be isolated for repairs and/or filter replacement?									
Are temperature controls provided? (Describe in detail)									
Dew point at maximum moiste	ure	°F	Design inlet volume_		SCFM				
Type of Fabric  Material  Weight  Thickness	_ oz/sq.yd	☐ Felted ☐ Membrane ☐ Woven ☐ Others: List: ☐ Felted-Woven							
Fabric permeability (clean) @	½" water-∆ P		CFM/sq.ft.						
Filter dimensions Length_		Diameter/\	Width						
Effective area per filter Maximum operating temperature (°F)									
Effective air to cloth ratio Minimum Maximum									
Drawing of Fabric Filter A sketch of the fabric filter and temperature indicator s	showing all ac	cess doors, catwal							
Operation and Cleaning									
Volume of gases handled ACFM @	°F		ross collector (in. of v ipment to be used to	,	oressure drop.				
Type of filter cleaning  Manual Cleaning  Mechanical Shakers Pneumatic Shakers  Describe the equipment provi		Bag Collapse Sonic Cleaning Reverse Air Flow		Reverse Other:					
Describe the equipment provi	dod ii diy oli li	cc all is required to	or concetor operation						
Cleaning Initiated By  Timer Frequency if timer actuated  Expected pressure drop range in. of water Other Specify									
Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If yes, describe.									
Describe the warning/alarm system that protects against operation when the unit is not meeting design requirements.									
<b>Emissions Data</b>									
Pollutant	_	Inlet	Outlet	Re	emoval Efficiency (%)				
	1		I	I					

Section C - Air Cleaning Device (Continued)								
6. Wet Collection Equ	ipment – N/A							
Equipment Specification	S							
Manufacturer		Туре		Model No.				
Design Inlet Volume (SCF	M)		Relative Particulate/Gas	Velocity (eje	ector scrubbers only)			
Describe the internal features (e.g., variable throat, gas/liquid diffusion plates, spray nozzles, liquid redistributors, bed limiters, etc.).								
Describe pH monitoring ar	nd pH adjustme	nt systems, if ap	plicable.					
Describe mist eliminator o	r separator (typ	e, configuration,	backflush capability, freq	luency).				
Attach particulate size efficiency curve.								
Operating Parameters								
Inlet volume of gases handled(ACFM) Outlet volume of gases handled(ACFM)								
	@	°F	@	_ °F	% Moisture			
recirculating solution, mak	eup water, blee	ed flow, etc.)			er (e.g., quenching section,			
Describe scrubber liquid supply system (amount of make-up and recirculating liquid, capacity of recirculating liquid system, etc.)								
State pressure drop range (in water) across scrubber (e.g., venturi throat, packed bed, etc.) only. Describe the equipment provide to measure the pressure drop. Do not include duct or de-mister losses.								
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.								
Emissions Data								
Pollutant Inlet Outlet Removal Efficiency (%)								

Section C - Air Cleaning Device (Continued)								
7. Electrostatic Precip	oitator – <i>N/A</i>							
<b>Equipment Specification</b>	S							
Manufacturer		Model No.			☐ Wet	e-Stage	☐ Dry ☐ Two-Stage	
Gas distribution grids	Yes No			esign Inlet Volume (SC aximum operating tem	,			
Total collecting surface are	ea	sq. ft. Co	ollect	tor plates size length_		ft. x width_	ft.	
Number of fields		Nι	ımbe	er of collector plates/fie	eld			
Spacing between collector	plates	inche	s.					
Maximum gas velocity	f	t./sec. Mi	nimu	um gas treatment time	:	sec.		
Total discharge electrode l Number of discharge elect			ımbe	er of collecting electrod	de rappers			
Rapper control	Magnetic	☐ Pneumatic		Other		[	Describe in detail	
Operating Parameters	Operating Parameters							
Inlet gas temperature (°F) State pressure drop range (inches water gauge) acros								
Outlet gas temperature (°I	F)	_		collector only  Describe the equiprocessing t				
Volume of gas handled (A	CFM)	_	Dust resistivity (ohm-cm). Will resistivity vary?					
Power requirements				1				
Number and size of Transf	ormer Rectifier	sets by electric	cal fi	eld				
Field No.	No. of S	-		ch Transformer KVA	KV Ave.	Each Ro /Peak	ectifier Ma DC	
Current Density  Micro ampe	res/ft².	Corona Power   Corona Power Density   Watts/1000 ACFM   Watts/ft².					· ·	
Will a flue gas conditioning	system be em	ployed? If yes	, des	scribe it.				
Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If yes, describe.								
Describe the warning/alarn	n system that p	rotects against	ope	eration when unit is no	t meeting o	design requ	irements.	
Emissions Data						·		
Pollutant	I	nlet		Outlet		Remov	al Efficiency (%)	

Section C - Air Cleaning Device (Continued)						
8. Adsorption Equipm	nent – <i>N/A</i>					
<b>Equipment Specification</b>	s					
Manufacturer	Туре			Model No.		
Design Inlet Volume (SCF	M)	Adsorber	nt charge per adsorber	r vessel and number of adsorber vessels		
Length of Mass Transfer Z	one (MTZ), supplied b	y the manuf	acturer based upon la	aboratory data.		
Adsorber diameter (ft.) and	d area ft <sup>2</sup> .)		Adsorption bed dep	oth (ft.)		
Adsorbent information						
Adsorbent type and physic	al properties.					
Working capacity of adsor	bent (%)			Heel percent or unrecoverable solvent weight % in the adsorbent after regeneration.		
Operating Parameters						
Inlet volume of gases han	dled (AC	CFM) @	°F			
Adsorption time per adsorp	otion bed		Breakthrough capa Lbs. of solvent / 10	ocity: 0 lbs. of adsorbent =		
Vapor pressure of solvents	at the inlet temperatu	re	Available steam in pounds to regenerate carbon adsorber (if applicable)			
Percent relative saturation	of each solvent at the	inlet temper	rature			
Attach any additional data including auxiliary equipment and operation details to thoroughly evaluate the control equipment.						
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.						
Emissions Data						
Pollutant	Inlet		Outlet	Removal Efficiency (%)		

Section C - Air Cleaning Device (Continued)								
9. Absorption Equipment – <i>N/A</i>								
Equipment Specifications								
Manufacturer		Туре			Model No	).		
Design Inlet Volume (SCF	M)		To	wer height (ft.) and	inside d	iameter (ft.)		
Packing type and size (if a	pplicable)		He	ight of packing (ft.)	(if applic	cable)		
Number of trays (if applica	ble)		Nu	mber of bubble cap	os (if app	olicable)		
Configuration  Counter-curren	ıt [	Cross flow		Cocurrent flow				
Describe pH and/or other monitoring and controls.								
Absorbent information								
Absorbent type and conce	ntration.		Re	tention time (sec.)				
Attach equilibrium data for	absorption (if a	applicable)	•					
						ply system (once through or e flow rates for makeup, bleed		
Operating Parameters								
Volume of gas handled (A	CFM) Inle	et temperature (°F)		Pressure drop (in. of water) and liquid flow rate.  Describe the monitoring equipment.				
State operating range for p	H and/or abso	orbent concentration	n in sci	rubber liquid.				
Describe the warning/alarr	n system that p	protects against op	eration	when unit is not n	neeting d	lesign requirements.		
Emissions Data								
Pollutant	ı	Inlet		Outlet		Removal Efficiency (%)		

Section C - Air Cleaning Device (Continued)									
10. Selective Cataly	ytic Reduction	(SCR) - <i>N/A</i>							
	•	ction (SNCR) – <i>N</i>							
Non-Selective Catalytic Reduction (NSCR) – N/A									
Equipment Specifications									
Manufacturer		Type Model No.							
Design Inlet Volume (SCF	M)		Design operating te	mperature	(°F)				
Is the system equipped with process controls for proper mixing/control of the reducing agent in gas stream? If yes, give details.									
Attach efficiency and other pertinent information (e.g., ammonia slip)									
<b>Operating Parameters</b>									
Volume of gases handled (ACFM) @ °F									
Operating temperature rai	nge for the SCF	R/SNCR/NSCR sy	stem (°F) From		°F To°F				
Reducing agent used, if ar	ny		Oxidation catalyst u	sed, if any					
State expected range of us	sage rate and c	oncentration.	,						
Service life of catalyst			Ammonia slip (ppm	Ammonia slip (ppm)					
Describe fully with a sketch giving locations of equipment, controls systems, important parameters and method of operation.									
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.									
<b>Emissions Data</b>									
Pollutant	l	nlet	Outlet		Removal Efficiency (%)				

Section C - Air Cleaning Device (Continued)									
11. Oxidizer/Afterburners – <i>N/A</i>									
Equipment Specifications									
Manufacturer		Type □ <sup>-</sup>	Thermal	☐ Catalytic	Model No.				
Design Inlet Volume (SCF	M)	Combustion chamber vol		,	ength, cross-sectional area, effective				
Describe design features, which will ensure mixing in combustion chamber.									
Describe method of preapplicable).	heating incom	ning gases (		ribe heat exchar cable).	ger system used for heat recovery (if				
Catalyst used	ed Life of catalyst		•	temperature rise talyst (°F)	Dimensions of bed (in inches).  Height:  Diameter or Width:  Depth:				
Are temperature sensing devices being provided to measure the temperature rise across the catalyst?   Yes  No  If yes, describe.									
Describe any temperature or sketch.	sensing and/or	recording dev	vices (incl	uding specific loc	ation of temperature probe in a drawing				
Burner Information									
Burner Manufacturer		Model No.	0.		Fuel Used				
Number and capacity of bu	ırners	Rated capac	city (each) Maximum capacity (each)						
Describe the operation of t	he burner		Attac	Attach dimensioned diagram of afterburner					
Operating Parameters									
Inlet flow rate (ACFM)	@	°F	Outle	t flow rate (ACFN	1)°F				
State pressure drop range across catalytic bed (in. of water).				Describe the method adopted for regeneration or disposal of the used catalyst.					
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.									
Emissions Data									
Pollutant	<u> </u>	nlet		Outlet	Removal Efficiency (%)				

Section C - Air Cleaning Device (Continued)								
12. Flares – <i>N/A</i>								
Equipment Specification	S							
Manufacturer			vated flare ner	☐ Grou		Model No.		
Design Volume (SCFM)		Dimensions of Diameter_		Height				
Residence time (sec.) and temperature (°F)	outlet	Turn down ration	)		Burner details			
Describe the flare design (air/steam-assisted or nonassisted), essential auxiliaries including pilot flame monitor of proposed flare with a sketch.								
Describe the operation of the flare's ignition system.								
Describe the provisions to	introduce auxi	liary fuel to the fla	re.					
Operation Parameters								
Detailed composition of the	ne waste gas	Heat content	Exit velo		Exit velocity	velocity		
Maximum and average ga	Maximum and average gas flow burned (ACFM)  Operating temperature (°F)							
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.								
<b>Emissions Data</b>								
Pollutant		Inlet		Outlet	Removal Ef	ficiency (%)		

	Section	n C - Air Cleaı	ning Device (Continu	ued)			
13. Other Control Equi	pment						
Equipment Specification	s						
Manufacturer Cooling Tower Depot or	equivalent	Type Cellular PVC Di Equivalent		Model No. <b>N/A</b>			
Design Volume (SCFM) ~1,000,000 scfm per cell			Capacity <b>N/A</b>				
Describe pH monitoring ar	nd pH adjustme	nt, if any.					
Indicate the liquid flow rate	e and describe e	equipment provide	d to measure pressure di	lrop and flow rate, if any.			
Attach efficiency curve and/or other efficiency information.  N/A							
Attach any additional date including auxiliary equipment and operation details to thoroughly evaluate the control equipment.  N/A							
Operation Parameters							
Volume of gas handled							
~1,000,000 (per cell)	ACFM @ <u>am</u>	<u>ıbient</u> °F <u>saturat</u>	t <u>ed</u> % Moisture				
Describe the warning/alarr	n system that p	rotects against op	eration when unit is not m	meeting design requirements.			
N/A							
Emissions Data							
Pollutant		nlet	Outlet	Removal Efficiency (%)			
	See	Attachment C	- Emission Inventory				

## **Section C - Air Cleaning Device (Continued)**

#### 14. Costs

Indicate cost associated with air cleaning device and its operating cost (attach documentation if necessary)

Device	Direct Cost	Indirect Cost	Total Cost	Annual Operating Cost
Drift Eliminators	TBD	TBD	TBD	TBD

#### 15. Miscellaneous

Describe in detail the removal, handling and disposal of dust, effluent, etc. from the air cleaning device including proposed methods of controlling fugitive emissions.

N/A

Attach manufacturer's performance guarantees and/or warranties for each of the major components of the control system (or complete system).

Vendor guarantee of 0.0005% drift rate.

Attach the maintenance schedule for the control equipment and any part of the process equipment that if in disrepair would increase air contaminant emissions.

The Refinery will develop a maintenance schedule in accordance with manufacturer's recommendations.

#### **Section B - Processes Information**

#### 1. Source Information – Fugitive Emissions from New Components

Source Description (give type, use, raw materials, product, etc). Attach additional sheets as necessary.

Fugitive emissions from new components such as valves, flanges, connectors, and pumps, etc., associated with the proposed project.

Manufacturer <b>N/A</b>	Model No. <b>N/A</b>	Number of Sources 1
Source Designation	Maximum Capacity	Rated Capacity
N/A	N/A	N/A

Type of Material Processed

Cooling water, refinery fuel gas, and process vapors and liquids associated with the ULSG project.

#### **Maximum Operating Schedule**

Hours/Day	Days/Week	Days/Year	Hours/Year
24	7	365	8,760

Operational restrictions existing or requested, if any (e.g., bottlenecks or voluntary restrictions to limit PTE)

Capacity (specify units)

Per Hour	Per Day	Per Week	Per Year
N/A	N/A	N/A	N/A
Operating Schedule	•		
Hours/Day	Days/Week	Days/Year	Hours/Year
N/A	N/A	N/A	N/A
Seasonal variations (	Months) From <b>N/A</b>	to	

If variations exist, describe them

N/A

2. Fuel – N/A					
Туре	Quantity Hourly	Annually	Sulfur	% Ash (Weight)	BTU Content
Oil Number N/A	GPH @ 60°F	X 10 <sup>3</sup>	% by wt		Btu/Gal. & Lbs./Gal. @ 60 °F
Oil Number <u>N/A</u>	GPH @ 60°F	Gal X 10 <sup>3</sup> Gal	% by wt		Btu/Gal. & Lbs./Gal. @ 60 °F
Natural Gas <u>N/A</u>	SCFH	X 10 <sup>6</sup> SCF	grain/100 SCF		Btu/SCF
Gas (other) N/A	SCFH	X 10 <sup>6</sup> SCF	grain/100 SCF		Btu/SCF
Coal <i>N/A</i>	TPH	Tons	% by wt		Btu/lb
Other * <u>N/A</u>					
*Note: Describe ar	nd furnish information	separately for oth	er fuels in Addendur	n B.	

Section B - Processes Information (Continued)						
3. Burner – N/A						
Manufacturer	Type and N	lodel No.			Number of Burners	
Description:				-		
Rated Capacity		Maximum C	apacity			
4. Process Storage Vessels						
A. For Liquids – N/A						
Name of material stored						
Tank I.D. No.	Manufacturer			Date Instal	led	
Maximum Pressure		Capacity	(gallons/M	eter³)		
Type of relief device (pressure set vent/c	onservation vent/	emergency v	rent/open ve	ent)		
Relief valve/vent set pressure (psig)		Vapor press. of liquid at storage temp. (psia/kPa)				
Type of Roof: Describe:						
Total Throughput Per Year		Number of fills per day (fill/day): Filling Rate (gal./min.): Duration of fill hr./fill):				
B. For Solids – N/A				,		
Type: ☐ Silo ☐ Storage Bin ☐ Other	, Describe	Name of	Material St	tored		
Silo/Storage Bin I.D. No.	Manufacturer			Date Instal	led	
State whether the material will be stored	in loose or bags i	n silos	Capacity	(Tons)		
Turn over per year in tons		Turn over per day in tons				
Describe fugitive dust control system for	loading and hand	lling operation	ns			
Describe material handling system						
5. Request for Confidentiality						
Do you request any information on this a If yes, include justification for confidential					∕es ⊠ No ed "confidential".	

#### **Section B - Processes Information (Continued)**

6.	Misce	llaneous	Inform	nation

Attach flow diagram of process giving all (gaseous, liquid and solid) flow rates. Also, list all raw materials charged to process equipment, and the amounts charged (tons/hour, etc.) at rated capacity (give maximum, minimum and average charges describing fully expected variations in production rates). Indicate (on diagram) all points where contaminants are controlled (location of water sprays, collection hoods, or other pickup points, etc.). Describe collection hoods location, design, airflow and capture efficiency. Describe any restriction requested and how it will be monitored.

See Attachment A – Application Narrative

Describe fully the fac	cilities provided to mon	itor and to record	l process o	operating conditions	, which may a	affect the emission
of air contaminants.	Show that they are rea	asonable and ade	equate.			

The proposed fugitive components will be incorporated into the Refinery's existing alternative monitoring plan as per 40 CFR Part 63, Subpart CC.

N/A

Identify and describe all fugitive emission points, all relief and emergency valves and any by-pass stacks.

See Attachment A - Application Narrative

Describe how emissions will be minimized especially during start up, shut down, process upsets and/or disruptions.

The proposed fugitive components will be incorporated into the Refinery's existing alternative monitoring plan as per 40 CFR Part 63, Subpart CC.

**Anticipated Milestones:** 

- i. Expected commencement date of construction/reconstruction/installation: **2Q2016**
- ii. Expected completion date of construction/reconstruction/installation: 2Q2017

iii. Anticipated date of start-up:

2Q2017

	Se	ection C - Air C	Cleaning Device				
1. Precontrol Emiss	sions* – <i>Not Availab</i>	ole					
		Maximum	Emission Rate		Calculation/		
Pollutant	Specify Units	Pounds/Hour	Hours/Year	Tons/Year	Estimation Method		
PM	opeomy emile			10110110	1		
PM <sub>10</sub>							
SO <sub>x</sub>							
CO							
NO <sub>x</sub>							
VOC Others: (e.g., HAPs)							
Others. (e.g., HAFS)							
* These emissions mus schedule for maximur values were determine	m limits or restricted	hours of operation	ted operating schedul on and/or restricted thr				
2. Gas Cooling – N/	⁄A						
Water quenching	Yes 🗌 No	Water injection ra	ate	GPM			
Radiation and convection cooling  Yes No			Air dilution Yes No If yes,CFM				
Forced Draft Yes	☐ No		Water cooled duct work Yes No				
Other							
Inlet Volume	ACFM		Outlet Volume	ACFM			
@°F	% Moisture		@°F	% Moisture			
Describe the system in o	detail.						

Section C - Air Cleaning Device (Continued)							
3. Settling Chambers – A	//A						
Manufacturer	_	/olume of gas handled ACF °F		Gas velocity	Gas velocity (ft/sec.)		
Length of chamber (ft.)	Width of	chamber (ft.)	Height of chamb	er (ft.)	Number of trays		
Water injection Yes [	No		Water injection r	ate (GPM)			
Emissions Data							
Inlet		Ou	tlet	R	emoval Efficiency (%)		
4. Inertial and Cyclone C	ollectors -			1			
Manufacturer		Type		Model N	Model No.		
Pressure drop (in. of water)		Inlet volumeACFM @°F		Outlet vo	olumeACFM @°F		
Number of individual cyclone(	s)		Outlet straightening vanes used?  Yes No				
Length of Cyclone(s) Cylinder	(ft.)	Diameter of Cyclone(s) Cylinder (ft.)		Length o	Length of Cyclone(s) cone (ft.)		
Inlet Diameter (ft.) or duct area	я (ft.²) of с	yclone(s)	Clone(s) Outlet Diameter (ft.) or duct area (ft.²) of cyclone(s)				
If a multi-clone or multi-tube u	nit is instal	lled, will any of the ind	ividual cyclones o	r cyclone tub	es be blanked or blocked off?		
Describe any exhaust gas rec	irculation l	oop to be employed.					
Attach particle size efficiency	curve						
<b>Emissions Data</b>							
Inlet		Ou	tlet	R	emoval Efficiency (%)		

Section C - Air Cleaning Device (Continued)							
5. Fabric Collector – N/A							
Equipment Specifications							
Manufacturer		Mo	del No.		Pressurized Design Suction Design		
Number of Compartments	N	umber of Filters Pe	er Compartment	Is Baghouse	e Insulated?		
Can each compartment be isolated for repairs and/or filter replacement?							
Are temperature controls provided? (Describe in detail)							
Dew point at maximum moist	ıre	°F	Design inlet volume		SCFM		
Type of Fabric  Material  Weight  Thickness	_ oz/sq.yd	☐ Felted ☐ Woven ☐ Felted-Wov					
Fabric permeability (clean) @	½" water-∆ P		CFM/sq.ft.				
Filter dimensions Length_		Diameter/	Width				
Effective area per filter			Maximum operating		(°F)		
Effective air to cloth ratio	Minimum_		Maximum				
Drawing of Fabric Filter A sketch of the fabric filter and temperature indicator s		cess doors, catwal			x, location of each pressure		
Operation and Cleaning							
Volume of gases handled ACFM @	°F		ross collector (in. of ipment to be used to	,	oressure drop.		
Type of filter cleaning  Manual Cleaning  Mechanical Shakers  Pneumatic Shakers		Bag Collapse Sonic Cleaning Reverse Air Flow		Reverse			
Describe the equipment provi	aea ii ary oii ir	ee air is required id	or collector operation				
Cleaning Initiated By  Timer Frequency if timer actuated  Expected pressure drop range in. of water Other Specify							
Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If yes, describe.							
Describe the warning/alarm system that protects against operation when the unit is not meeting design requirements.							
<b>Emissions Data</b>							
Pollutant		Inlet	Outlet	R	emoval Efficiency (%)		
				1			

Section C - Air Cleaning Device (Continued)								
6. Wet Collection Equ	ipment – N/A							
<b>Equipment Specification</b>	S							
Manufacturer		Туре		Model No	).			
Design Inlet Volume (SCF	M)	Relative Particulate/Gas Velocity (ejector scrubbers only)						
Describe the internal feat limiters, etc.).	ures (e.g., var	iable throat, gas.	/liquid diffusion plates,	spray nozz	zles, liquid redistributors, bed			
Describe pH monitoring ar	nd pH adjustme	nt systems, if app	olicable.					
Describe mist eliminator o	r separator (typ	e, configuration, I	backflush capability, freq	uency).				
Attach particulate size effic	ciency curve.							
Operating Parameters								
Inlet volume of gases han	dled	(ACFM)	Outlet volume of ga	ses handle	ed (ACFM)			
	@	°F	@	°F	% Moisture			
Liquid flow rates. Descrecirculating solution, mak			easure liquid flow rates	to scrubb	per (e.g., quenching section,			
Describe scrubber liquid s etc.)	upply system (a	amount of make-	up and recirculating liqui	d, capacity	of recirculating liquid system,			
State pressure drop range (in water) across scrubber (e.g., venturi throat, packed bed, etc.) only. Describe the equipment provide to measure the pressure drop. Do not include duct or de-mister losses.								
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.								
Emissions Data								
Pollutant		nlet	Outlet		Removal Efficiency (%)			

	Section	n C - Air Cl	ean	ing Device (Cont	inued)			
7. Electrostatic Precip	oitator – <i>N/A</i>							
<b>Equipment Specification</b>	S							
Manufacturer		Model No.			☐ Wet	e-Stage	☐ Dry ☐ Two-Stage	
Gas distribution grids	] Yes □ No			Design Inlet Volume (SCFM)  Maximum operating temperature (°F)				
Total collecting surface are	ea	sq. ft. C	ollect	tor plates size length_	_	ft. x width_	ft.	
Number of fields		N	umbe	er of collector plates/fi	eld			
Spacing between collector	plates	inche	es.					
Maximum gas velocity	1	t./sec. M	inimu	um gas treatment time	e:	sec.		
Total discharge electrode length ft.  Number of discharge electrodes Number of collecting electrode rappers  Rapper control								
	3							
Operating Parameters								
Inlet gas temperature (°F)				State pressure drop	o range (in	ches water	gauge) across	
Outlet gas temperature (°	F)	<u></u>	collector only					
				Describe the equip	ment			
Volume of gas handled (A	CFM)	_		Dust resistivity (ohm-cm). Will resistivity vary?				
Power requirements								
Number and size of Trans	former Rectifier	sets by electr	ical fi	eld				
Field No.	No. of	Sets	Ea	ch Transformer KVA	KV Ave.	Each Ro /Peak	ectifier Ma DC	
Current Density  Micro ampe	res/ft².	Corona Power es/ft². Watts/1000 ACFM			Corona Power Density Watts/ft².			
Will a flue gas conditioning	system be em	ployed? If yes	s, des	scribe it.				
Does air cleaning device e	mploy hopper I	neaters, hoppe	er vib	rators or hopper level	detectors?	If yes, des	scribe.	
Describe the warning/alarr	n system that p	rotects agains	t ope	eration when unit is no	t meeting o	design requ	irements.	
Emissions Data								
Pollutant	I	nlet		Outlet		Remov	al Efficiency (%)	

Section C - Air Cleaning Device (Continued)					
8. Adsorption Equipm	nent – <i>N/A</i>				
<b>Equipment Specification</b>	s				
Manufacturer	Туре			Model No.	
Design Inlet Volume (SCFM)  Adsorbent			nt charge per adsorber	r vessel and number of adsorber vessels	
Length of Mass Transfer Z	one (MTZ), supplied b	y the manuf	acturer based upon la	aboratory data.	
Adsorber diameter (ft.) and area ft <sup>2</sup> .)			Adsorption bed depth (ft.)		
Adsorbent information					
Adsorbent type and physic	al properties.				
Working capacity of adsorbent (%)			Heel percent or unrecoverable solvent weight % in the adsorbent after regeneration.		
Operating Parameters					
Inlet volume of gases handled (ACFM) @ °F					
Adsorption time per adsorption bed			Breakthrough capacity: Lbs. of solvent / 100 lbs. of adsorbent =		
Vapor pressure of solvents at the inlet temperature			Available steam in pounds to regenerate carbon adsorber (if applicable)		
Percent relative saturation of each solvent at the inlet temperature					
Attach any additional data	including auxiliary equ	uipment and	operation details to th	noroughly evaluate the control equipment	ī. <b>.</b>
Describe the warning/alarr	n system that protects	against ope	eration when unit is no	t meeting design requirements.	
<b>Emissions Data</b>					
Pollutant	Inlet		Outlet	Removal Efficiency (%)	

Section C - Air Cleaning Device (Continued)								
9. Absorption Equipm	nent – N/A							
<b>Equipment Specification</b>	S							
Manufacturer		Туре			Model No	0.		
Design Inlet Volume (SCF	M)		To	wer height (ft.) and	inside d	iameter (ft.)		
Packing type and size (if a	pplicable)		He	ight of packing (ft.)	(if applic	cable)		
Number of trays (if applica	ble)		Nu	mber of bubble cap	os (if app	olicable)		
Configuration  Counter-curren	ıt [	Cross flow		Cocurrent flow				
Describe pH and/or other monitoring and controls.								
Absorbent information								
Absorbent type and conce	ntration.		Re	tention time (sec.)				
Attach equilibrium data for	absorption (if a	applicable)	•					
						ply system (once through or e flow rates for makeup, bleed		
Operating Parameters								
Volume of gas handled (A	CFM) Inle	et temperature (°F)		Pressure drop (in. of water) and liquid flow rate.  Describe the monitoring equipment.				
State operating range for p	H and/or abso	orbent concentration	n in sci	rubber liquid.				
Describe the warning/alarr	n system that p	protects against op	eration	when unit is not n	neeting d	lesign requirements.		
<b>Emissions Data</b>								
Pollutant	ľ	Inlet		Outlet		Removal Efficiency (%)		

Section C - Air Cleaning Device (Continued)										
10. Selective Cataly	ytic Reduction	(SCR) - <i>N/A</i>								
	•	ction (SNCR) – <i>N</i>								
Non-Selective Catalytic Reduction (NSCR) – <i>N/A</i>										
Equipment Specifications										
Manufacturer		Type Model No.								
Design Inlet Volume (SCF	M)		Design operating te	mperature	(°F)					
Is the system equipped with process controls for proper mixing/control of the reducing agent in gas stream? If yes, give details.										
Attach efficiency and other pertinent information (e.g., ammonia slip)										
Operating Parameters										
Volume of gases handled (ACFM) @ °F										
Operating temperature range for the SCR/SNCR/NSCR system (°F) From°F To°F										
Reducing agent used, if any  Oxidation catalyst used, if any										
State expected range of us	sage rate and c	oncentration.								
Service life of catalyst			Ammonia slip (ppm	nonia slip (ppm)						
Describe fully with a sketch giving locations of equipment, controls systems, important parameters and method of operation.										
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.										
<b>Emissions Data</b>										
Pollutant	l	nlet	Outlet		Removal Efficiency (%)					

Section C - Air Cleaning Device (Continued)									
11. Oxidizer/Afterburne	ers – <i>N/A</i>								
<b>Equipment Specification</b>	s								
Manufacturer		Туре 🗌	The	ermal	☐ Catalytic	Model	No.		
Design Inlet Volume (SCF	M)	Combustion chamber vo			dimensions (	length,	cross-sectional area,	effective	
Describe design features, which will ensure mixing in combustion chamber.									
Describe method of preapplicable).	heating incom	ning gases	(if	Descril applica		nger sys	stem used for heat re	covery (if	
Catalyst used	Life of catalyst				emperature rise alyst (°F)	Heiç Diar	Dimensions of bed (in inches).  Height:  Diameter or Width:  Depth:		
Are temperature sensing devices being provided to measure the temperature rise across the catalyst?   No If yes, describe.									
Describe any temperature sensing and/or recording devices (including specific location of temperature probe in a drawing or sketch.								drawing	
Burner Information									
Burner Manufacturer Model No.		Model No.	lo.		Fuel U	Jsed			
Number and capacity of burners Rated capa			city	city (each) Maximum capacity (each)					
Describe the operation of the burner				Attach dimensioned diagram of afterburner					
Operating Parameters									
Inlet flow rate (ACFM) @°F						°F			
State pressure drop range across catalytic bed (in. of water).				Describe the method adopted for regeneration or disposal of the used catalyst.				osal of	
Describe the warning/alarr	n system that p	rotects again	st o	peration	when unit is no	t meetin	g design requirements.		
Emissions Data				_					
Pollutant	<u> </u>	nlet			Outlet		Removal Efficiency	(%)	

Section C - Air Cleaning Device (Continued)								
12. Flares – <i>N/A</i>								
Equipment Specification	S							
Manufacturer			vated flare ner	☐ Grou		Model No.		
Design Volume (SCFM)		Dimensions of Diameter_		Height				
Residence time (sec.) and temperature (°F)	outlet	Turn down ratio	)		Burner details			
Describe the flare design (flare with a sketch.	(air/steam-assi	sted or nonassist	ed), essent	ial auxiliaries i	ncluding pilot flame m	nonitor of proposed		
Describe the operation of the flare's ignition system.								
Describe the provisions to	introduce auxi	liary fuel to the fla	ire.					
Operation Parameters								
Detailed composition of the	ne waste gas	Heat content	Heat content			Exit velocity		
Maximum and average gas flow burned (ACFM)  Operating temperature (°F)								
Describe the warning/alarr	n system that <sub>l</sub>	orotects against o	peration wh	nen unit is not	meeting design requi	rements.		
<b>Emissions Data</b>								
Pollutant		Inlet		Outlet	Removal Ef	ficiency (%)		

Section C - Air Cleaning Device (Continued)									
13. Other Control Equi	pment – N/A								
Equipment Specification	ıs		1						
Manufacturer		Туре		Model No.					
Design Volume (SCFM)			Capacity						
Describe pH monitoring and pH adjustment, if any.									
Indicate the liquid flow rate and describe equipment provided to measure pressure drop and flow rate, if any.									
Attach efficiency curve and/or other efficiency information.									
Attach any additional date including auxiliary equipment and operation details to thoroughly evaluate the control equipment.									
Operation Parameters									
Volume of gas handled									
ACFM @ °F % M	oisture								
Describe fully giving impor	tant parameter	s and method of o	peration.						
Describe the warning/alarr	m system that p	rotects against op	peration when unit is not	meeting design requirements.					
Emissions Data									
Pollutant	I	nlet	Outlet	Removal Efficiency (%)					

	Section C -	Air Cleaning Device	e (Continued)	
14. Costs				
Indicate cost associated	with air cleaning device	and its operating cost (	attach documentation	n if necessary)
Not available				
Device	Direct Cost	Indirect Cost	Total Cost	Annual Operating Cos
V/A				
5. Miscellaneous				
	noval, handling and disp	osal of dust, effluent, et	tc. from the air cleani	ng device including proposed
nethods of controlling fu	gitive emissions.			
V/A				
Attach manufacturer's pe or complete system).	erformance guarantees a	and/or warranties for ea	ch of the major comp	conents of the control system
V/A				
WA				
Attach the maintenance	schedule for the control	equipment and any par	t of the process equi	pment that if in disrepair woul
ncrease air contaminant				

	Section D - Additional Information		
	ill the construction, modification, etc. of the sources covered by this application increase facility? If so, describe and quantify.	ase emissions from ot	her sources at
Se	ee Attachment C – Emissions Inventory.		
lf t	his project is subject to any one of the following, attach a demonstration to show co	mpliance with applica	ble standards.
a.	Prevention of Significant Deterioration permit (PSD), 40 CFR 52?	☐ YES	⊠ NO
b.	New Source Review (NSR), 25 Pa. Code Chapter 127, Subchapter E?	⊠ YES	□NO
C.	New Source Performance Standards (NSPS), 40 CFR Part 60? (If Yes, which subpart) <i>GGGa</i>	⊠ YES	□NO
d.	National Emissions Standards for Hazardous Air Pollutants (NESHAP), 40 CFR Part 61? (If Yes, which subpart)	☐ YES	⊠ NO
e.	Maximum Achievable Control Technology (MACT) 40 CFR Part 63? (If Yes, which part) <b>CC</b>	⊠ YES	□NO
	each a demonstration showing that the emissions from any new sources will be the	minimum attainable th	rough the use
	best available technology (BAT). ee Attachment A – Application Narrative.		
Pr	ovide emission increases and decreases in allowable (or potential) and actual emiss	sions within the last fiv	re (5) years for
ар	plicable PSD pollutant(s) if the facility is an existing major facility (PSD purposes).		( / )
Se	ee Attachment C – Emissions Inventory.		

#### Section D - Additional Information (Continued)

Indicate emission increases and decreases in tons per year (tpy), for volatile organic compounds (VOCs) and nitrogen oxides (NOx) for NSR applicability since January 1, 1991 or other applicable dates (see other applicable dates in instructions). The emissions increases include all emissions including stack, fugitive, material transfer, other emission generating activities, quantifiable emissions from exempted source(s), etc.

		Indicate Yes		VC	Cs	N	Ox
Permit number	Date	or <b>No</b> if emission increases and decreases were used previously for	Source I. D. or Name	Emission increases in potential to emit	Creditable emission decreases in actual emissions	Emission increases in potential to emit	Creditable emission decreases in actual emissions
(if applicable)	issued	netting	Source I. D. or Name	(tpy)	(tpy)	(tpy)	(tpy)
		Se	ory.				
		_					

If the source is subject to 25 Pa. Code Chapter 127, Subchapter E, New Source Review requirements,

### See Attachment A – Application Narrative

- Identify Emission Reduction Credits (ERCs) for emission offsets or demonstrate ability to obtain suitable ERCs for emission offsets.
- b. Provide a demonstration that the lowest achievable emission rate (LAER) control techniques will be employed (if applicable).
- c. Provide an analysis of alternate sites, sizes, production processes and environmental control techniques demonstrating that the benefits of the proposed source outweigh the environmental and social costs (if applicable).

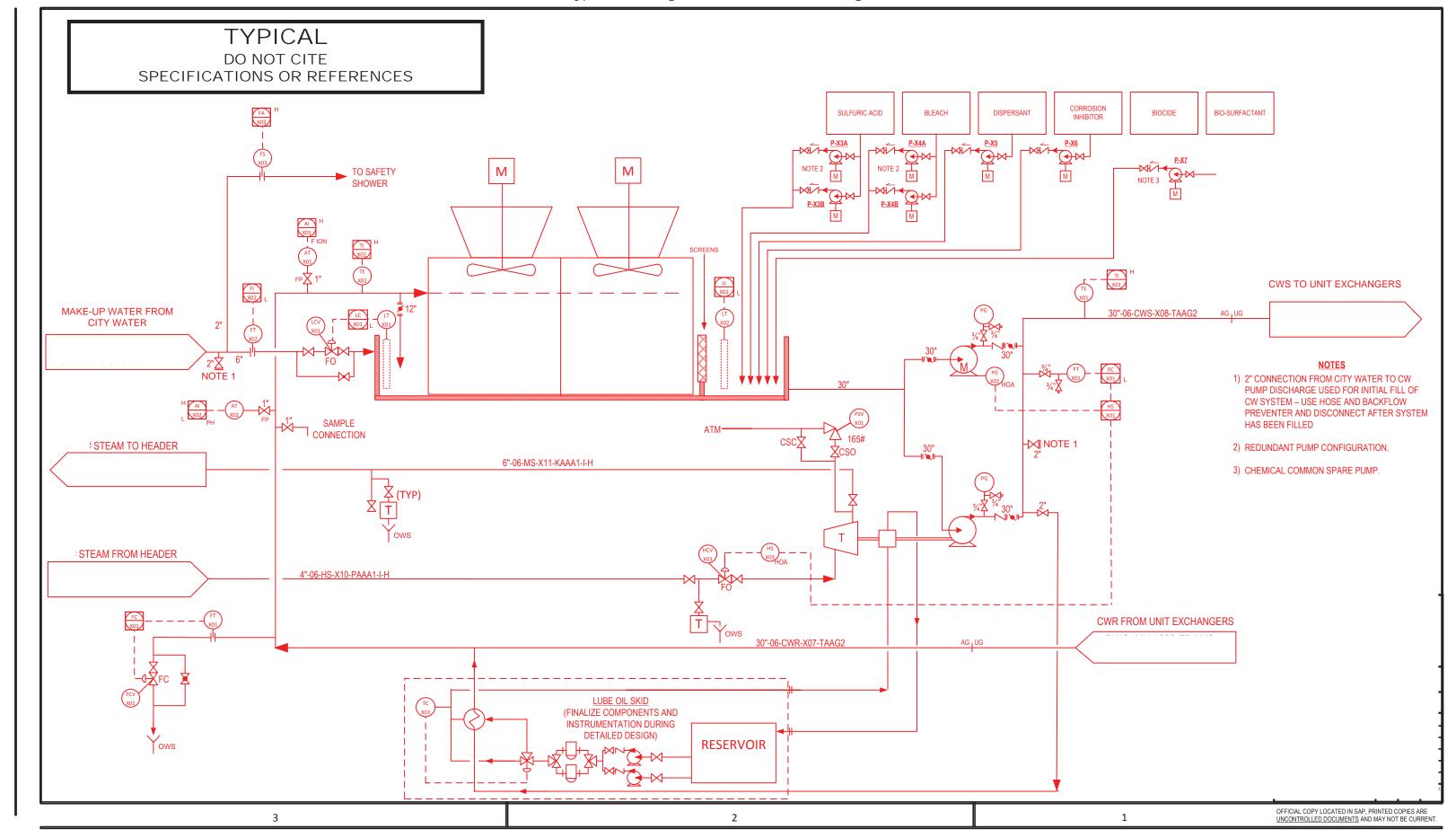
Attach calculations and any additional information necessary to thoroughly evaluate compliance with all the applicable requirements of Article III and applicable requirements of the Clean Air Act adopted thereunder. The Department may request additional information to evaluate the application such as a standby plan, a plan for air pollution emergencies, air quality modeling, etc. **See Attachment C – Emissions Inventory.** 

Section E - Compliance Demonstration - N/A
Note: Complete this section if source is not a Title V facility. Title V facilities must complete Addendum A.
Method of Compliance Type: Check all that apply and complete all appropriate sections below
☐ Monitoring ☐ Testing ☐ Reporting
Recordkeeping Work Practice Standard
Monitoring:
a. Monitoring device type (Parameter, CEM, etc):
b. Monitoring device location:
c. Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:
Testing:
a. Reference Test Method: Citation
b. Reference Test Method: Description
Recordkeeping:
Describe what parameters will be recorded and the recording frequency:
Reporting:
Describe what is to be reported and frequency of reporting:
b. Reporting start date:
Work Practice Standard:
Describe each:

	Section	on F - Flu	e and Air	Contamir	nant Emissio	on	
1. Estimated Atmos	pheric Emiss	sions*					
		Ma	aximum emis	sion rate			Calculation/
Pollutant	specify u	nits	lbs/hr		tons/yr.	E	stimation Method
PM			Soo Attoohn	ont C Er	missions Inver	tori	
PM <sub>10</sub>		,	See Allacilli	ient C – En	nissions Inver	ntory.	
SO <sub>x</sub>							
CO							
$NO_x$							
VOC							
Others: ( e.g., HAPs)							
* These emissions mus schedule for maximum values were determine	n limits or rest	ricted hour					
2. Stack and Exhaus	ster						
Stack Designation/Num	ber <i>TBD</i>						
List Source(s) or source  Cooling Tower	ID exhausted	d to this sta	nck:	% of flow e	exhausted to sta	ack:	
Stack height above grade Grade elevation (ft.) ~ 1			tack diamete	` ,	let duct area (s	q. ft.)	f. Weather Cap  ☐ YES ☐ NO
Distance of discharge to	nearest prop	erty line (ft	t.). Locate or	n topograph	nic map.		
~600 – 1,000 ft							
Does stack height meet Good Engineering Practice (GEP)?  N/A							
If modeling (estimating) of ambient air quality impacts is needed, attach a site plan with buildings and their dimensions and other obstructions. <b>N/A</b>							
Location of stac Latitude/Longite	l Latitude I Longitude						itude
Point of Origi	n	Degrees	Minutes	Second	s Degrees	Minutes	Seconds
Stack exhaust Volume ~2,000,000	ACFM	Temperat	ture <u><b>85</b></u> °F		Moist	ure <u>satura</u>	ted %
Indicate on an attached necessary dimensions. <b>N/A</b>	d sheet the lo	ocation of	sampling po	rts with res	spect to exhau	st fan, bree	eching, etc. Give all
Exhauster (attach fan cu	irves) <i>N/A</i>		in.	of water <u>N//</u>	4	HP @ <b>N</b>	<b>/A</b> RPM.
** If the data and collection, provide the						I Information	on Form-Authorization

2. Stack and Exhauster								
Stack Designation/Number New Fugi	tive Compo	onents						
List Source(s) or source ID exhausted			% of flow exh	austed to sta	ıck: <b>0</b> %			
Pipes, valves, flanges, connectors, pumps, etc.  Stack height above grade (ft.) N/A  Grade elevation (ft.) N/A  N/A  Stack diamete			er (ft) or Outlet duct area (sq. ft.)  f. Weather Cap –  N/A  YES \( \text{NO} \)					
Distance of discharge to nearest property	erty line (ft.)	. Locate o	n topographic n	nap.				
TBD								
Does stack height meet Good Enginee  N/A	Does stack height meet Good Engineering Practice (GEP)?  N/A							
If modeling (estimating) of ambient air quality impacts is needed, attach a site plan with buildings and their dimensions and other obstructions. <i>N/A</i>								
Location of stack** Latitude/Longitude		Latitude	Lon			gitude		
Point of Origin	Degrees	Minutes	Seconds	Degrees	Minutes	Seconds		
Plant Entrance								
Stack exhaust Volume <u><b>N/A</b></u> ACFM	Temperatu	re <u><i>N/A</i></u> °F		Moistu	re <u><b>N/A</b></u> %			
ate on an attached sheet the location dimensions.  N/A	of sampling	ports with	respect to exh	aust fan, bre	eeching, et	c. Give all necessary		
Exhauster (attach fan curves) N/A		in.	of water <u>N/A</u>		HP @ <u><b>N</b>//</u>	RPM.		
** If the data and collection method Application, provide the additional de			•		l Information	on Form-Authorization		

Section G - Attachments
Number and list all attachments submitted with this application below:
Attachment A – Application Narrative Attachment B – PADEP Application Forms Attachment C – Emissions Inventory Attachment D – Municipal Notification Letters Attachment E – All4 Inc. Quality Seal





### **Addendum A: Source Applicable Requirements**

Describe and cite all applicable requirements pertaining to this source.

Note: A Method of Compliance Worksheet (Addendum 1) must be completed for each requirement listed.

Citation Number	Citation Limitation	Limitation Used
40 CFR §63.654(c)(1)	The owner or operator must perform monitoring to identify leaks of total strippable volatile organic compounds (VOC) from each heat exchange system.	N/A
25 Pa. Code §123.13(c)(1)(iii)	Filterable PM from the proposed cooling tower may not exceed 0.02 grains per dry standard cubic foot.	PM limits as listed in §123.13(c)(1)(iii).
25 Pa. Code §127.12(a)(5)	Show that the emissions from a new source will be the minimum attainable through the use of the best available technology.	Use of drift eliminators with a drift rate of 0.0005% and LDAR monitoring.



# Addendum 1 Method Of Compliance Worksheet

SEC	SECTION 1. APPLICABLE REQUIREMENT						
Fede	ral Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC	7		
Plant	Plant Code: 45-5201144 Plant Name: Trainer Refinery, PA						
Appli	cable Requir	ement for: (ple	ase check only	one box below)			
	The entire si	ite					
	A group of s	sources, Group	ID:				
	A single sou	ırce, Unit ID:	Proposed	Cooling Tower			
	Alternative S	Scenario, Scena	ario Name:				
Citati	ion #: 40 C	CFR §63.654(c)	(1)				
Com	pliance Metho	od based upon:	Appl	icable Requirement		Gap Filling Requirement	
Meth	od of Compli	ance Type: (Ch	eck all that app	lies and complete all ap	opropriat	te sections below)	
$\boxtimes$	Monitorin	ng 🖂	Testing	$\boxtimes$	Repor	ting	
	Record K	eeping	Work Practi	ce Standard			
Sec	Section 2: Monitoring						
1. Monitoring device type (stack test, CEM, etc.):  Monthly Sampling							
2. N	2. Monitoring device location: Return line						
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							
Leaks of total strippable volatile organic compounds (VOCs) recorded monthly.							
3. H	3. How will data be reported: Semi-annual reports will be submitted per 40 CFR Part 63, Subpart CC.						

#### Section 3: Testing

1. Reference Test Method Description:	Air Stripping Method (Modified El Paso Method) for Determination of Volatile Organic Compound Emissions from Water Sources
2. Reference Test Method Citation:	Texas Commission of Environmental Quality (TCEQ), Sampling Procedures Manual, Appendix P: Cooling Tower Monitoring Guidance.

### Section 4: Record Keeping

Describe what parameters will be recorded and the frequency of recording:

The date and concentration of strippable hydrocarbon when a leak is detected and the date and concentration of strippable hydrocarbon once the leak is repaired.

### Section 5: Reporting

#### Describe what is to be reported and the frequency of reporting:

Periodic reporting submitted every six (6) months including any leaks that occurred, the concentration of strippable hydrocarbon before and after the leak is repaired, the date the leak was identified and the date it was repaired.

1. Reporting start date: Six (6) months after the date of the Notification of Compliance Status report is submitted

#### Section 6: Work Practice Standard

Describe any work practice standards:	
N/A	
	_



# Addendum 1 Method Of Compliance Worksheet

SEC	SECTION 1. APPLICABLE REQUIREMENT					
Feder	al Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC		
Plant	Code:	45-5201144	Plant	Trainer Refinery, PA		
Applic	cable Requir	ement for: (plea	ase check only	one box below)		
	The entire si	ite				
	A group of s	ources, Group	D:			
$\boxtimes$	A single sou	ırce, Unit ID:	Propose	d Cooling Tower		
	Alternative S	Scenario, Scena	rio Name:			
Citatio	on #: 25 P	a. Code §123.1	3(c)(1)(iii) an	d 25 Pa. Code §127.12(a)(5)		
Comp	liance Metho	od based upon:	⊠ App	licable Requirement Gap Filling Requirement		
Metho	od of Compli	ance Type: (Ch	eck all that ap	plies and complete all appropriate sections below)		
	Monitorin	ng 🗌	Testing	Reporting		
	Record K	eeping	Work Prac	tice Standard		
Sect	Section 2: Monitoring					
4.	Monitoring etc.):	g device type (st	ack test, CEM	N/A		
5.	Monitoring location:	g device	N/A			
Descr	Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:					

6. How will data be reported:	N/A	
Section 3: Testing		
2. Reference Test Method Description:	_	N/A
3. Reference Test Method	Citation:	N/A
Section 4: Record Keep	ing	
Describe what parameters will be	e recorded	and the frequency of recording:
N/A		
Section 5: Reporting		
Describe what is to be reported	and the free	quency of reporting:
N/A		
1. Reporting start date:		
Section 6: Work Practice	e Standard	<b>1</b>
Describe any work practice star	ndards:	
Monroe Energy proposes to op	perate the pi	roposed new cooling tower according to the manufacturer
specifications.		



# Addendum 1 Method Of Compliance Worksheet

SECTION	SECTION 1. APPLICABLE REQUIREMENT						
Federal Tax	Federal Tax Id: 45-5201144 Firm Name: Monroe Energy, LLC						
Plant Code:	Plant Code: 45-5201144 Plant Trainer Refinery, PA						
Applicable F	Requir	ement for: (ple	ase check only	y one box below)			
The er	ntire si	ite					
A grou	up of s	ources, Group	ID: Propose	ed Cooling Towers			
A sing	le sou	rce, Unit ID:					
Altern	ative S	Scenario, Scen	ario Name:				
Citation #:	25 P	a. Code §127.	12(a)(5)				
Compliance	Metho	od based upon	⊠ App	Olicable Requirement Gap Filling Requirement			
Method of C	ompli	ance Type: (Cl	neck all that ap	oplies and complete all appropriate sections below)			
⊠ Mo	nitorin	ıg 🗌	Testing	Reporting			
⊠ Red	cord K	eeping 🔀	Work Prac	ctice Standard			
Section 2:	Section 2: Monitoring						
7. Monitoring device type (stack test, CEM, etc.):  Sampling							
	8. Monitoring device $N/A$ location:						
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							
Monroe Energy will monitor total dissolved solids (TDS) in the cooling tower water. The cooling water circulating rate is constant.							

Addendum 1	
9. How will data be N/A reported:	
Section 3: Testing	
4. Reference Test Method Description:	Sampling and analysis of TDS in circulated water.
5. Reference Test Method Citation:	N/A
Section 4: Record Keeping	
Describe what parameters will be recorde	ed and the frequency of recording:
Monroe Energy proposes to maintain re	ecords of monthly TDS concentrations and the amount of water
circulated through the proposed cooling	g tower.
Section 5: Reporting	
Describe what is to be reported and the fi	requency of reporting:
N/A	
2. Reporting start date:	
Continue Con Monda Burnetina Ctanada	

### Section 6: Work Practice Standard

Describe any work practice standards:

Monroe Energy proposes to operate the proposed new cooling tower according to the manufacturer specifications.



### **COMBUSTION UNIT**

### Application for Plan Approval to Construct, Modify or Reactivate an Air Contamination Source and/or Install an Air Cleaning Device

This application and the General Information Form (GIF) must be included in the submittal

Before completing this form, read the instructions provided with this form.

Section /	A - Facility Name, Checklis	st And Certification
Organization Name or Registered Fictit DEP Client ID# (If Known): 296139	ious Name/Facility Name: <u>Monr</u>	oe Energy, LLC – Trainer Refinery
Type of Review required and Fees:		
<ul> <li>☑ Source requiring approval und</li> <li>☑ Source requiring approval und</li> <li>☐ Source requiring the establish</li> </ul>	er NSR regulations:	\$ <u>1,700</u> \$ <u>5,300</u> \$
	Applicant's Checkl	list
Check the following	ist to make sure that all the re	quired documents are included.
□ General Information Form	(GIF)	
□ Processes Plan Approval a	Application	
Compliance Review Form facilities submitting on a period	or provide reference of most odic basis: 5/14/2015	recently submitted compliance review form for
	and Municipal Notifications	
□ Permit Fees		
Addendum A: Source Appl	icable Requirements (only applic	cable to existing Title V facility)
Certification of Truth	, Accuracy and Completer	ness by a Responsible Official
I, Jeffrey K. Warmann		of law in 18 Pa. C. S. A. §4904, and
35 P.S. §4009(b) (2) that hased on info	rmation and belief formed after r	reasonable inquiry, the statements and information
in this application are true accurate and	I complete.	1.1
(Signature):	Date:	9/14/2015
Name (Print): Jeffrey Warmann	Title: /	President and CEO
	OFFICIAL USE ONLY	
Application No.	Unit ID	Site ID AUTH. ID Reviewed By
DEP Client ID #:	APS. ID	AUTH. ID
Date Received	Date Assigned	of 2 <sup>nd</sup> Technical Deficiency
Comments:	Date C	of Z <sup>IM</sup> Technical Deliciency

Section B - Combustion Unit Information						
1. Combustion Units: Co	oal 🗌 Oil 🔲 Natural Ga	as Other:	Refinery Gas	_		
Description: Reactor Effluent H	leater H-124-01 (H01)					
Manufacturer  Tulsa Heaters, Inc.	Model No. <i>N/A</i>		Number of units	S		
Maximum heat input (Btu/hr)  99.6 MMBtu/hr	Rated heat input (Btu/hr) 99.6 MMBtu/hr	Typical heat	input (Btu/hr)	Furnace Volume  16,040 ft <sup>3</sup>		
Grate Area (if applicable)		Method of fir	ing	1 10,0 10 10		
Indicate how combustion air is s	upplied to boiler	1 114141141	<u> </u>			
Natural draft Indicate the Steam Usage: N/A						
mulcate the Steam Osage. N/A						
Mark and describe soot Cleaning	g Method: <b>N/A</b>					
i. Air Blown	iv.	Other				
ii. Steam Blown	٧.	Frequency of	Cleaning			
iii. Brushed and Vacuumed`						
	Maximum Opera	ting schedu	ıle			
Hours/Day 24		ays/Year <b>65</b>	Ho: <b>8,7</b>	urs/Year <b>60</b>		
Operational restrictions taken or	requested, if any (e.g., bottler	necks or volunt	ary restrictions t	o limit potential to emit)		
Capacity (specify units)			<b>T</b>			
	,	er week <b>6,732.8 MMB</b> t		· year 2 <b>,496 MMBtu</b>		
ээ.о иливш	·		•	2,490 WIWIDLU		
	Typical Operati	ng schedul	е			
		ays/Year		urs/Year		
		65 ~	8,7	60		
Seasonal variations (Months): If variations exist, describe them.  N/A						
Operating using primary fuel: From to Operating using secondary fuel: Form to Non-operating: From to						
Non-operating.	rioiii	_ 10				
2. Specify the primary, secondary and startup fuel. Furnish the details in item 3.						
Primary & Startup Fuel = Refinery Fuel Gas						

#### Section B - Combustion Unit Information (Continued) 3. Fuel % Ash Quantity Hourly **Annually** Sulfur (Weight) **BTU Content Type** Oil Number GPH@ $X 10^{3}$ Btu/Gal. & Lbs./Gal. @ 60 °F 60°F Gal % by wt Oil Number GPH @ X 10<sup>3</sup> Btu/Gal. & 60°F Gal % by wt Lbs./Gal. @ 60 °F Oil Number GPH@ $X 10^{3}$ Btu/Gal. & Lbs./Gal. @ 60 °F 60°F Gal % by wt Natural Gas SCFH $X 10^{6}$ gr/100 Btu/SCF SCF Gal Gas (other) **SCFH** $X 10^{6}$ gr/100 Btu/SCF SCF Gal Coal Other\* <162 ppm (3-hr Refinery Fuel avg.) as H2S Gas ~ 7.38 E08 ~ 84,263 SCFH Negligible ~ 1,182 Btu/SCF <50 ppm (12-SCF/YR month rolling avg.) as H2S \* Note: Describe and furnish information separately for other fuels in Addendum B. 4. Burner Manufacturer Model Number Type of Atomization (Steam, air, press, mech., rotary cup) **Callidus CUBL** Maximum fuel firing rate (all burners) **Number of Burners** Normal fuel firing rate 12.45 MMBtu/hr 8.91 MMBtu/hr If oil, temperature and viscosity. Maximum theoretical air requirement 15% excess air Percent excess air 100% rating 15% Turndown ratio 50% Combustion modulation control (on/off, low-high fire, full automatic, manual). Describe. Manual control Main burner flame ignition method (electric spark, auto gas pilot, hand-held torch, other). Describe. Natural gas pilot Nitrogen Oxides (NO<sub>x</sub>) control Options Mark and describe the NO<sub>x</sub> control options adopted Other. \_\_\_\_ Low excess air (LEA) Flue gas recirculation Over fire air (OFA) ☐ Burner out of service Reburning ☐ Low NO<sub>x</sub> burners with over fire ☐ Flue gas treatment (SCR / SNCR) air

Section B - Combustion Unit Information (Continued)
6. Miscellaneous Information
Describe fly ash reinjection operation N/A
Describe, in detail, the equipment provided to monitor and to record the source(s) operating conditions, which may affect emissions of air contaminants. Show that they are reasonable and adequate.
Continuous Emission Monitoring Systems (CEMS) will measure $NO_X$ and $O_2$ through direct extraction. The heater will also be equipped with a fuel gas flow meter. Fuel gas will be supplied by the existing North Side Fuel Gas system which is already monitored for $H_2S$ and heating value (Btu/scf).
Describe each proposed modification to an existing source.  N/A
Describe how emissions will be minimized especially during start up, shut down, combustion upsets and/or disruptions. Provide emission estimates for start up, shut down and upset conditions. Provide duration of start up and shut down.
Emissions will be minimized by operating the heater in accordance with manufacturer specifications and by minimizing startup time.
Describe in detail with a schematic diagram of the control options adopted for SO <sub>2</sub> (if applicable). <b>N/A</b>
Anticipated milestones:
Expected commencement date of construction/reconstruction:  Expected completion date of construction/reconstruction:  Anticipated date(s) of start-up:  2Q2016  2Q2017  2Q2017

Section C - Air Cleaning Device						
1. Precontrol Emissions* – Not Available						
Emission Rate						
		Maximum	Emission Rate	T	Calculation/	
Pollutant	Specify Units	Pounds/Hour	Hours/Year	Tons/Year	Estimation Method	
PM						
PM <sub>10</sub>						
SOx						
CO						
NO <sub>x</sub>						
VOC						
Others: (e.g., HAPs)						
* These emissions mus schedule for maximur values were determine	n limits or restricted	hours of operation	ed operating schedule and/or restricted throu			
2. Gas Conditioning -	- <b>N/A</b>					
Water quenching	YES NO	Water injection	n rate(	GPM		
Radiation and convectio	n cooling YES	□NO	Air dilution YE	S 🗌 NO		
			If YES,	CFM		
Forced draft	YES NO		Water cooled duct wor	k YES [	NO	
Other						
Inlet volume			Outlet volume			
	ACFM@	°F	ACFM@	)°F	% Moisture	
Describe the system in detail.						

	Sectio	n C - Air Cleanin	g Devi	ce (Contir	nued)		
3. Inertial and Cyclone Col	lectors – A	I/A					
Manufacturer		Туре			Model No.		
Pressure Drop (in. of water)	Inlet Volu	me		Outlet Volu	me		
		ACFM @	°F	A	.CFM @	_°F	_% Moisture
Number of Individual Cyclone	(s)		Outlet	Straightening	Vanes Used?	☐ Yes	□ No
Length of Cyclone(s) Cylinder	ylinder (ft) Diameter of Cyclone		e(s) Cylin	(s) Cylinder Length of cyclone(s) cone (ft)		(ft)	
Inlet Diameter (ft) or Duct Area	a (ft²) of Cy	clone(s)	Outlet Diameter (ft) or Duct area (ft²) of cyclone(s)				
If a multi-clone or multi-tube unit is installed, will any of the individual cyclones or cyclone tubes be blanked or blocked off?					locked off?		
Describe any exhaust gas recirculation loop to be employed.							
Attach particle size efficiency curve							
Emission data		T					
Inlet		Ou	tlet		Remov	al Efficienc	sy (%)

	Section	ո C - Air Cleaning	g Device (Cont	inued)		
4. Fabric Collector – N/A						
<b>Equipment Specifications</b>						
Manufacturer			Model No.	☐ Pressurized Design ☐ Suction Design		
Number of Compartments		Number of Filters Per	Compartment	Is Baghouse Insulated?  ☐ Yes ☐ No		
Can each compartment be isolated for repairs and/or filter replacement?						
Are temperature controls provided? (Describe in detail)						
Dew point at maximum moiste	ure	°F   I	Design inlet volume	eSCFM		
Type of Fabric						
Material		Felted	☐ Membr	ane		
Weight	_ oz/sq.yd	☐ Woven	☐ Others:	: List:		
Thickness		☐ Felted-Wov	ven .			
Fabric permeability (clean) @			_CFM/sq.ft.			
Filter dimensions	Diam	neter/Width				
Effective area per filter				g temperature (°F)		
Effective air to cloth ratio Minimum Maximum						
Drawing of Fabric Filter  A sketch of the fabric filter showing all access doors, catwalks, ladders and exhaust ductwork, location of each pressure and temperature indicator should be attached.						
Operation and Cleaning						
Volume of gases handled °F		•	oss collector (in. of pment to be used to	water). o monitor the pressure drop.		
Type of filter cleaning  Manual Cleaning  Mechanical Shakers  Pneumatic Shakers	☐ Bag Collapse ☐ Reverse Air Jets ☐ Sonic Cleaning ☐ Other:					
If compressed air is required for collector operation, describe the equipment with the compressor to provide dry air free from oil.						
Cleaning Initiated By  Timer Frequency if timer actuated Expected pressure drop range in. of water  Other Specify						
Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If yes, describe.						
Describe the warning/alarm system that protects against operation when the unit is not meeting design requirements.						
Emissions Data						
Pollutant		Inlet	Outlet	Removal Efficiency (%)		
	1		ĺ			

	Section	C - Air Clea	ning Device (Contir	nued)	
5. Wet Collection Equipm	nent:- N/A				
Equipment Specifications					
Manufacturer		Туре		Model No	
Design Inlet Volume (SCFM	Design Inlet Volume (SCFM)  Relative Particulate/Gas Velocity (ejector scrubbers only)				
Describe the internal feature limiters, etc.).	res (e.g., varia	ble throat, gas/	liquid diffusion plates, s	pray nozzle	es, liquid redistributors, bed
Describe pH monitoring and	d pH adjustment	t systems, if app	licable.		
Describe mist eliminator or	separator (type,	configuration, b	packflush capability, frequ	iency).	
Attach particulate size effici	ency curve.				
Operating Parameters					
Inlet volume of gases hand	led	(ACFM)	Outlet volume of ga	ses handle	d (ACFM)
	@	°F	@	_ °F	% Moisture
Liquid flow rates. Describe equipment provided to measure liquid flow rates to scrubber (e.g., quenching section, recirculating solution, makeup water, bleed flow, etc.)					
Describe scrubber liquid supply system (amount of make-up and recirculating liquid, capacity of recirculating liquid system, etc).					
State pressure drop range (in water) across scrubber (e.g., venturi throat, packed bed, etc.) only. Describe the equipment provide to measure the pressure drop. Do not include duct or de-mister losses.					
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.					
Emissions Data					
Pollutant	li	nlet	Outlet		Removal Efficiency (%)

		Section C	- Air Cleanir	ng Device	(Contir	nued)	
6. Electrostati	c Precipitator –	N/A					
Equipment spe	cifications						
Manufacturer		N	Model No.			Wet Single-Stage	☐ Dry ☐ Two-Stage
Gas distribution grids  YES NO						F)	
Total collecting s	surface area	s	sq. ft. Collecto	or plates size	length	ft. x w	idth ft.
Number of fields	Num	ber of colle	ctor plates/field _	Sp	acing bet	ween collector p	latesinches.
Maximum gas ve	elocity		ft/sec.	Minimur	m gas trea	atment time:	sec.
Total discharge	electrode length		ft.				
Number of d	ischarge electroc	les		Numbei	r collectin	g electrode rappo	ers
Rapper control	Magr	etic	☐ Pneuma	tic	Other		
Describe in o	detail						
Operating para	meters						
Inlet gas temper	ature (°F)			State pressure drop range (water gauge) across collector			
Outlet gas temperature (°F) only. Describe the equipment.							
Volume of gas handled (ACFM)			Dust resist	Dust resistivity (ohm-cm). Will resistivity vary?			
Power requireme							
Number and size	e of Transformer	Rectifier set	s by electrical fie	eld	T	Each D	4 ! £ !
Field No.	No. of 6	<b>\</b> -4-	Each Tran		101	Each Ro	
Field No.	No. of S	bets	KV	A	NV.	Ave./Peak	MaDC
Current density		(	Corona power		•	Corona power	density
Mic	cro amperes/ft²	_	Watts	s/1000 ACFM	/1000 ACFMWatts/ft <sup>2</sup>		Watts/ft <sup>2</sup>
Will a flue gas co	onditioning syster	n be employ	yed? If yes, desc	cribe it.			
	0 ,		,				
Does air cleaning device employ hopper heaters, hopper vibrators or hopper level detectors? If yes, describe.							
Describe the wa	rning/alarm syste	m that prote	ects against oper	ation when u	nit is not	meeting design r	equirements.
Emissions data	a						
Pollu	tant	lı	nlet	Οι	ıtlet	Remo	oval Efficiency (%)

	Section C - Air Cleaning Device (Continued)					
7. Absorption Equipment:	· N/A					
Equipment specifications						
Manufacturer		Туре		1	Model No	
Design inlet volume (SCFM)			Tower height	(ft) and insid	de diameter (ft)	
Packing type and size (if applied	cable)		Height of pac	king (ft) (if a	pplicable)	
Number of trays (if applicable)			Number of bu	ıbble caps (i	f applicable)	
Configuration:	-current	☐ Cross	s flow	☐ Cocuri	rent flow	
Describe pH and/or other mon	itoring and	controls				
Absorbent information						
Absorbent type and concentra	tion	Sorbent injection rate		1	Retention time (sec)	
Attach equilibrium data for abs	orption (If a	applicable).				
					nix) supply system (once through or	
recirculating, system capacity, and recirculation.	etc) to tho	roughly evaluate t	he control equ	iipment. Ind	licate the flow rates for makeup, bleed	
Operating parameters						
Operating parameters				<u> </u>		
Volume of gas handled (ACFM	1)				e drop (in of water) and liquid flow rate. e the equipment.	
		Describe		Describe	; the equipment.	
State operating range for pH a	nd/or abso	rbent concentratio	n in scrubber l	iquid.		
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.						
Emissions data						
Pollutant		Inlet	Ou	ıtlet	Removal Efficiency (%)	

	Section C - Air Cle	eaning Device (Cont	inued)		
☐ SELECTIVE NON-CA	8. SELECTIVE CATALYTIC REDUCTION (SCR) – N/A  SELECTIVE NON-CATALYTIC REDUCTION (SNCR) – N/A  NON-SELECTIVE CATALYTIC REDUCTION (NSCR) – N/A				
Equipment specifications					
Manufacturer	Туре		Model No		
Design inlet volume (SCFM)		Design operating temp	perature (°F)		
Is the system equipped with period details.	process controls for prope	er mixing/control of the red	ducing agent in gas stream? If yes, give		
Attach efficiency and other pe	rtinent information (e.g., A	Ammonia, urea slip).			
Operating parameters					
Volume of gases handled (AC	FM) @(°	F)			
Operating temperature range	for the SCR/SNCR/NSCF	R system (°F)	From To		
Reducing agent used, if any.		Oxidation catalyst	Oxidation catalyst used, if any.		
State expected range of usag	e rate and concentration.				
Service life of catalyst		Ammonia slip (pp	m)		
Describe fully with a sketch giving locations of equipment, controls system, important parameters and method of operation.					
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.					
Emissions data					
Pollutant	Inlet	Outlet	Removal Efficiency (%)		

	Sectio	n C - Air Clea	ning Device (Contir	nued)			
9. Other Control Equipm	nent: <i>N/A</i>						
Equipment specifications	Equipment specifications						
Manufacturer		Туре		Model No			
Design inlet volume (SCFM	1)		Capacity				
Describe pH monitoring and	d pH adjustme	ent, if any.					
Indicate the liquid flow rate	and describe	equipment provid	led to measure pressure d	lrop and flow rate, if any.			
Attach efficiency curve and	or other effic	iency information					
Attach any additional data i	ncluding auxil	iary equipment a	nd operation details to tho	roughly evaluate the control equipment.			
Operating parameters							
Volume of gas handled							
@		_ °F % Mois	ture <i>(by volume)</i>				
Describe, in detail, important parameters and method of operation.							
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.							
Emissions data – N/A – T	he FGR is int	egral to the boil	er design.				
Pollutant	Inl	et	Outlet	Removal Efficiency (%)			

### **Section C - Air Cleaning Device (Continued)**

# 10. Costs – N/A Indicate cost associated with air cleaning device and its operating cost (attach documentation if necessary)

Device	Direct Cost	Indirect Cost	<b>Total Cost</b>	Operating Cos

#### 11. MISCELLANEOUS - N/A

Describe in detail the removal, handling and disposal of dust, effluent, etc. from the air cleaning device including proposed methods of controlling fugitive emissions.

Attach manufacturer's performance guarantees and/or warranties for each of the major components of the control system (or complete system).

Attach the maintenance schedule for the control equipment and any part of the process equipment that, if in disrepair, would increase air contaminant emissions.

	Section B - Combustion	on Unit Info	rmation	
2. Combustion Units: Coal Oil Natural Gas Other: Refinery Gas				
Description: Stripper Reboiler Heater H-124-02 (H02)				
Manufacturer  Tulsa Heaters, Inc.	Model No. N/A		Number of uni	ts
Maximum heat input (Btu/hr)  44.2 MMBtu/hr	Rated heat input (Btu/hr) 44.2 MMBtu/hr	Typical heat 44.2 MMBtu	input (Btu/hr) /hr	Furnace Volume 6,682 ft <sup>3</sup>
Grate Area (if applicable)  N/A  Method of firing  Natural draft				
Indicate how combustion air is s Natural draft	upplied to boiler			
Indicate the Steam Usage: N/A				
Mark and describe soot Cleaning	g Method: <b>N/A</b>			
<ul> <li>i. Air Blown</li> <li>ii. Steam Blown</li> <li>iii. Brushed and Vacuumed`</li> <li>iv. Other</li></ul>				
	Maximum Opera	ting schedu	ule	
		ays/Year		ours/Year <b>760</b>
Operational restrictions taken or	requested, if any (e.g., bottler	necks or volunt	tary restrictions	to limit potential to emit)
Capacity (specify units)				
		er week <b>,392.0 MMBt</b> u		er year <b>85,440 MMB</b> tu
	Typical Operati	ng schedul	е	
		ays/Year <b>65</b>		ours/Year <b>760</b>
Seasonal variations (Months): It			1 - 2	
Operating using primary fuel:		_ From		_ to
Operating using secondary fuel:	Гиона	_ Form		_ to
	From			-
3. Specify the primary, second Primary & Startup Fuel = F		ne details in ite	em 3.	

Section B - Combustion Unit Information (Continued)						
5. Fuel	5. Fuel					
Туре	Quantity Hourly	Annually	Sulfur	% Ash (Weight)	BTU Content	
Oil Number	GPH @ 60°F	X 10 <sup>3</sup> Gal	9/ by wt		Btu/Gal. & Lbs./Gal. @ 60 °F	
Oil Number	GPH @	X 10 <sup>3</sup>	% by wt		Btu/Gal. &	
	60°F	Gal	% by wt		Lbs./Gal. @ 60 °F	
Oil Number	GPH @ 60°F	X 10 <sup>3</sup> Gal	% by wt		Btu/Gal. & Lbs./Gal. @ 60 °F	
Natural Gas						
	SCFH	X 10 <sup>6</sup> Gal	gr/100 SCF		Btu/SCF	
Gas (other)		Gai	301			
, ,	SCFH	X 10 <sup>6</sup>	gr/100		Btu/SCF	
Coal		Gal	SCF			
Other* <i>Refinery Fuel</i>			<162 ppm (3-hr avg.) as H₂S			
Gas	27 225 00511	~ 3.26 E08	avy.) as H <sub>2</sub> S	Navioible	4 400 D4./CCE	
	~ 37,225 SCFH	SCF/YR	<50 ppm (12-	Negligible	~ 1,182 Btu/SCF	
			month rolling avg.) as H₂S			
			3,			
* Note: Describe ar	nd furnish informatio	n senarately for oth	per fuels in Addendur			
6. Burner	* Note: Describe and furnish information separately for other fuels in Addendum B.  6. Burner					
Manufacturer Callidus	Model <b>CUBL</b>	Number	Number Type of Atomization (Steam, air, pres			
Number of Burners	•		ng rate (all burners)	Normal fue		
If oil, temperature a	nd viscositv.	11.05 MMBtu/hr		7.66 MMB	tu/nr	
N/A						
Maximum theoretica  15% excess air	al air requirement					
Percent excess air	100% rating					
15%						
Turndown ratio 50%						
	ation control (on/off,	low-high fire, full a	utomatic, manual). D	escribe. <i>Manua</i>	al control	
Main burner flame i	gnition method (elec	ctric spark, auto gas	s pilot, hand-held tord	ch, other). Desc	cribe. <i>Natural gas pilot</i>	
5. Nitrogen Oxide	es (NO <sub>x</sub> ) control Op	otions				
	<u> </u>					
Mark and describe the NO <sub>x</sub> control options adopted						
☐ Low excess	air (LEA)	☐ Flue gas	recirculation	Other		
Over fire air	r (OFA)	☐ Burner ou	t of service			
⊠ Low-NO <sub>x</sub> bu	urner	Reburning	g			
Low NO <sub>x</sub> bu	urners with over fire	☐ Flue gas SNCR)	treatment (SCR /			

Section B - Combustion Unit Infor	mation (Continued)			
6. Miscellaneous Information				
Describe fly ash reinjection operation N/A				
Describe, in detail, the equipment provided to monitor and to record the emissions of air contaminants. Show that they are reasonable and ade				
Continuous Emission Monitoring Systems (CEMS) will measure NO <sub>x</sub> and O <sub>2</sub> through direct extraction. The heater will also be equipped with a fuel gas flow meter. Fuel gas will be supplied by the existing North Side Fuel Gas system which is already monitored for H <sub>2</sub> S and heating value (Btu/scf).				
Describe each proposed modification to an existing source.  N/A				
Describe how emissions will be minimized especially during start up, Provide emission estimates for start up, shut down and upset conditions				
Emissions will be minimized by operating the heater in accordance minimizing startup time.	e with manufacturer specifications and by			
Describe in detail with a schematic diagram of the control options adopt N/A	ed for SO <sub>2</sub> (if applicable).			
Anticipated milestones:				
Expected completion date of construction/reconstruction:	2016 2017 2017			

	Section C - Air Cleaning Device				
1. Precontrol Emission	ons* – <i>Not Available</i>	9			
Emission Rate					
		Maximum	Emission Rate		Calculation/
Pollutant	Specify Units	Pounds/Hour	Hours/Year	Tons/Year	Estimation Method
PM					
PM <sub>10</sub>					
SOx					
СО					
NO <sub>x</sub>					
VOC					
Others: (e.g., HAPs)					
* These emissions mus schedule for maximur values were determine	m limits or restricted	hours of operation	ed operating schedule and/or restricted thro		
2. Gas Conditioning -	- <b>N</b> /A				
Water quenching	YES NO	Water injection	n rate	GPM	
Radiation and convection	n cooling YES	□NO	Air dilution Y	S 🗌 NO	
			If YES,	CFM	
Forced draft	YES NO		Water cooled duct wo	rk YES	NO
Other					
Inlet volume			Outlet volume		
	ACFM@	°F	ACFM@	<sup>®</sup> °F	% Moisture
Describe the system in o	detail.	1			

	Section	on C - Air Cleanin	g Devi	ce (Contir	nued)		
3. Inertial and Cyclone Col	lectors – <i>N</i>	I/A					
Manufacturer		Туре			Model No.		
Pressure Drop (in. of water)	Inlet Volu	me		Outlet Volu	me		
		ACFM @	°F	A	CFM @	_°F	_% Moisture
Number of Individual Cyclone	(s)		Outlet	Straightening	Vanes Used?	☐ Yes	☐ No
Length of Cyclone(s) Cylinder	(ft)	Diameter of Cyclone	e(s) Cylir	nder	Length of cyclo	one(s) cone	(ft)
Inlet Diameter (ft) or Duct Area	a (ft²) of Cy	clone(s)	Outlet I	Diameter (ft)	or Duct area (ft²)	of cyclone	(s)
If a multi-clone or multi-tube u	nit is install	ed, will any of the indi	vidual cy	clones or cyc	clone tubes be bl	lanked or b	locked off?
Describe any exhaust gas recirculation loop to be employed.							
Attach particle size efficiency curve							
Emission data		T			T		
Inlet		Ou	tlet		Remova	al Efficienc	y (%)

	Section	C - Air Cleaning	g Device (Conti	inued)		
4. Fabric Collector – N/A						
<b>Equipment Specifications</b>						
Manufacturer			Model No.	☐ Pressuri	zed Design Design	
Number of Compartments	1	Number of Filters Per	Compartment	Is Baghouse	e Insulated?	
Can each compartment be iso	olated for repa	airs and/or filter repla	cement?	☐ Yes	□ No	
Are temperature controls prov	vided? (Descr	ibe in detail)		☐ Yes	□ No	
Dew point at maximum moistu	ure	°F	Design inlet volume	)	SCFM	
Type of Fabric  Material  Weight  Thickness  Fabric permeability (clean) @	_ oz/sq.yd in		ven .			
Filter dimensions			- '			
Effective area per filter	Effective area per filter Maximum operating temperature (°F)					
			Maximum			
Drawing of Fabric Filter A sketch of the fabric filter sand temperature indicator s			s, ladders and exh	aust ductwork	c, location of each pressure	
Operation and Cleaning						
Volume of gases handled ACFM °F		•	ross collector (in. of pment to be used to	,	oressure drop.	
Type of filter cleaning  Manual Cleaning  Mechanical Shakers Pneumatic Shakers		☐ Bag Collapse☐ Sonic Cleaning☐ Reverse Air Flow		Other: _	e Air Jets	
If compressed air is required from oil.	for collector	operation, describe	the equipment with	h the compre	ssor to provide dry air free	
Cleaning Initiated By  Timer Frequency if timer actuated  Expected pressure drop range in. of water Other Specify						
Does air cleaning device emp	oloy hopper h	eaters, hopper vibrat	ors or hopper level	detectors? If	yes, describe.	
Describe the warning/alarm s	ystem that pr	otects against opera	tion when the unit is	s not meeting	design requirements.	
<b>Emissions Data</b>						
Pollutant		Inlet	Outlet	R	emoval Efficiency (%)	
	1		1	ı		

	Section	C - Air Clea	ning Device (Contir	nued)		
5. Wet Collection Equipr	nent:- N/A					
Equipment Specifications	;					
Manufacturer		Туре		Model No		
Design Inlet Volume (SCFM	1)		Relative Particulate/Gas	Velocity (e	jector scrubbers only)	
Describe the internal feature limiters, etc.).	ires (e.g., varia	ble throat, gas/	liquid diffusion plates, s	pray nozzle	es, liquid redistributors, bed	
Describe pH monitoring and	d pH adjustmen	t systems, if app	licable.			
Describe mist eliminator or	separator (type	configuration, b	packflush capability, frequ	iency).		
Attach particulate size effici	ency curve.					
Operating Parameters						
Inlet volume of gases hand	Inlet volume of gases handled (ACFM) Outlet volume of gases handled (ACFM)					
	@	°F	@	_ °F	% Moisture	
Liquid flow rates. Describe equipment provided to measure liquid flow rates to scrubber (e.g., quenching section, recirculating solution, makeup water, bleed flow, etc.)						
Describe scrubber liquid supply system (amount of make-up and recirculating liquid, capacity of recirculating liquid system, etc).						
State pressure drop range (in water) across scrubber (e.g., venturi throat, packed bed, etc.) only. Describe the equipment provide to measure the pressure drop. Do not include duct or de-mister losses.						
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.						
Emissions Data						
Pollutant	lı	nlet	Outlet		Removal Efficiency (%)	

Section C - Air Cleaning Device (Continued)							
6. Electrostati	c Precipitator –	N/A					
Equipment spe	cifications						
Manufacturer		N	Model No.			Wet Single-Stage	☐ Dry ☐ Two-Stage
Gas distribution  YES	grids NO						F)
Total collecting s	surface area		sq. ft. Collecto	or plates size	length	ft. x w	ridth ft.
Number of fields	Num	ber of colle	ctor plates/field _	Sp	acing bet	ween collector p	latesinches.
Maximum gas ve	elocity		ft/sec.	Minimur	m gas trea	atment time:	sec.
	electrode length _						
Number of d	ischarge electrod	es		Number	r collectin	g electrode rappo	ers
Rapper control	Magn	etic	☐ Pneuma	tic	Other		
Describe in o	detail						
Operating para	meters						
	ature (°F)						gauge) across collector
Outlet gas tempe	Outlet gas temperature (°F) only. Describe the equipment.						
Volume of gas handled (ACFM) Dust resistivity (ohm-cm). Will resistivity vary?				tivity vary?			
Power requireme							
Number and size	e of Transformer	Rectifier set	ts by electrical fie	ld	1	Each D	4 i fi
Field No.	No. of C	<b>\</b> -4-	Each Tran				
Field No.	No. of S	ets	KV	Α	NV.	Ave./Peak	MaDC
Current density		(	Corona power			Corona power	density
Mic	cro amperes/ft²	_	Watts	s/1000 ACFM	1		Watts/ft <sup>2</sup>
Will a flue gas co	onditioning syster	n be employ	yed? If yes, desc	ribe it.			
, and the second	0 ,		, , ,				
Does air cleanin	g device employ	hopper heat	ters, hopper vibra	ators or hopp	er level d	etectors? If yes,	describe.
Describe the wa	rning/alarm syste	m that prote	ects against oper	ation when u	nit is not	meeting design r	requirements.
Emissions data	1						
Pollu	tant	I	nlet	Οι	ıtlet	Remo	oval Efficiency (%)

	Sectio	n C - Air Clear	ning Device	(Continu	ıed)
7. Absorption Equipment:	· N/A				
Equipment specifications					
Manufacturer		Туре		1	Model No
Design inlet volume (SCFM)			Tower height	(ft) and insid	le diameter (ft)
Packing type and size (if applied	cable)		Height of pack	king (ft) (if ap	oplicable)
Number of trays (if applicable)			Number of bu	ıbble caps (it	applicable)
Configuration:	-current	☐ Cross	s flow	☐ Cocurr	ent flow
Describe pH and/or other mon	itoring and	controls			
Absorbent information					
Absorbent type and concentra	tion	Sorbent injection	rate	F	Retention time (sec)
Attach equilibrium data for abs	orption (If a	applicable).			
Attach any additional information regarding auxiliary equipment, reagent (slurry mix) supply system (once through or recirculating, system capacity, etc) to thoroughly evaluate the control equipment. Indicate the flow rates for makeup, bleed and recirculation.					
Operating parameters					
Volume of gas handled (ACFM	1)	Inlet temperature	: (°F)	Pressure o	drop (in of water) and liquid flow rate.
	-,	mot tomporator	, ( . )		ne equipment.
State operating range for pH a	nd/or abso	rbent concentratio	n in scrubber l	iquid.	
Describe the warning/alarm sy	stem that p	protects against op	eration when u	unit is not m	eeting design requirements.
Emissions data					
Pollutant		Inlet	Ou	ıtlet	Removal Efficiency (%)

	Section C - Air Cle	aning Device (Conti	inued)			
☐ SELECTIVE NON-CA	TIC REDUCTION (SCR) - TALYTIC REDUCTION (S TALYTIC REDUCTION (N	NCR) – <i>N/A</i>				
Equipment specifications	1					
Manufacturer	Туре		Model No			
Design inlet volume (SCFM)		Design operating temp	perature (°F)			
Is the system equipped with p details.	process controls for prope	r mixing/control of the red	ducing agent in gas stream? If yes, give			
Attach efficiency and other pe	rtinent information (e.g., A	mmonia, urea slip).				
Operating parameters						
Volume of gases handled (AC	FM) @(°	F)				
Operating temperature range	for the SCR/SNCR/NSCR	system (°F)	From To			
Reducing agent used, if any.		Oxidation catalyst	used, if any.			
State expected range of usag	e rate and concentration.	·				
Service life of catalyst		Ammonia slip (ppi	m)			
Describe fully with a sketch giving locations of equipment, controls system, important parameters and method of operation.						
Describe the warning/alarm system that protects against operation when unit is not meeting design requirements.						
Emissions data	Emissions data					
Pollutant	Inlet	Outlet	Removal Efficiency (%)			

	Section	n C - Air Clea	ning Device (Contir	nued)
9. Other Control Equipm	ent: <i>N/A</i>			
Equipment specifications				
Manufacturer		Туре		Model No
Design inlet volume (SCFM	)		Capacity	
Describe pH monitoring and	l pH adjustme	nt, if any.		
Indicate the liquid flow rate	and describe e	equipment provid	ed to measure pressure of	drop and flow rate, if any.
Attach efficiency curve and/	or other effici	ency information		
Attach any additional data in	ncluding auxilia	ary equipment ar	nd operation details to tho	roughly evaluate the control equipment.
Operating parameters				
Volume of gas handled				
_		°F % Mois	ture (by volume)	
Describe, in detail, importar	t parameters a	and method of op	peration.	
Describe the warning/alarm	system that p	rotects against o	peration when unit is not i	meeting design requirements.
Emissions data – N/A – TI	ne FGR is inte	egral to the boil	er design.	
Pollutant	Inle	et	Outlet	Removal Efficiency (%)

#### **Section C - Air Cleaning Device (Continued)**

10. Costs - N/A				
Indicate cost associated	with air cleaning device	and its operating cost (attac	ch documentation if neces	ssary)
Device	Direct Cost	Indirect Cost	Total Cost	Operating Cost
11. MISCELLANEOUS -	- N/A	1	<u> </u>	
Describe in detail the ren methods of controlling fug		oosal of dust, effluent, etc.	from the air cleaning dev	ice including proposed
Attach manufacturer's per (or complete system).	erformance guarantees	and/or warranties for each	of the major components	s of the control system
Attach the maintenance s	schedule for the control	equipment and any part of t	the process equipment th	at, if in disrepair,
would increase air contar		71		, ,

	Section D - Additional Information		
the	Il the construction, modification, etc. of the sources covered by this application increase emiss facility? If so, describe and quantify.  e Attachment A – Application Narrative.	sions from othe	r sources at
16.4		20 8 11	
If t	his project is subject to any one of the following, attach a demonstration to show compliance v	vith applicable	standards
a.	Prevention of Significant Deterioration permit (PSD), 40 CFR Part 52?	☐ YES	⊠ NO
b.	New Source Review, 25 Pa. Code Chapter 127, Subchapter E?		□ NO
c.	New Source Performance Standards, 40 CFR Part 60? (If Yes, which subpart) <i>Ja</i>		□ NO
d.	National Emissions Standards for Hazardous Air Pollutants (NESHAPS), 40 CFR Part 61? If Yes, which subpart)	☐ YES	⊠ NO
e.	Maximum Achievable Control Technology (MACT), 40 CFR Part 63? (If Yes, which subpart) <b>DDDDD</b>	⊠ YES	□ NO
	ach a demonstration showing that the emissions from any new source will be the minimum a st available technology (BAT).	ttainable throu	gh the use of
Se	e Attachment A – Application Narrative.		
	ovide emission increases and decreases in allowable (or potential) and actual emissions plicable PSD pollutant(s) if the facility is an existing major facility (for PSD purposes)	within the las	t 5 years for
Se	e Attachment C – Emissions Inventory		

#### Section D - Additional Information (Continued)

Indicate emission increases and decreases in tons per year (tpy), for volatile organic compounds (VOCs) and nitrogen oxides (NOx) for NSR applicability since January 1, 1991 or other applicable dates (See other applicable date in instructions). The emissions increases include all emissions including stack, fugitive, material transfer, other emission generating activities, quantifiable emissions from the exempted source(s), etc.

		Indicate Yes		VC	<b>C</b> s	N	Ox
Permit number (if applicable)	Date issued	or <b>No</b> if emission increases and decreases were used previously for netting	Source I.D. or Name	Emission increases in potential to emit (tpy)	Creditable emission decreases in actual emissions (tpy)	Emission increases in potential to emit (tpy)	Creditable emission decreases in actual emissions (tpy)
αρριιοασίο)	100000	noung	Course I.D. or Italie	(47)	(127)	(423)	(12)
					<u> </u>		
		Se	ee Attachment C – Emissio	ns Inventor	y		
		,					
_							

If the source is subject to 25 Pa. Code Chapter 127, Subchapter E, New Source Review requirements, **See Attachment A – Application Narrative.** 

- Identify Emission Reduction Credits (ERCs) for emission offsets or demonstrate ability to obtain suitable ERCs for emission offsets.
- b. Provide a demonstration that the lowest achievable emission rate (LAER) control techniques will be implemented (if applicable).
- c. Provide an analysis of alternate sites, sizes, production processes and environmental control techniques demonstrating that the benefits of the proposed source outweigh the environmental and social costs (if applicable).

Attach calculations and any additional information necessary to thoroughly evaluate compliance with all the applicable requirements of 25 Pa. Code Article III and applicable requirements of the Clean Air Act and regulations adopted there under. The Department may request additional information to evaluate the application such as a stand by plan, a plan for air pollution emergencies, air quality modeling, etc.

See Attachment C - Emissions Inventory.

Section E - Compliance Demonstration – N/A
Note: Complete this section if the facility is not a <u>-Title V facility</u> . Title V facilities must complete Addendum A.
Method of Compliance Type: Check all that apply and complete all appropriate sections below.
<ul> <li>☐ Monitoring</li> <li>☐ Testing</li> <li>☐ Reporting</li> <li>☐ Recordkeeping</li> <li>☐ Work Practice Standard</li> </ul>
Monitoring:
a. Monitoring device type (stack test, CEM etc.):
b. Monitoring device location:
c. Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:
Testing:
a. Reference Test Method Citation:
b. Reference Test Method Description:
Recordkeeping:
Describe the parameters that will be recorded and the recording frequency:
Reporting:
a. Describe the type of information to be reported and the reporting frequency:
b. Reporting start date:
Work Practice Standard: Describe each

Section F - Flue and Air Contaminant Emission									
1. Estimated Maximum Emissions*									
	Maximum emission rate  Calculation/						culation/		
Pollutant	specify unit		its lbs/hr		r	ton	ıs/yr.		tion Method
PM									
PM <sub>10</sub>									
SO <sub>x</sub>									
СО		See	Attachm	ent C – E	missio	ns Inventory	<i>y</i>		
NO <sub>x</sub>									
VOC									
Others: ( e.g., HAPs)									
* These emissions must schedule for maximum values were determine	limits o	r restric	ted hours						
2. Stack and Exhaus	ster								
Stack Designation/Numb	oer <i>PAD</i>	EP to a	ssign						
List Source(s) or source ID exhausted to this stack:  ### 64									
Stack height above grade (ft.) 150' 4" Stack diame Grade elevation (ft.) ~ 10 feet 5' 2"				er (ft) o	or Outlet duct	area (sq. ft.)		ther Cap ES 🔲 NO	
Distance of discharge to	Distance of discharge to nearest property line (ft.). Locate on topographic map.								
~ 600 - 1,000 feet									
Does stack height meet Good Engineering Practice (GEP)?  N/A									
If modeling (estimating) of ambient air quality impacts is needed, attach a site plan with buildings and their dimensions and other obstructions. <b>N/A</b>									
Location of Stack**			Latitude				Longitude		e
Latitude/Longitude									
Point of Origin			Degree	es Min	utes	Seconds	Degrees	Minutes	Seconds
Stack Exhaust									
Volume <u>~29,316</u> ACFM Temperature <u>450</u> °F Moisture <u>15</u> %									
Exhauster (attach fan curves) <u><b>N/A</b></u> in. of water <u><b>N/A</b></u> HP @ <u><b>N/A</b></u> RPM.									
** If the datum and collection method information and codes differ from those provided on the General Information Form - Authorization Application, provide the additional required by that form on a separate sheet.									

2. Stack and Exhauster							
Stack Designation/Number PADEP to assign							
List Source(s) or source ID exhausted to this stack:  H02				% of flow exhausted to stack: 100%			
Stack height above grade (ft.) 115' 3.5"  Grade elevation (ft.) ~ 10 feet  Stack diameter 3' 4"			er (ft) o	er (ft) or Outlet duct area (sq. ft.)  Weather Cap  YES			•
Distance of discharge to nearest propert	ty line (ft.). L	ocate or	n topog	raphic map.			
~600 - 1,000 feet							
Does stack height meet Good Engineering Practice (GEP)?  N/A							
If modeling (estimating) of ambient air of and other obstructions. <b>N/A</b>	quality impac	ts is ne	eded, a	attach a site p	lan with build	ings and the	ir dimensions
Location of Stack**		Latit	ude			Longitude	
Latitude/Longitude							
Point of Origin	Degrees	Minu	utes	Seconds	Degrees	Minutes	Seconds
Stack Exhaust           Volume							
Exhauster (attach fan curves) <u>N/A</u> in. of water <u>N/A</u> HP @ <u>N/A</u> RPM.							
** If the datum and collection method information and codes differ from those provided on the General Information Form - Authorization Application, provide the additional required by that form on a separate sheet.							

# **Section G - Attachments** Number and list all attachments submitted with this application below: Attachment A – Application Narrative Attachment B - PADEP Application Forms Attachment C – Emissions Inventory Attachment D - Municipal Notification Letters Attachment E - All4 Inc. Quality Seal



#### **Addendum A: Source Applicable Requirements**

Describe and cite all applicable requirements pertaining to this source.

Note: A Method of Compliance Worksheet (Addendum 1) must be completed for each requirement listed.

Citation Number	Citation Limitation	Limitation Used
40 CFR §60.102a(g)(1)(ii)	Monroe shall not burn in any fuel gas combustion device, any fuel gas that contains H <sub>2</sub> S in excess of 162 ppmv determined on a 3-hour rolling average basis and 50 ppmv determined on a 12-month rolling average basis.	$H_2S$ fuel limitations as required in $\S60.102a(g)(1)(ii)$ .
40 CFR §60.102a(g)(2)(i)(B)	The emissions of $NO_X$ from the two (2) heaters will be limited to 0.040 lb/MMBtu at high heat release rate, determined on a 30-day rolling average.	$NO_X$ emissions limitations as required in $\S60.102a(g)(2)(i)(B)$ .
40 CFR §60.103a(c)(2)	Monroe will conduct a root cause analysis and a corrective action analysis for the process heaters for each instance indicated.	Conditions as specified in §60.102a(c)(2).
40 CFR §60.104a(a)	Monroe will conduct a NO <sub>X</sub> performance test of the new process heaters no later than 60 days after achieving maximum production rate or 180 days after initial startup, whichever comes first.	Performance testing as required in §60.104a(a).
40 CFR §60.107a(a)(2)  Monroe shall install, operate, calibrate and maintain a device to continuously monitor fuel gas H <sub>2</sub> S content.		Monitoring of fuel gas $H_2S$ content and operations for fuel gas combustion device and flares as specified in $60.107a(a)(2)$ .
40 CFR §60.107a(d)	Monroe shall install, operate, calibrate and maintain a device to continuously monitor the emissions rate of NO <sub>X</sub> into the atmosphere.	Monitoring of $NO_X$ emissions and operations for process heaters as specified in 40 CFR §60.107a(d).

Citation Number	Citation Limitation	Limitation Used
40 CFR §60.108a(b)	Monroe will notify the administrator of the specific monitoring provisions of \$60.106a for which Monroe intends to comply. This notification will be submitted with the notification of initial startup required by \$60.7(a)(3).	Notifications as required in §60.108a(b).
40 CFR §60.108a(c)	Monroe will maintain records of excess emissions. Monroe will record the required information no later than 45 days following the end of a discharge exceeding this threshold.	Records as required in 40 CFR §60.108a(c).
40 CFR §60.108a(d)	Monroe will submit semiannual excess emission reports containing the required information.	Excess emission reporting as specified in §60.108a(d).
40 CFR §63.7500(a)(3)	Monroe will operate and maintain the heaters in a manner consistent with safety and good air pollution control practices for minimizing emissions.	Compliance with work practice standards.
40 CFR §63.7510(e) and §63.7510(j)	Monroe will complete the one-time energy assessment specified in the Work Practice Standards of Table 3.	Compliance with initial requirements as required in §63.7510(e) and §63.7510(j)
40 CFR §63.7540(a)(10)	Monroe will meet the Work Practice Standards of Table 3 which include annual tune ups. The tune-ups will contain the required elements listed in §63.7540(a)(10). Tune-up reports will be maintained on site and submitted to the Administrator, if requested. The tune-up reports will contain the information required in §63.7540(a)(10)(vi)(A) through (C).	Compliance with continuous requirements as required in §63.7540(a)(10)
40 CFR §63.7550	Monroe will submit all compliance reports in accordance with 40 CFR §63.7550.	Compliance reports as required in 40 CFR §63.7550.
40 CFR §63.7560	Monroe will keep all required records on-site for at least two (2) years, and off-site for at least five (5) years.	Recordkeeping requirements as required in 40 CFR §63.7560.

Citation Number	Citation Limitation	Limitation Used
25 Pa. Code §§123.1 & 123.2	No fugitive emissions and no fugitive particulate emissions beyond the property line.	No fugitive emissions and no fugitive particulate emissions beyond the property line.
25 Pa. Code §§123.11 & 123.13	Particulate emission from process heater H-01 must remain under 0.27 lb/MMBtu, calculated using the equation 3.6E <sup>-0.56</sup> , where E represents the heat input to the boiler in MMBtu/hr, when E is equal to or greater than 50 but less than 600. Particulate emission from process heater H-02 must remain under 0.40 lb/MMBtu.	N/A
25 Pa. Code §123.22	SO <sub>2</sub> emissions are not to exceed more than 1.0 lb/MMBtu of SO <sub>2</sub> per hour.	N/A
25 Pa. Code §123.41	Visible emissions no greater than 20% for a period aggregating more than 3 minutes in any 1 hour or no greater than or equal to 60% at any one time.	No visible emissions greater than 20% for a period aggregating more than 3 minutes in any 1 hour or no greater than or equal to 60% at any one time
25 Pa. Code §127.12(a)(5)	Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), proper design, operation and good combustion and engineering practices as BAT for CO emissions.	CO BAT
25 Pa. Code §127.12(a)(5)	Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), proper design, operation and good combustion and engineering practices as BAT for VOC emissions.	VOC BAT
25 Pa. Code §127.12(a)(5)	Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning) and the application of low $NO_X$ burners and a $NO_X$ emission rate of 0.035 lb/MMBtu (30-day rolling average).	NO <sub>X</sub> BAT

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Citation Number	Citation Limitation	Limitation Used
25 Pa. Code §127.12(a)(5)	Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), and an emission rate for SO <sub>2</sub> to be <162 ppm H <sub>2</sub> S (3-hr average) and 50 ppm (12-month rolling average) in fuel gas, for BAT for SO <sub>2</sub> .	SO <sub>2</sub> BAT
25 Pa. Code §127.12(a)(5)	Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and annual combustion tuning), proper design, operation and good combustion and engineering practices as BAT for PM emissions.	PM BAT



SEC	SECTION 1. APPLICABLE REQUIREMENT							
Fede	eral Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC				
Plan	t Code:	45-5201144	Plant Name:	Trainer Refinery, PA				
Appl	Applicable Requirement for: (please check only one box below)							
	The entire s	ite						
	A group of s	ources, Group ID	Proposed 1	Process Heaters (H-01 and H-02)				
	A single sou	ırce, Unit ID:						
	Alternative S	Scenario, Scenar	io Name:					
	Citation #: $40 \ CFR \ \S 60.102a(g)(1)(ii)$ Compliance Method based upon: $\square$ Applicable Requirement $\square$ Gap Filling Requirement							
Method of Compliance Type: (Check all that applies and complete all appropriate sections below)  ☑ Monitoring ☐ Testing ☑ Reporting  ☑ Record Keeping ☐ Work Practice Standard								
Section 2: Monitoring								
1. Monitoring device type (stack test, CEM, etc.): $H_2S$ CEMS.								
2. N	2. Monitoring device location: Downstream of the North Side Fuel Gas Mix Pot							
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:								
Refinery fuel gas is continuously monitored for the H <sub>2</sub> S concentration on an hourly basis to demonstrate compliance on a 3-hour rolling average basis.								

3. How will data be reported: N/A						
Section 3: Testing						
1. Reference Test Method Description: $N/A$						
2. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording:						
$H_2S$ concentration in the refinery fuel gas. Data are averaged in accordance with 40 CFR Part 60, Subpart						
Ja and PADEP's Continuous Source Monitoring Manual, Revision 8.						
<u></u>						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
Monroe will submit reports of H <sub>2</sub> S monitoring data on a quarterly basis in accordance with 40 CFR Part						
60, Subpart Ja and PADEP's Continuous Source Monitoring Manual, Revision 8.						
3. Reporting start date: Already ongoing						
Section 6: Work Practice Standard						
Describe any work practice standards:						
<u>N/A</u>						



SEC	SECTION 1. APPLICABLE REQUIREMENT						
Fede	ral Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC			
Plant	t Code:	45-5201144	Plant Name:	Trainer Refinery, PA			
Appl	Applicable Requirement for: (please check only one box below)						
	The entire si	te					
	A group of s	ources, Group ID:	Proposed Pro	cess Heaters (H-01 and H-02)			
	A single sou	rce, Unit ID:					
	Alternative S	Scenario, Scenario	o Name:				
Citat	ion #: 40 C	FR §60.102a(g)(2	(2)(i)(B)				
Com	pliance Metho	od based upon:	Applicabl	e Requirement Gap Filling Requirement			
Meth	od of Compli	ance Type: (Chec	k all that applies	and complete all appropriate sections below)			
$\boxtimes$							
	Record Keeping Work Practice Standard						
Section 2: Monitoring							
4. Monitoring device type (stack test, CEM, etc.): $NO_X CEMS$							
5. N	5. Monitoring device location: Stack						
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							
	Stack exhaust is continuously monitored for the $NO_X$ emission rates on an hourly basis to demonstrate compliance on a 30-day rolling average.						

6. How will data be reported: $N\!/\!A$						
Section 3: Testing						
4. Reference Test Method Description: N/A						
5. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording:						
$NO_X$ emission rates will be monitored and averaged in accordance with 40 CFR Part 60, Subpart Ja and						
PADEP's Continuous Source Monitoring Manual, Revision 8.						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
Monroe will submit $NO_X$ data reports on a quarterly basis.						
6. Reporting start date:  The end of the calendar quarter in which the unit(s) first start up						
Section 6: Work Practice Standard						
Describe any work practice standards:						
$N\!/\!A$						



SECTIO	SECTION 1. APPLICABLE REQUIREMENT							
Federal	Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC				
Plant Co	ode:	45-5201144	Plant Name:	Trainer Refinery, PA				
Applicat	Applicable Requirement for: (please check only one box below)							
Th	e entire si	te						
A group of sources, Group ID: Proposed Process Heaters (H-01 and H-02)								
A s	single sou	rce, Unit ID:						
Alt	ternative S	Scenario, Scenario	o Name:					
Citation	Citation #: $40 \ CFR \ \S 60.103 a(c)(2)$							
Complia	nce Metho	od based upon:	Applica	able Requirement Gap Filling Requirement				
Method of Compliance Type: (Check all that applies and complete all appropriate sections below)								
	Monitorin	g	Testing	Reporting				
	Record Keeping Work Practice Standard							
Section 2: Monitoring								
1. Moni	itoring dev	vice type (stack te	st, CEM, etc.):	N/A				
2. Moni	itoring dev	vice location:	N/A					
Describe	Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							

3. How will data be reported: N/A						
Section 3: Testing						
Reference Test Method Description:	N/A					
2. Reference Test Method Citation:	N/A					
Section 4: Record Keeping						
Describe what parameters will be recorded a	nd the frequency of recording:					
N/A						
Section 5: Reporting						
Describe what is to be reported and the frequ	uency of reporting:					
N/A						
3. Reporting start date:						
Section 6: Work Practice Standard						
Describe any work practice standards:						
Monroe will conduct a root cause analysis and a corrective action analysis for the process heaters for each						
instance specified in 40 CFR $\S60.103a(c)(2)$ .						



SECTION 1. APPLICABLE REQUIREMENT					
Federal Tax Id: 45-52	01144	Firm Name:	Monroe Energy, LLC		
Plant Code: <u>45-52</u>	01144	Plant Name:	Trainer Refinery, PA		
Applicable Requirement for: (please check only one box below)					
The entire site					
A group of sources	, Group II	D: Proposed	Process Heaters (H-01	and H-02)	
A single source, Un	it ID:				
Alternative Scenario	o, Scena	rio Name:			
Citation #: 40 CFR §60	Citation #: 40 CFR §60.104a(a)				
Compliance Method base	ed upon:	Appli	cable Requirement	Gap Filling Requirement	
Method of Compliance Type: (Check all that applies and complete all appropriate sections below)					
Monitoring		Testing		Reporting	
Record Keeping		Work Practi	ce Standard		
Section 2: Monitori	ing				
4. Monitoring device typ	e (stack	test, CEM, etc.)	: N/A		
5. Monitoring device loc	ation:	N/A			
Describe all parameters b	eing mo	nitored along w	rith the frequency and d	uration of monitoring each parameter:	

6. How will data be reported: N/A	
Section 3: Testing	
4. Reference Test Method Description:	Conduct a $NO_X$ performance test of the new process heaters no later than 60 days after achieving maximum production rate or 180 days after initial startup, whichever comes first.
5. Reference Test Method Citation:	Method 7, 7A, 7C, 7D, or 7E of appendix A-4 to 40 CF Part 60 for moisture content and for the emission rate of NOX calculated as nitrogen dioxide (NO <sub>2</sub> ).
Section 4: Record Keeping	
Describe what parameters will be record	ed and the frequency of recording:
·	ou and modulinoy of rocording.
•	
N/A  Section 5: Reporting	
N/A  Section 5: Reporting  Describe what is to be reported and the t	
N/A  Section 5: Reporting  Describe what is to be reported and the t	requency of reporting:
N/A  Section 5: Reporting  Describe what is to be reported and the the Monroe will report the results of the N	requency of reporting:
N/A  Section 5: Reporting  Describe what is to be reported and the the Monroe will report the results of the N  6. Reporting start date:	requency of reporting:  Ox performance test as required by 40 CFR Part 60, Subpart A.
N/A  Section 5: Reporting  Describe what is to be reported and the the Monroe will report the results of the N  6. Reporting start date:	requency of reporting:  Ox performance test as required by 40 CFR Part 60, Subpart A.



SEC	SECTION 1. APPLICABLE REQUIREMENT				
Fede	ral Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC	
Plant	t Code:	45-5201144	Plant Name:	Trainer Refinery, PA	
Appli	icable Requir	ement for: (pleas	se check only o	ne box below)	
	The entire si	te			
	A group of s	ources, Group ID	Proposed I	Process Heaters (H-01 and H-02)	
	A single sou	ırce, Unit ID:			
	Alternative S	Scenario, Scenar	io Name:		
Citati	ion #: 40 C	FR §60.107a(a)	(2)		
Com	pliance Metho	od based upon:	Applic	able Requirement Gap Filling Requirement	
Meth	Method of Compliance Type: (Check all that applies and complete all appropriate sections below)				
$\boxtimes$	Monitorin	ig	Testing	Reporting	
	Record Keeping Work Practice Standard				
Section 2: Monitoring					
7. N	7. Monitoring device type (stack test, CEM, etc.): $H_2S$ CEMS				
8. N	8. Monitoring device location: Downstream of North Side Fuel Gas Mix Pot				
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:					
Refin	Refinery fuel gas is continuously monitored for the H <sub>2</sub> S concentration.				

9. How will data be reported: N/A	
Section 3: Testing	
7. Reference Test Method Description:	N/A
8. Reference Test Method Citation:	N/A
Section 4: Record Keeping	
Describe what parameters will be recorded	and the frequency of recording:
H <sub>2</sub> S concentrations will be monitored an	d averaged in accordance with 40 CFR Part 60, Subpart Ja and
PADEP's Continuous Source Monitoring	g Manual, Revision 8.
Section 5: Reporting	
Describe what is to be reported and the fre	quency of reporting:
N/A	
9. Reporting start date:	
Section 6: Work Practice Standard	d
Describe any work practice standards:	
N/A	



SECTION 1. APPLICABLE REQUIREMENT					
Fede	eral Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC	
Plan	t Code:	45-5201144	Plant Name:	Trainer Refinery, PA	
Appl	icable Requir	ement for: (plea	se check only	one box below)	
	The entire si	ite			
	A group of sources, Group ID: Proposed Process Heaters (H-01 and H-02)				
	A single sou	ırce, Unit ID:			
	Alternative \$	Scenario, Scena	rio Name:		
Citat	ion #: 40 C	EFR §60.107a(d	)		
Com	Compliance Method based upon:  Applicable Requirement  Gap Filling Requirement				
Method of Compliance Type: (Check all that applies and complete all appropriate sections below)					
Moti	ou or compil	unoc Type. (On	on an mar app	nes and complete an appropriate sections select;	
$\boxtimes$	Monitoring Testing Reporting				
	Record Keeping Work Practice Standard				
Section 2: Monitoring					
10. Monitoring device type (stack test, CEM, etc.): $NO_X$ and $O_2$ CEMS					
11. N	Monitoring de	vice location:	Stack		
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:					
Stack exhaust is continuously monitored for the $NO_X$ emission rates (30-day rolling average) and $O_2$ concentrations.					

12. How will data be reported:	Data will be reported electronically to PADEP in accordance with the Continuous Source Monitoring Manual, Revision 8.			
Section 3: Testing				
10. Reference Test Method Descr	iption: N/A			
11. Reference Test Method Citation	on: N/A			
Section 4: Record Keeping	$oldsymbol{g}$			
Describe what parameters will be	recorded and the frequency of recording:			
NO <sub>X</sub> emission rates and O <sub>2</sub> cond	centrations will be monitored and averaged in accordance with 40 CFR Part			
60, Subpart Ja and PADEP's Co	ontinuous Source Monitoring Manual, Revision 8.			
Section 5: Reporting				
Describe what is to be reported a	nd the frequency of reporting:			
N/A				
12. Reporting start date:				
Section 6: Work Practice Standard				
Describe any work practice standards: $N\!/\!A$				



SECTION 1. APPLICABLE REQUIREMENT				
Federal Tax Id:	<i>45-5201144</i> F	Firm Name:	Monroe Energy, LLC	•
Plant Code:	45-5201144 F	Plant Name:	Trainer Refinery, PA	
Applicable Requ	irement for: (plea	ise check only	one box below)	
The entire	site			
A group o	sources, Group II	D: Propose	d Process Heaters (H-	01 and H-02)
A single s	ource, Unit ID:			
Alternativ	Scenario, Scena	rio Name:		
Citation #: 40	CFR §60.108a(b)	)-(d)		
Compliance Me	hod based upon:	App	olicable Requirement	Gap Filling Requirement
Method of Com	oliance Type: (Che	eck all that ap	plies and complete all a	appropriate sections below)
Monito	ring	Testing		Reporting
Record	Keeping	Work Prac	tice Standard	
Section 2: Monitoring				
1. Monitoring	levice type (stack t	test, CEM, etc	:.): N/A	
2. Monitoring device location: N/A				
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:				
3. How will dat	a be reported: $N_{i}$	// <b>A</b>		

Section 3:	resting					
1. Reference T	est Method Description:	N/A				
2. Reference T	est Method Citation:	N/A				
Section 4:	Record Keeping					
Describe what p	parameters will be recorded	and the frequency of recording:				
Monroe will me	aintain the records requir	ed by §60.108a(c) and record all periods of excess emissions.				
Section 5:	Reporting					
Describe what i	s to be reported and the fre	equency of reporting:				
Monroe will su	Monroe will submit the specific monitoring provisions for which Monroe intends to comply. Monroe will					
submit a semia	submit a semiannual excess emissions report for all periods of excess emissions. Monroe will submit					
notification of	the actual date of initial s	tartup within 15 days after such date.				
3. Reporting s	tart date: At the end of occurs.	the semi-annual reporting period in which the ULSG startup				
Section 6: Work Practice Standard						
Describe any work practice standards:						
N/A						



SECTION 1. APPLICABLE REQUIREMENT						
Federal	l Tax ld:	45-5201144	Firm Name:	Monroe Energy, LLC		
Plant Co	ode:	45-5201144	Plant Name:	Trainer Refinery, PA		
<ul><li>□ Th</li><li>□ A</li></ul>	Applicable Requirement for: (please check only one box below)  The entire site  A group of sources, Group ID:   Proposed Process Heaters (H-01 and H-02)					
A	single sou	ırce, Unit ID:				
AI	Iternative S	Scenario, Scena	rio Name:			
Citation	n#: <u>40 C</u>	FR §63.7500(a	)(3)			
Complia	Compliance Method based upon: Applicable Requirement Gap Filling Requirement					
Method	Method of Compliance Type: (Check all that applies and complete all appropriate sections below)  Monitoring Testing Reporting					
	Record K	_	_	tice Standard		
Sectio	Section 2: Monitoring					
1. Monitoring device type (stack test, CEM, etc.): $N/A$						
2. Mor	2. Monitoring device location: N/A		N/A			
Describ	Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:					

3. How will data be reported: $N/A$
Section 3: Testing
1. Reference Test Method Description: N/A
2. Reference Test Method Citation: N/A
Section 4: Record Keeping
Describe what parameters will be recorded and the frequency of recording: $N\!/\!A$
Section 5: Reporting
Describe what is to be reported and the frequency of reporting:
N/A
3. Reporting start date:
Section 6: Work Practice Standard
Describe any work practice standards:
Monroe will operate and maintain the heaters in a manner consistent with safety and good air pollution
control practices for minimizing emissions.



SECTION 1. APPLICABLE REQUIREMENT					
Federal Tax I	d:	45-5201144	Firm Name:	Monroe Energy, LLC	
Plant Code:		45-5201144	Plant Name:	Trainer Refinery, PA	
Applicable Ro	equir	rement for: (plea	ase check only	one box below)	
The ent	ire s	ite			
	o of s	sources, Group	ID: Proposed	Process Heaters (H-01 and H-02)	
A single	e sou	ırce, Unit ID:			
Alterna	tive	Scenario, Scena	ario Name:		
Citation #:	40 C	CFR §§63.7510	(e) and 63.7510	O(j)	
Compliance I	Compliance Method based upon:  Applicable Requirement  Gap Filling Requirement				
Method of Co	Method of Compliance Type: (Check all that applies and complete all appropriate sections below)				
Mon	Monitoring Testing Reporting				
Reco	ord K	Geeping 🔀	Work Practi	ce Standard	
Section 2: Monitoring					
4. Monitoring device type (stack test, CEM, etc.): N/A					
5. Monitorin	g de	vice location:	N/A		
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:					

6. How will data be reported: N/A						
Section 3: Testing						
4. Reference Test Method Description: N/A						
5. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording:						
N/A						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
N/A						
6. Reporting start date:						
Section 6: Work Practice Standard						
Describe any work practice standards:						
Monroe will complete the one-time energy assessment specified in the Work Practice Standards of Table 3.						



SECTION 1. APPLICABLE REQUIREMENT							
Federal Tax Id: 45-5201144 Firm Name: Monroe Energy, LLC							
Plant Code:		45-5201144	Plant Name:	Trainer Refinery,	PA		
Applicable F	Applicable Requirement for: (please check only one box below)						
The er	ntire si	te					
A grou	up of s	ources, Group I	D: Proposed P	rocess Heaters (H-0	01 and H-02)		
A sing	le sou	rce, Unit ID:					
Altern	ative S	Scenario, Scena	rio Name:				
Citation #:	40 C	FR §63.7540(a	)(10)				
Compliance	Compliance Method based upon: Applicable Requirement Gap Filling Requirement						
Method of C	ompli	ance Type: (Ch	eck all that applie	s and complete all a	ppropriate sections below)		
<u></u> Мо	nitorin	g 🗌	Testing		Reporting		
Red	Record Keeping Work Practice Standard						
Section 2: Monitoring							
7. Monitoring device type (stack test, CEM, etc.): N/A							
8. Monitori	8. Monitoring device location: N/A						
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							

9. How will data be reported: $N/A$						
Section 3: Testing						
7. Reference Test Method Description: N/A						
8. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording:						
Monroe will maintain records of annual tune-ups performed on the proposed process heaters.						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
N/A						
9. Reporting start date:						
Section 6: Work Practice Standard						
Describe any work practice standards:						
Monroe will perform annual tune-ups of the proposed process heaters.						



SECTION 1. APPLICABLE REQUIREMENT							
Fede	Federal Tax Id: 45-5201144 Firm Name: Monroe Energy, LLC						
Plant	Plant Code: 45-5201144 Plant Name: Trainer Refinery, PA						
Appli	cable Requir	ement for: (plea	se check only	one box below)			
	•						
Ш	The entire s	ite					
	A group of s	sources, Group I	D: Proposed	Process Heaters (H-01 and H-02)			
	A single sou	ırce, Unit ID:					
	Alternative	Scenario, Scena	rio Name:				
Citati	Citation #: 40 CFR §63.7550						
Comp	Compliance Method based upon:   Applicable Requirement   Gap Filling Requirement						
Metho	od of Compli	ance Type: (Che	eck all that app	lies and complete all appropriate sections below)			
	Monitorir	ng 🗌	Testing	Reporting			
Record Keeping Work Practice Standard							
Section 2: Monitoring							
10. Monitoring device type (stack test, CEM, etc.): N/A							
11. M	11. Monitoring device location: N/A						
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							

12. How will data be reported: N/A						
Section 3: Testing						
10. Reference Test Method Description: N/A						
11. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording: $N\!/\!A$						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
Monroe will submit all compliance reports as required in accordance with 40 CFR §63.7550.						
12. Reporting start date:						
Section 6: Work Practice Standard						
Describe any work practice standards:						
N/A						



SECTION 1. APPLICABLE REQUIREMENT								
Federal Ta	x ld:	45-5201144	Firm Name:	Monroe Energy, LL	C			
Plant Code	e:	45-5201144	Plant Name:	Trainer Refinery, P.	A			
Applicable	Applicable Requirement for: (please check only one box below)							
The	entire s	ite						
A gr	oup of s	ources, Group ID	: Proposed I	Process Heaters (H-0.	1 and H-02)			
A sir	ngle sou	ırce, Unit ID:						
Alter	native \$	Scenario, Scenar	io Name:					
Citation #:	40 C	CFR §63.7560						
Compliance Method based upon:  Applicable Requirement  Gap Filling Requirement								
Method of Compliance Type: (Check all that applies and complete all appropriate sections below)  Monitoring Testing Reporting								
Record Keeping Work Practice Standard								
Section 2: Monitoring								
13. Monitoring device type (stack test, CEM, etc.): N/A								
14. Monito	14. Monitoring device location: N/A							
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:								

15. How will data be reported: $N/A$						
Section 3: Testing						
13. Reference Test Method Description: N/A						
14. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording:						
Monroe will maintain records on-site for at least two (2) years, and off-site for at least five (5) years.						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
N/A						
15. Reporting start date:						
Section 6: Work Practice Standard						
Describe any work practice standards:						
N/A						



SECTION 1. APPLICABLE REQUIREMENT						
Federal Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC			
Plant Code: 45-5201144 Plant Name: Trainer Refinery, PA						
Applicable Requir	ement for: (ple	ase check only	y one box below)			
The entire si	te					
A group of s	ources, Group	ID: Propose	ed Process Heaters (H-01 and H-02)			
A single sou	ırce, Unit ID:					
Alternative S	Scenario, Scen	ario Name:				
Citation #: 25 PA Code §123.1 & §123.2						
Compliance Method based upon:  Applicable Requirement  Gap Filling Requirement						
Method of Compli	ance Type: (Ch	eck all that ap	pplies and complete all appropriate sections below)			
Monitorin	g 🗌	Testing	Reporting			
Record K	Record Keeping Work Practice Standard					
Section 2: Monitoring						
1. Monitoring device type (stack test, CEM, etc.): Daily visual observations						
2. Monitoring device location: $N/A$						
Describe all narameters being monitored along with the frequency and duration of monitoring each narameter:						

The property line is visually monitored daily to ensure fugitive emissions are not leaving the property.						
3. How will data be reported: Semi-annual TVOP deviations reports.						
Section 3: Testing						
1. Reference Test Method Description: N/A						
2. Reference Test Method Citation: N/A						
Section 4: Record Keeping						
Describe what parameters will be recorded and the frequency of recording:						
The Refinery maintains a log of visible emission observations in accordance with the Refinery's TVOP.						
Section 5: Reporting						
Describe what is to be reported and the frequency of reporting:						
Deviations will be reported semi-annually.						
1. Reporting start date: Ongoing						
Section 6: Work Practice Standard						
Describe any work practice standards:						
Monroe will operate according to good operating practices.						



SEC	SECTION 1. APPLICABLE REQUIREMENT						
Federal Tax Id: 45-5201144 Fir		Firm Name:	Monroe Energy, LLC	1			
Plan	t Code:	45-5201144	Plant Name:	Trainer Refinery, PA			
Appl	Applicable Requirement for: (please check only one box below)						
	The entire si	ite					
	A group of s	ources, Group	ID: Proposed	d Process Heaters (H-0	1 and H-02)		
	A single sou	ırce, Unit ID:					
	Alternative S	Scenario, Scen	ario Name:				
Citat	ion #: 25 P	a. Code §123.1	11 and §123.13				
Com	Compliance Method based upon: Applicable Requirement Gap Filling Requirement						
Meth	Method of Compliance Type: (Check all that applies and complete all appropriate sections below)						
	Monitorin	ng 🖂	Testing		Reporting		
	Record Keeping Work Practice Standard						
Section 2: Monitoring							
1. N	1. Monitoring device type (stack test, CEM, etc.): N/A						
2. N	Monitoring de	vice location:	N/A				
	Describe all parameters being monitored along with the frequency and duration of monitoring each						

3. How will data be reported: N/A							
Section 3: Testing							
1. Reference Test Method Description: N/A							
2. Reference Test Method Citation: N/A							
Section 4: Record Keeping							
Describe what parameters will be recorded and the frequency of recording: $N\!/\!A$							
Section 5: Reporting							
Describe what is to be reported and the frequency of reporting:							
N/A							
2. Reporting start date:							
Section 6: Work Practice Standard							
Describe any work practice standards:							
Monroe will operate the proposed heaters according to manufacturer specifications, and firing only refinery							
fuel gas.							



#### Addendum 1 Method Of Compliance Worksheet

SECTION 1. APPLICABLE REQUIREMENT							
Federal Tax Id: 45-5201144 Fi		Firm Name:	Monroe Energy, LLC				
Plant Code: <u>45-52</u>	<i>01144</i> F	Plant Name:	Trainer Refinery, PA				
Applicable Requirement for: (please check only one box below)  The entire site							
A group of sources	s, Group II	D: Proposed	d Process Heaters (H-0	1 and H-02)			
A single source, U	nit ID:						
Alternative Scenar	io, Scena	rio Name:					
Citation #: 25 Pa. Cod	Citation #: 25 Pa. Code §123.22						
Compliance Method base	ed upon:		licable Requirement	Gap Filling Requirement			
Method of Compliance Type: (Check all that applies and complete all appropriate sections below)							
Monitoring		Testing		Reporting			
Record Keeping Work Practice Standard							
Section 2: Monitoring							
1. Monitoring device type (stack test, CEM, etc.): $H_2S$ CEMS							
2. Monitoring device location: Downstream of North Side Fuel Gas Mix Pot							
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:							

Refinery fuel gas is continuously monitored for the  $H_2S$  concentration.

3. How will data be reported:	Data are reported in accordance with 40 CFR Part 60, Subpart Ja and PADEP's Continuous Source Monitoring Manual.					
Section 3: Testing	Section 3: Testing					
1. Reference Test Method Desc	ription: N/A					
2. Reference Test Method Citat	ion: N/A					
Section 4: Record Keepin	ng					
Describe what parameters will be	e recorded and the frequency of recording:					
H <sub>2</sub> S concentration is continuo	usly monitored and recorded.					
Section 5: Reporting						
Describe what is to be reported a	and the frequency of reporting:					
·	and the frequency of reporting: se with 40 CFR Part 60, Subpart Ja and the PADEP's Continuous Source					
·						
Data are reported in accordance Monitoring Manual.						
Data are reported in accordance Monitoring Manual.	ee with 40 CFR Part 60, Subpart Ja and the PADEP's Continuous Source					
Data are reported in accordance  Monitoring Manual.  4. Reporting start date:  Onse	going.  Standard					
Data are reported in accordance Monitoring Manual.  4. Reporting start date: Ons  Section 6: Work Practice  Describe any work practice stand	going.  Standard					



SECT	SECTION 1. APPLICABLE REQUIREMENT			
Federal Tax Id: 45-5201144 Firm Name: Monroe Energy, LLC				Monroe Energy, LLC
Plant Code: 45-5201144 Plant Name: Trainer Refinery, PA				Trainer Refinery, PA
Applic	able Requir	ement for: (ple	ease check only	y one box below)
	The entire site			
	A group of s	ources, Group	ID: Propose	d Process Heaters (H-01 and H-02)
	A single sou	rce, Unit ID:		
	Alternative S	Scenario, Scen	ario Name:	
Citatio	n #: 25 P	a. Code §123.4	41	
Compl	iance Metho	od based upon	: App	olicable Requirement Gap Filling Requirement
Metho	d of Compli	ance Type: <i>(</i> Cl	neck all that an	plies and complete all appropriate sections below)
	Monitorin		Testing	Reporting
	Record K	_	_	tice Standard
Section 2: Monitoring				
1. Monitoring device type (stack test, CEM, etc.): Daily visual observations				
2. Mc	2. Monitoring device location: N/A			
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:				
Stacks	Stacks and facility are monitored daily.			

3. How will data be reported:	Deviations are reported semi-annually in accordance with the Refinery's TVOP.						
Section 3: Testing							
Reference Test Method Des	cription: N/A						
2. Reference Test Method Cita	ntion: N/A						
Section 4: Record Keep	ing						
Describe what parameters will I	be recorded and the frequency of recording:						
Results of opacity observation	s will be recorded daily in accordance with the Refinery's TVOP.						
Section 5: Reporting	Section 5: Reporting						
Describe what is to be reported	and the frequency of reporting:						
Monroe will report any deviat	tion in the Title V Semi-annual report every six months.						
3. Reporting start date:							
Section 6: Work Practice Standard							
Describe any work practice star	ndards:						
Monroe will operate the prope	Monroe will operate the proposed heaters in accordance with good combustion practices and proper						
maintenance of the burners. The burners will be maintained and operated according to the manufacturer's							
recommendations. Monroe w	ill conduct the one-time energy assessment specified at 40 CFR §63.7510(j,)						
and annual tune-up requirements specified in 40 CFR §63.7540(a)(10).							



SECTION	SECTION 1. APPLICABLE REQUIREMENT					
Federal Tax	c ld:	45-5201144	Firm Name:	Monroe Energy, LLC	•	
Plant Code	•	45-5201144	Plant Name:	Trainer Refinery, PA		
Applicable	Requir	ement for: (pl	ease check o	nly one box below)		
The e	ntire s	te				
A gro	up of s	ources, Group	DID: Propo	sed Process Heaters (H-0	01 and H	<i>I-02</i> )
A sing	gle sou	ırce, Unit ID:				
Alterr	native \$	Scenario, Sce	nario Name:			
Citation #:	25 P	a. Code §127.	.12(a)(5) - Cc	O BAT		
Compliance	e Metho	od based upor	n: 🔀 A	pplicable Requirement		Gap Filling Requirement
Method of 0	Compli	ance Type: (C	heck all that a	applies and complete all a	ıppropria	te sections below)
Mo	Monitoring Testing Reporting					
Re	Record Keeping Work Practice Standard					
Section 2: Monitoring						
1. Monitoring device type (stack test, CEM, etc.): N/A						
2. Monitor	2. Monitoring device location: $N/A$					
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:						
3. How wi	II data	be reported:	N/A			

Section 3:	Testing	
1. Reference	Test Method Description:	N/A
2. Reference	Test Method Citation:	N/A
Section 4:	Record Keeping	
Describe what	parameters will be recorded	and the frequency of recording:
N/A		
Section 5:	Reporting	
Describe what	is to be reported and the fre	equency of reporting:
N/A		
3. Reporting	start date:	
Section 6:	Work Practice Standar	d
Describe any v	vork practice standards:	
Monroe prop	oses compliance with the B	oiler MACT work practice standards (i.e., burner maintenance and
annual combi	ıstion tuning proper design	, operation and good combustion and engineering practices as
BAT for CO e	missions.	



SECT	SECTION 1. APPLICABLE REQUIREMENT			
Federal Tax Id: 45-5201144 Fi		Firm Name:	Monroe Energy, LLC	
Plant (	Code:	45-5201144	Plant Name:	Trainer Refinery, PA
Applic	able Requir	ement for: (ple	ease check only	y one box below)
□ ¹	The entire s	ite		
	A group of s	ources, Group	ID: Propose	d Process Heaters (H-01 and H-02)
	A single soι	ırce, Unit ID:		
	Alternative S	Scenario, Scer	nario Name:	
Citatio	on #: 25 P	a. Code §127.	12(a)(5) - VOC	C BAT
Compl	liance Metho	od based upon	: App	olicable Requirement Gap Filling Requirement
Metho	d of Compli	ance Type: (C	heck all that ap	plies and complete all appropriate sections below)
	Monitorin	ng	Testing	Reporting
	Record K	eeping $igtharpoonup$	Work Prac	tice Standard
Section 2: Monitoring				
4. Mc	4. Monitoring device type (stack test, CEM, etc.): N/A			
5. Mc	i. Monitoring device location: N/A			
Descri	Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:			

6. How will data be reported: N/A
Section 3: Testing
4. Reference Test Method Description: N/A
5. Reference Test Method Citation: N/A
Section 4: Record Keeping
Describe what parameters will be recorded and the frequency of recording:
N/A
Section 5: Reporting
Describe what is to be reported and the frequency of reporting:
N/A
6. Reporting start date:
Section 6: Work Practice Standard
Describe any work practice standards:
Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and
annual combustion tuning), proper design, operation and good combustion and engineering practices as
BAT for VOC emissions.



SECTION	SECTION 1. APPLICABLE REQUIREMENT				
Federal Tax Id: <u>45-5201144</u> Firm Nam			Firm Name:	Monroe Energy, LLC	
Plant Code	<b>)</b> :	45-5201144	Plant Name:	Trainer Refinery, PA	
Applicable	Requir	ement for: (ple	ease check only	y one box below)	
The	entire si	te			
A green     A green	oup of s	ources, Group	ID: Propose	ed Process Heaters (H-01 and H-02)	
A sir	igle sou	rce, Unit ID:			
Alter	native S	Scenario, Scer	ario Name:		
Citation #:	25 P	a. Code §127.	$12(a)(5) - NO_{2}$	x BAT	
Complianc	e Metho	od based upon	: App	olicable Requirement Gap Filling Requirement	
Method of	Compli	ance Type: (Cl	neck all that ap	plies and complete all appropriate sections below)	
M	onitorin	g 🗆	Testing	Reporting	
R	Record Keeping Work Practice Standard				
Section 2: Monitoring					
7. Monito	7. Monitoring device type (stack test, CEM, etc.): N/A				
8. Monito	8. Monitoring device location: N/A		N/A		
Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:					

9. How will data be reported: N/A
Section 3: Testing
7. Reference Test Method Description: N/A
8. Reference Test Method Citation: N/A
Section 4: Record Keeping
Describe what parameters will be recorded and the frequency of recording:
N/A
Section 5: Reporting
Describe what is to be reported and the frequency of reporting:
N/A
9. Reporting start date:
Section 6: Work Practice Standard
Describe any work practice standards:
Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and
annual combustion tuning), good operation practices and a low-NO <sub>X</sub> burners to meet the proposed BAT
emission rate for $NO_X$ .



SEC	SECTION 1. APPLICABLE REQUIREMENT			
Fede	ral Tax ld:	45-5201144	Firm Name:	Monroe Energy, LLC
Plant	Code:	45-5201144	Plant Name:	Trainer Refinery, PA
Annli	iooble Dogwi	romant fare (nl	aga ahaak anb	v and hav halow)
Appi	cable Requi	rement for: (pi	ease check only	one box below)
	The entire s	site		
	A group of	sources, Group	ID: Propose	d Process Heaters (H-01 and H-02)
	A single so	urce, Unit ID:		
	Alternative	Scenario, Scer	nario Name:	
Citati	ion #: 25 I	Pa. Code §127.	$12(a)(5) - SO_2$	BAT
Com	pliance Meth	od based upon	: App	licable Requirement
Meth	od of Compl	iance Type: (C	heck all that ap	plies and complete all appropriate sections below)
	Monitori	ng _	Testing	Reporting
	Record I	Keeping 🔀	Work Prac	tice Standard
Section 2: Monitoring				
10. Monitoring device type (stack test, CEM, etc.): N/A				
11. N	11. Monitoring device location: N/A			
Desc	Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:			

12. How will data be reported: $N/A$
Section 3: Testing
10. Reference Test Method Description: N/A
11. Reference Test Method Citation:  N/A
Section 4: Record Keeping
Describe what parameters will be recorded and the frequency of recording:
N/A
Section 5: Reporting
Describe what is to be reported and the frequency of reporting:
N/A
12. Reporting start date:
Section 6: Work Practice Standard
Describe any work practice standards:
Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and
annual combustion tuning), good operation practices and firing refinery fuel gas that complies with 40
CFR Part 60, Subpart Ja as BAT for SO <sub>2</sub> .



SEC	SECTION 1. APPLICABLE REQUIREMENT			
Fede	ral Tax Id:	45-5201144	Firm Name:	Monroe Energy, LLC
Plant	Code:	45-5201144	Plant Name:	Trainer Refinery, PA
Annli	icable Pegu	iroment for: (nl	asa chack anly	y one box below)
Appi	•		ease check only	y one box below)
	The entire	site		
	A group of	sources, Group	ID: Propose	d Process Heaters (H-01 and H-02)
	A single so	urce, Unit ID:		
	Alternative	Scenario, Scer	nario Name:	
Citat	ion #: 25	Pa. Code §127.	12(a)(5) - PM	BAT
Com	pliance Metl	nod based upon	: App	olicable Requirement Gap Filling Requirement
Meth	od of Comp	liance Type: (C	heck all that ap	plies and complete all appropriate sections below)
	Monitor	ing	Testing	Reporting
	Record	Keeping 🔀	Work Prac	tice Standard
Section 2: Monitoring				
13. Monitoring device type (stack test, CEM, etc.): N/A				
14. N	14. Monitoring device location: N/A			
Desc	Describe all parameters being monitored along with the frequency and duration of monitoring each parameter:			

15. How will data be reported: N/A
Section 3: Testing
13. Reference Test Method Description: N/A
14. Reference Test Method Citation: N/A
Section 4: Record Keeping
Describe what parameters will be recorded and the frequency of recording:
N/A
Section 5: Reporting
Describe what is to be reported and the frequency of reporting:
N/A
15. Reporting start date:
Section 6: Work Practice Standard
Describe any work practice standards:
Monroe proposes compliance with the Boiler MACT work practice standards (i.e., burner maintenance and
annual combustion tuning), proper design, operation and good combustion and engineering practices as
BAT for PM emissions.



Monroe Energy, LLC 4101 Post Road Trainer, PA 19061 (610) 364-8000

May 14, 2015

FedEx: 7736 0305 8668

James Rebarchak
Regional Air Program Manager
Commonwealth of Pennsylvania
Department of Environmental Protection
2 East Main Street
Norristown, PA 19401

RE: Semi-Annual Air Compliance History Report

Monroe Energy, LLC – Trainer Refinery Title V Operating Permit No. 23-00003

Dear Mr. Rebarchak:

In accordance with 25 Pa. Code §127.412(j), Monroe Energy, LLC is submitting the enclosed updated Air Pollution Control Act Compliance Review Form. Monroe Energy updates the form semi-annually.

Please feel free to contact me at (610) 364-8528 if you have any questions regarding this submittal.

Sincerely,

MONROE ENERGY, LLC

David M. Chetkowski, P.E.

Air Program Lead

Enclosure



#### AIR POLLUTION CONTROL ACT COMPLIANCE REVIEW FORM

Fully and accu	urately provide the following inform	ation, as specified	d. Attach	additional sheets as necessary.			
Type of Compliance Review Form Submittal (check all that apply)  ☐ Original Filing Date of Last Compliance Review Form Filing:							
☐ New Plan	rpe of Submittal  New Plan Approval  New Operating Permit  Renewal of Operating Permit  Extension of Plan Approval  Change of Ownership  Periodic Submission (@ 6 mos)  Other:						
	SECTION A. GENE	RAL APPLICATI	ION INFO	DRMATION			
	licant/Permittee/("applicant") tions-attach documentation of le y, LLC	egal name)					
Address	4101 Post Road						
	Trainer, PA 19061						
Telephone	610-364-8000	Γaxpayer ID# _	45-5201	144			
Permit, Plan /	Approval or Application ID#	TVOP-23-00003					

#### SECTION B. GENERAL INFORMATION REGARDING "APPLICANT"

If applicant is a corporation or a division or other unit of a corporation, provide the names, principal places of business, state of incorporation, and taxpayer ID numbers of all domestic and foreign parent corporations (including the ultimate parent corporation), and all domestic and foreign subsidiary corporations of the ultimate parent corporation with operations in Pennsylvania. Please include all corporate divisions or units, (whether incorporated or unincorporated) and privately held corporations. (A diagram of corporate relationships may be provided to illustrate corporate relationships.) Attach additional sheets as necessary.

Unit Name	Principal Places of Business	State of Incorporation	Taxpayer ID	Relationship to Applicant
Delta Air Lines, Inc.	Atlanta, GA	Delaware	58-0218548	Parent
Monroe Energy, LLC	Trainer, PA	Delaware	45-5201144	Applicant: 100% owned by Parent
MIPC, LLC	Aston, PA and Philadelphia, PA	Delaware	45-5201987	100% owned by Parent

#### SECTION C. SPECIFIC INFORMATION REGARDING APPLICANT AND ITS "RELATED PARTIES"

Pennsylvania Facilities. List the name and location (mailing address, municipality, county), telephone number, and relationship to applicant (parent, subsidiary or general partner) of applicant and all Related Parties' places of business, and facilities in Pennsylvania. Attach additional sheets as necessary.

Unit Name	Street Address	County and Municipality	Telephone No.	Relationship to Applicant
Trainer Refinery	4101 Post Road	Delaware/Trainer Borough	610-364- 8000	Applicant
Philadelphia Terminal	4210 G Street	Philadelphia/ Philadelphia	215-533- 7310	Owned and Operated by MIPC, LLC
Chelsea Terminal	920 Cherry Tree Rd	Delaware/Aston Township	610-485- 5410	Owned and Operated by MIPC, LLC

Provide the names and business addresses of all general partners of the applicant and parent and subsidiary corporations, if any.

Name	Business Address	
Delta Air Lines, Inc.	P.O. Box 20706, Atlanta, GA 30320	
MIPC, LLC	920 Cherry Tree Rd., Aston, PA 19014	

#### 2700-PM-AQ0004 Rev. 6/2006

List the names and business address being permitted (i.e. plant manager).	of persons with overall management responsibility for the process
Name	Business Address
Jeffrey K. Warmann, CEO & President	4101 Post Rd, Trainer, PA 19061

Plan Approvals or Operating Permits. List all plan approvals or operating permits issued by the Department or an approved local air pollution control agency under the APCA to the applicant or related parties that are currently in effect or have been in effect at any time 5 years prior to the date on which this form is notarized. This list shall include the plan approval and operating permit numbers, locations, issuance and expiration dates. Attach additional sheets as necessary.

Air Contamination Source	Plan Approval/ Operating Permit#	Location	Issuance Date	Expiration Date
Trainer Refinery	TVOP-23-00003	Trainer	06/25/2014	06/25/2019
Trainer Refinery	PA-23-0003S	Trainer	08/03/2011	08/03/2015
Trainer Refinery	PA-23-0003Y	Trainer	10/14/2014	04/14/2016
Trainer Refinery	See Attachment B			
Chelsea Terminal	See Attachment B			
Philadelphia Terminal	See Attachment B			

Compliance Background. (Note: Copies of specific documents, if applicable, must be made available to the Department upon its request.) List all documented conduct of violations or enforcement actions identified by the Department pursuant to the APCA, regulations, terms and conditions of an operating permit or plan approval or order by applicant or any related party, using the following format grouped by source and location in reverse chronological order. Attach additional sheets as necessary. See the definition of "documented conduct" for further clarification. Unless specifically directed by the Department, deviations which have been previously reported to the Department in writing, relating to monitoring and reporting, need not be reported.

Date	Location	Plan Approval/ Operating Permit#	Nature of Documented Conduct	Type of Department Action	Status: Litigation Existing/Continuing or Corrected/Date	Dollar Amount Penalty
See Attach- ment C						\$
						\$
						\$
						\$
						\$
						\$
	-000				, alvertwo	\$
						\$
						\$
						\$

List all incidents of deviations of the APCA, regulations, terms and conditions of an operating permit or plan approval or order by applicant or any related party, using the following format grouped by source and location in reverse chronological order. This list must include items both currently known and unknown to the Department. Attach additional sheets as necessary. See the definition of "deviations" for further clarification.

Date	Location	Plan Approval/ Operating Permit#	Nature of Deviation	Incident Status: Litigation Existing/Continuing Or Corrected/Date
See				
Attachment D				
	•			

<u>CONTINUING OBLIGATION</u>. Applicant is under a continuing obligation to update this form using the Compliance Review Supplemental Form if any additional deviations occur between the date of submission and Department action on the application.

#### **VERIFICATION STATEMENT**

Subject to the penalties of Title 18 Pa.C.S. Section 4904 and 35 P.S. Section 4009(b)(2), I verify under penalty of law that I am authorized to make this verification on behalf of the Applicant/Permittee. I further verify that the information contained in this Compliance Review Form is true and complete to the best of my belief formed after reasonable inquiry. I further verify that reasonable procedures are in place to ensure that "documented conduct" and "deviations" as defined in 25 Pa Code Section 121.1 are identified and included in the information set forth in this Compliance Review Form.

# Attachment A Air Pollution Control Act Compliance Review Form List of Parent Companies and Subsidiaries with Operations in PA

As of the date of this report, the only wholly-owned Delta Air Lines, Inc. facilities which presently operate or own property in Pennsylvania are Monroe Energy, LLC and MIPC, LLC whose locations are noted on the Compliance Review Form.

# Attachment B Air Pollution Control Act Compliance Review Form Plan Approvals or Operating Permits (a)

Air Contamination Source	Plan Approval/ Operating Permit #	Location	Issuance Date	Eumination Date
Source	Permit #	Location	issuance Date	Expiration Date
Tuein au Dafin au	DA 33 00031	Tuelle	00/20/2000	Incorporated into TVOP on
Trainer Refinery	PA-23-0003J	Trainer	06/20/2008	
				03/12/2010
Total D. Com	DA 33 0003K	T t	05/04//2000	Incorporated
Trainer Refinery	PA-23-0003K	Trainer	05/01//2009	into TVOP on
				03/12/2010
			0.0/0.0/0.000	Incorporated
Trainer Refinery	PA-23-0003M	Trainer	06/22/2009	into TVOP on
				10/28/2011
				Incorporated
Trainer Refinery	PA-23-0003N	Trainer	07/14/2009	into TVOP on
				03/12/2010
Trainer Refinery	PA-23-0003O	Trainer	09/21/2009	Withdrawn on
Trainer Kermery	FA-23-00030	Halliel	03/2.1/2003	03/21/2011
				Incorporated
Trainer Refinery	PA-23-0003P	Trainer	12/17/2009	into TVOP in
				07/01/2013
Tuning a Definer	PA-23-0003T	Tueinen	10/27/2011	Withdrawn
Trainer Refinery	PA-23-00031	Trainer	10/27/2011	on 11/19/2012
T . D .:	DA 22 000211	-	11/00/2011	Withdrawn
Trainer Refinery	PA-23-0003U	Trainer	11/09/2011	on 05/09/2014
~ 0	54.00.00001/		0.11.0/0.10	Withdrawn
Trainer Refinery	PA-23-0003V	Trainer	04/12/2012	on 05/30/2013
				Incorporated
Trainer Refinery	PA-23-0003W	Trainer	09/24/2013	into TVOP in
,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,,	,,	09/22/2014
				Incorporated
Trainer Refinery	PA-23-0003X	Trainer	03/13/2014	into TVOP in
Trainer Kermery	17, 25 00057	Humer	03/13/2014	09/22/2014
				03/22/2014
	TVOP			
Chelsea Terminal	23-00041	Aston	11/28/2012	11/28/2017
Philadelphia	TVOP			
Terminal	V11-018	Philadelphia	12/31/2012	12/31/2017
Terminal	A TT-OTO			

<sup>(</sup>a) Plan Approvals and Operating permits that were active or in effect in the last 5 years.

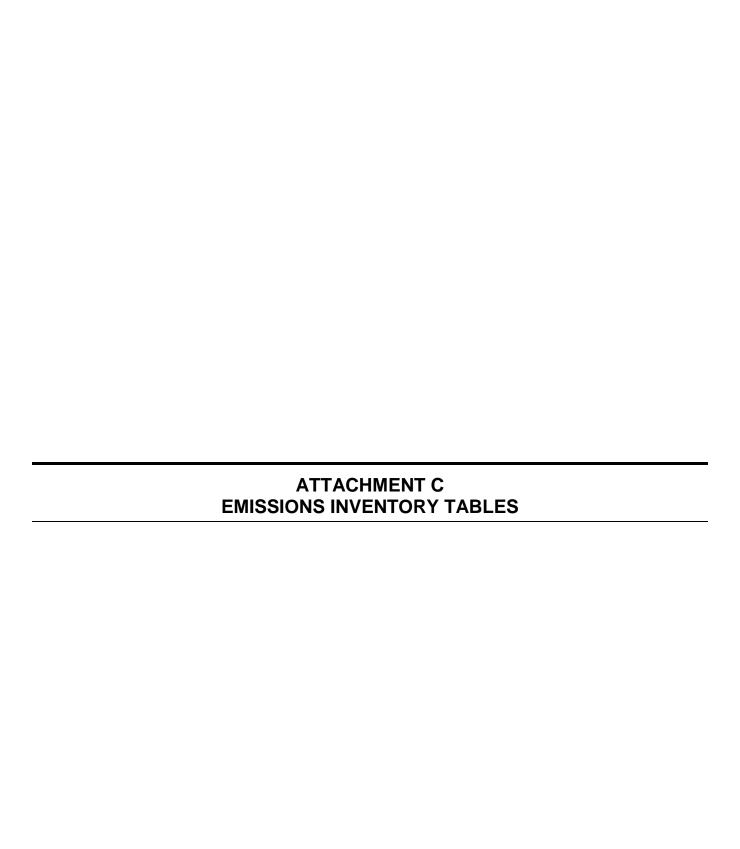
#### Attachment C Air Pollution Control Act Compliance Review Form **Compliance Background**

Date [1]	Location [2]	Plan Approval / Operating Permit #	Nature of Documented Conduct	Type of Department Action	Status: Litigation Existing / Continuing or Corrected / Date	Dollar Amount Penalty
03/24/2015	Trainer Refinery	TVOP 23-00003	NOV for Platformer catalyst exceeding chloride limits.	NOV	No action Required.	None
11/17/2014	Trainer Refinery	TVOP 23-00003	Penalty assesment for all NOVs issued in 2014.	Penalty	Corrected on 11/17/2014	\$15,268
10/03/2014	Trainer Refinery	TVOP 23-00003	NOV for failure to maintain records pursuant to RICE MACT.	NOV	Corrected	
07/30/2014	Trainer Refinery	TVOP 23-00003	NOV for failure to maintain records and delinquent report pursuant to BWON.	NOV	Corrected	Included in
06/06/2014	Trainer Refinery	TVOP 23-00003	NOV for failure to maintain records  pursuant to storage tank  requirements.	NOV	Corrected	10/14/2014 assessment.
05/16/2014	Trainer Refinery	TVOP 23-00003	NOV for failure to log visible emission observations.	NOV	No action Required.	
04/28/2014	Trainer Refinery	TVOP 23-00003	NOV for failure to include date on report.	NOV	Corrected on 05/09/2014	
03/24/2014	Trainer Refinery	TVOP 23-00003	Penalty Assesment for 08/02/2013 NOV.	Penalty	Settled on 04/08/2014	\$6,000
01/30/2014	Trainer Refinery	TVOP 23-00003	MACT Group 1 Tank vented directly to atmosphere, bypassing control by the Main Flare, when a PSV malfunctioned and opened below its setpoint.	NOV	Corrected on 01/30/2014	Included in 10/14/2014 assessment.
08/02/2013	Trainer Refinery	TVOP 23-00003	Failure to sample Platformer catalyst in accordance with OMMP.	NOV	Corrected on 08/21/2013	Included in 3/24/2014 assessment.
04/18/2012	Trainer Refinery	TVOP 23-00003	NOV for Use of a pump without mechanical seals on two occasions.	NOV	Settled	None
11/15/2010	Trainer Refinery	TVOP 23-00003	NOV for NSPS QQQ Repairs	NOV	Settled	\$11,100
07/30/2010	Trainer Refinery	TVOP 23-00003	NOV for Platformer HCl Emission Records	NOV	Settled	
05/12/2010	Trainer Refinery	TVOP 23-00003	CACP for CEMS	Penalty	Settled	\$96,000
05/12/2010	Trainer Refinery	TVOP 23-00003	CACP for FCCU Emissions and Flaring	Penalty	Settled	\$20,000

<sup>[1]</sup> Monroe Energy, LLC purchased the Trainer Refinery from Phillips66 on June 22, 2012.
[2] See Reports submitted by Monroe transportation facilities (Chelsea and Philadelphia Terminals) for compliance background.

## Attachment D Air Pollution Control Act Compliance Review Form List of Deviations

Monroe Energy, LLC informs the Department on a regular basis regarding incidents and deviations through various reports, including but not limited to, CEMS reports, LDAR reports, Title V deviation and certification reports, incident reports, and Refinery MACT reports.



### Table C-1 Monroe Energy, LLC - Trainer, PA Refinery PSD Baseline Actual Emission Rates

	Emission Unit							Emis	sion Rate (	tpy)						
	Emission Unit	PM	PM <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>2</sub>	VOC	CO	Lead	H <sub>2</sub> S	TRS	CO <sub>2</sub>	N <sub>2</sub> O	CH₄	<b>Total GHG</b>	CO <sub>2</sub> e <sup>(a)</sup>
101	FCC Unit	43.06	63.93	56.61	46.18	297.01	3.18	15.63	2.47E-04	-	-	499,375.51	2.93	14.67	499,393.10	500,614.22
733	FCCU Feed Heater	0.10	0.42	0.42	0.44	1.76	0.30	0.93	3.73E-05	0.01	0.01	16,695.75	0.17	0.85	16,696.77	16,767.57
735	Kerosene/HCN HTU Feed Heater	0.22	0.36	0.36	0.39	6.41	0.26	3.23	1.82E-05	2.74E-03	2.77E-03	4,319.92	0.04	0.22	4320.18	4,338.50
736	Diesel HTU Heater	0.24	0.42	0.42	0.49	10.39	0.06	3.49	3.35E-05	0.01	0.01	13,802.45	0.14	0.70	13,803.30	13,861.83
741	D2/VGO Hydrotreater Feed Heater	0.43	0.33	0.33	0.64	8.01	0.44	7.44	4.78E-05	0.01	0.01	23,209.06	0.24	1.18	23,210.47	23,308.90
737	Naphtha HDS Heater	1.19	1.87	1.87	1.96	26.07	1.35	20.86	1.22E-04	0.02	0.02	33,037.72	0.34	1.68	33039.73	33,179.83
738	Platformer Feed Heater	8.45	13.44	13.44	14.10	147.14	9.73	1.57	9.42E-04	0.19	0.19	284,157.46	2.89	14.45	284,174.80	285,379.82
739	Isocracker 1st Stage Heater	0.55	0.96	0.96	1.01	15.65	0.70	11.21	6.49E-05	0.01	0.01	14,711.55	0.15	0.75	14712.45	14,774.84
740	Isocracker Splitter Reboiler	0.69	1.19	1.19	1.25	15.70	0.86	13.38	7.83E-05	0.01	0.01	18,382.52	0.19	0.93	18383.64	18,461.59
742	VCD 541 VAC Heater	0.18	0.71	0.71	0.77	13.38	0.51	7.34	4.31E-05	0.01	0.01	13,793.59	0.14	0.70	13794.44	13,852.93
743	VCD 542 VAC Heater	0.44	0.78	0.78	0.44	4.48	0.02	0.01	2.38E-05	0.01	0.01	17,771.31	0.18	0.90	17772.39	17,847.75
746	VCD 544 VAC Heater	1.35	2.88	2.88	2.37	12.53	2.19	1.34	1.40E-04	0.02	0.02	35,464.65	0.36	1.80	35466.81	35,617.21
744	ACD 543 Crude Heater	4.32	7.22	7.22	7.89	28.30	5.23	81.32	4.82E-04	0.09	0.09	143,860,54	1.46	7.31	143869.31	144,479,38
745	ACD 544 Crude Heater	4.68	7.59	7.59	8.29	32.82	5.49	83,63	4.91E-04	0.09	0.09	145,398.35	1.48	7.39	145407.22	146,023,81
34	Boiler 9	0.53	1.69	1.51	1.93	4.14	0.11	1.17	4.51E-04	0.06	0.06	72,880.82	0.14	1.37	72,882,33	72,956.09
35	Boiler 10	0.38	1.06	1.01	1.91	3.89	0.10	8.72	4.32E-04	0.06	0.06	83,481.92	0.16	1.57	83,483.65	83,568.14
102	SRU	0.10	0.38	0.38	19.27	5.22	0.24	3,56	2.04E-05	0.00	-	2,852,70	0.06	5.88E-03	2,852.76	2,870,38
103	Main Flare	4.05	5.04	5.04	10.04	10.19	33.12	58.11	1.14E-04	14.23	_	51,382,53	0.96	8.75	51,392.24	51,887.23
165	Tank 93	-	-	-	-	-	2.46		1.172 07	-	_	-	0.50	-	-	-
166	Tank 94	_	-	_	-	_	1.61	-	-	_	-	_	-	-	_	_
126	Tank 95	-	-	_	-	_	2.13	-	_	_	-	_	-	-	-	_
127	Tank 96	-	-	_	-	_	3.27	_	_	_	_	_	-	-	-	_
137	Tank 152	-		-	-	-	1.38		-	-		_	-	-	-	
138	Tank 153				_	_	0.15	_		_	_	_				_
140	Tank 155	-	-	-	-	-	0.13	-	-	-	-	=	-	-	-	
140	Tank 157	-		-	-	-	0.15		-	-		_	-	-	-	
300	Tank 158 (Source ID 193)						3.50	-	-	_			_			
143	Tank 158 (Source ID 193) Tank 159	-	-	-	-	-	3.32		-	-	-	-		-	-	-
194	Tank 139	-	-	-	-	_	4.86	-	-	-	-	-	-	-	=	-
194	Tank 160	-	-	-	-		2.70	-	-	-	-	-	-	-	-	-
144	Tank 161 Tank 162	-	-	-	-	-	0.87	-	-	-	-	-	-	-	-	-
145	**				-	-	1.60	-	-	-	-	-	-	_	-	
146	Tank 163	-	-	-	-	-		-	-	-	-	-	-	-	-	-
	Tank 164	-	-	-	-	-	2.53	-	-	-	-	-	-	-	-	-
148 149	Tank 165	-	-	-	-	-	3.09	-	-	-	-	-	-	-	-	-
- 1,	Tank 166	-	-	-	-	-	2.16	-	-	-	-	-	-	-	-	-
150	Tank 168	-	-	-	-	-	1.53	-	-	-	-	-	-	-	-	-
152	Tank 170	-	1	-	-	-	3.02	-	-	-	-	-	-	-	-	-
155	Tank 174	-	1	-	-	-	4.09	-	-	-	-	-	-	-	-	-
156	Tank 175	-	-	-	-	-	5.35	-	-	-	-	-	-	-	-	-
157	Tank 178	-	-	-	-	-	4.53	-	-	-	-	-	-	-	-	-
160	Tank 181	-	-	-	-	-	3.03	-	-	-	-	-	-	-	-	-
161	Tank 182	-	-	-	-	-	6.52	-	-	-	-	-	-	-	-	-
163	Tank 185	-	-	-	-	-	7.02	-	-	-	-	-	-	-	-	-
164	Tank 186	-	-	-		-	4.75	-	-		-	-	-	-	-	
	ne Emissions (tons/24 months)	141.92	220.54	205.42	238.75	1,286.16	279.26	645.90	7.58E-03	29.70	1.25	2,949,157	23.95	129.63	2,949,310.23	2,959,534.50
Total Bo	aseline Actual Emissions	70.96	110.27	102.71	119.38	643.08	139.63	322.95	3.79E-03	14.85	0.62	1,474,578	11.98	64.81	1,474,655.12	1,479,767.25
	Baseline Period	Aug-13	Aug-13	Aug-13	Aug-13	Aug-13	Aug-13	Jan-13	Nov-12	Jan-09	Apr-09	Jun-09	Jun-09	Jun-09	Jun-09	Jun-09
	Dasenne Ferioa	Jul-15	Jul-15	Jul-15	Jul-15	Jul-15	Jul-15	Dec-14	Oct-14	Dec-10	Mar-11	May-11	May-11	May-11	May-11	May-11
Ľ-																

 $<sup>^{(</sup>a)}\,CO_2e$  is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{\substack{i=1\\i=1}}^n GHG_i \times GWP_i$$

 $\label{eq:where GHGi} We in a mass emissions of greenhouse gas i (short tons/year)$   $GWPi = global \ warming \ potential \ of \ greenhouse \ gas \ i \ from \ the \ table \ below$ 

Pollutant	GWP (100 year)
$CO_2$	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

Table C-2
Monroe Energy, LLC - Trainer, PA Refinery
NNSR Baseline Actual Emission Rates

		Emission Rate (tpy)					
	Emission Unit		PM <sub>2.5</sub> NNSF	2	Ozone NNSR		
		PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>x</sub>	NO <sub>x</sub>	VOC	
101	FCC Unit	56.61	46.18	297.01	297.01	3.18	
733	FCCU Feed Heater	0.42	0.44	1.76	1.76	0.30	
735	Kerosene/HCN HTU Feed Heater	0.36	0.39	6.41	6.41	0.26	
736	Diesel HTU Heater	0.42	0.49	10.39	10.39	0.06	
741	D2/VGO Hydrotreater Feed Heater	0.33	0.64	8.01	8.01	0.44	
737	Naphtha HDS Heater	1.87	1.96	26.07	26.07	1.35	
738	Platformer Feed Heater	13.44	14.10	147.14	147.14	9.73	
739	Isocracker 1st Stage Heater	0.96	1.01	15.65	15.65	0.70	
740	Isocracker Splitter Reboiler	1.19	1.25	15.70	15.70	0.86	
742	VCD 541 VAC Heater	0.71	0.77	13.38	13.38	0.51	
743	VCD 542 VAC Heater	0.78	0.44	4.48	4.48	0.02	
746	VCD 544 VAC Heater	2.88	2.37	12.53	12.53	2.19	
744	ACD 543 Crude Heater	7.22	7.89	28.30	28.30	5.23	
745	ACD 544 Crude Heater	7.59	8.29	32.82	32.82	5.49	
34	Boiler 9	1.51	1.93	4.14	4.14	0.11	
35	Boiler 10	1.01	1.91	3.89	3.89	0.10	
102	SRU	0.38	19.27	5.22	5.22	0.24	
103	Main Flare	5.04	10.04	10.19	10.19	33.12	
165	Tank 93	-	-	-	-	2.46	
166	Tank 94	_	_	-	_	1.61	
126	Tank 95	-	_	_	_	2.13	
127	Tank 96	-	_	_	_	3.27	
137	Tank 152	_	_	_	_	1.38	
138	Tank 153	-	_	_	_	0.15	
140	Tank 155	-	_	-	_	0.13	
142	Tank 157	_	_	-	_	0.15	
300	Tank 158 (Source ID 193)	-	_	_	_	3.50	
143	Tank 159 (Source 15 175)	_	_	_	_	3.32	
194	Tank 160	_	_	-	_	4.86	
144	Tank 161	_	_	_	_	2.70	
145	Tank 162	_	_	_	_	0.87	
146	Tank 163		-	_	_	1.60	
147	Tank 164		-	_		2.53	
148	Tank 165		_	-		3.09	
149	Tank 166	<u>-</u>	-	-	_	2.16	
150	Tank 168		-			1.53	
152			-	_		3.02	
155						4.09	
156	Tank 174		-	-	-	5.35	
157	Tank 178	-		-	-	4.53	
160	Tank 178	-	-	-	-	3.03	
	Tank 182	-	-	-	-	6.52	
161	Tank 182	-	-	-	-		
163		-	-	-	_	7.02	
164	Tank 186	205.42	220 55	1 206 16	1 207 17	4.75	
	line Emissions (tons/24 months)	205.42	238.75	1,286.16	1,286.16	279.20	
Total .	Baseline Actual Emissions	102.71	119.38	643.08	643.08	139.63	
	Baseline Period	Aug-13 Jul-15	Aug-13 Jul-15	Aug-13 Jul-15	Aug-13	Aug-1	

## Table C-3 Monroe Energy, LLC - Trainer, PA Refinery Projected Future Operations

MMBtu/hr   MMBtu/yr   MMBtu/yr		Emission Unit	Projected I	Heat Duty <sup>(a)</sup>	Projected Annual Hours
101   FCC Unit			MMBtu/hr	MMBtu/yr	of Operation
733	Existing Unit	s			•
735   Kerosene/HCN HTU Feed Heater   20	101	FCC Unit <sup>(b)</sup>	-	_	8,760
736	733	FCCU Feed Heater	23	201,480	8,760
741         D2/VGO Hydrotreater Feed Heater         18         157,680         8,760           737         Naphtha HDS Heater         76         665,760         8,760           738         Platformer Feed Heater         493         4,318,680         8,760           739         Isocracker Ist Stage Heater         33         289,080         8,760           740         Isocracker Splitter Reboiler         44         385,440         8,760           742         VCD 541 VAC Heater         36         315,360         8,760           743         VCD 542 VAC Heater         20         175,200         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           744         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           162         SRU         -         -         8,760           165         Tank 93         -         -         8,760           166         Tank 94         -         -         8,760           127         Tank 95         - <td>735</td> <td>Kerosene/HCN HTU Feed Heater</td> <td>8.3</td> <td>72,708</td> <td>8,760</td>	735	Kerosene/HCN HTU Feed Heater	8.3	72,708	8,760
737         Naphtha HDS Heater         76         665,760         8,760           738         Platformer Feed Heater         493         4,318,680         8,760           739         Isocracker Ist Stage Heater         33         289,080         8,760           740         Isocracker Spitter Reboiler         44         385,440         8,760           742         VCD 541 VAC Heater         36         315,360         8,760           743         VCD 542 VAC Heater         20         175,200         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           744         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           166         Tank 93         -         -         8,760           126         Tank 94         -         -         8,760           127         Tank 96         -         -	736	Diesel HTU Heater	20	175,200	8,760
738         Platformer Feed Heater         493         4,318,680         8,760           739         Isocracker 1st Stage Heater         33         289,080         8,760           740         Isocracker Splitter Reboiler         44         385,440         8,760           742         VCD 541 VAC Heater         36         315,360         8,760           743         VCD 542 VAC Heater         20         175,200         8,760           746         VCD 544 VAC Heater         71         621,960         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           166         Tank 93         -         -         8,760           126         Tank 94         -         -         8,760           127         Tank 96         -         -	741	D2/VGO Hydrotreater Feed Heater	18	157,680	8,760
739         Isocracker Ist Stage Heater         33         289,080         8,760           740         Isocracker Splitter Reboiler         44         385,440         8,760           742         VCD 541 VAC Heater         36         315,360         8,760           743         VCD 542 VAC Heater         20         175,200         8,760           746         VCD 544 VAC Heater         260         2,277,600         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           166         Tank 93         -         -         8,760           126         Tank 94         -         -         8,760           127         Tank 95         -         -         8,760           133         Tank 152         -         -         8,760     <	737	Naphtha HDS Heater	76	665,760	8,760
740         Isocracker Splitter Reboiler         44         385,440         8,760           742         VCD 541 VAC Heater         36         315,360         8,760           743         VCD 542 VAC Heater         20         175,200         8,760           746         VCD 544 VAC Heater         71         621,960         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           165         Tank 93         -         -         8,760           126         Tank 94         -         -         8,760           127         Tank 96         -         -         8,760           137         Tank 152         -         -         8,760           142         Tank 157         -         -         8,760           142	738	Platformer Feed Heater	493	4,318,680	8,760
742         VCD 541 VAC Heater         36         315,360         8,760           743         VCD 542 VAC Heater         20         175,200         8,760           746         VCD 544 VAC Heater         71         621,960         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           165         Tank 93         -         -         8,760           166         Tank 94         -         -         8,760           127         Tank 95         -         -         8,760           137         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           142         Tank 157<	739	Isocracker 1st Stage Heater	33	289,080	8,760
743         VCD 542 VAC Heater         20         175,200         8,760           746         VCD 544 VAC Heater         71         621,960         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           165         Tank 93         -         -         8,760           166         Tank 94         -         -         8,760           126         Tank 95         -         -         8,760           127         Tank 96         -         -         8,760           137         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           142         Tank 157         -         -         8,760           143         Tank 159         -         - <td>740</td> <td>Isocracker Splitter Reboiler</td> <td>44</td> <td>385,440</td> <td>8,760</td>	740	Isocracker Splitter Reboiler	44	385,440	8,760
746         VCD 544 VAC Heater         71         621,960         8,760           744         ACD 543 Crude Heater         260         2,277,600         8,760           745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           165         Tank 93         -         -         8,760           166         Tank 94         -         -         8,760           126         Tank 95         -         -         8,760           137         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           142         Tank 157         -         -         8,760           142         Tank 157         -         -         8,760           142         Tank 159         -         -         8,760           144         Tank 160         - <t< td=""><td>742</td><td>VCD 541 VAC Heater</td><td>36</td><td>315,360</td><td>8,760</td></t<>	742	VCD 541 VAC Heater	36	315,360	8,760
744         ACD 543 Crude Heater         260         2,277,600         8,760           745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           165         Tank 93         -         -         8,760           166         Tank 94         -         -         8,760           127         Tank 96         -         -         8,760           137         Tank 152         -         -         8,760           137         Tank 152         -         -         8,760           137         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           140         Tank 157         -         -         8,760           143         Tank 158         -         -	743	VCD 542 VAC Heater	20	175,200	8,760
745         ACD 544 Crude Heater         260         2,277,600         8,760           34         Boiler 9         -         -         8,760           35         Boiler 10         -         -         8,760           102         SRU         -         -         8,760           103         Main Flare         -         -         8,760           165         Tank 93         -         -         8,760           166         Tank 94         -         -         8,760           126         Tank 95         -         -         8,760           127         Tank 96         -         -         8,760           133         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           142         Tank 157         -         -         8,760           143         Tank 158 (Source ID 193)         -         -         8,760           143         Tank 158 (Source ID 193)         -         -         8,760           144         Tank 159         -         -	746	VCD 544 VAC Heater	71	621,960	8,760
34	744	ACD 543 Crude Heater	260	2,277,600	8,760
35	745	ACD 544 Crude Heater	260	2,277,600	8,760
102   SRU	34	Boiler 9	-	-	8,760
103	35	Boiler 10	-	-	8,760
165	102	SRU	-	-	8,760
166	103	Main Flare	-	-	8,760
126	165	Tank 93	-	-	8,760
127         Tank 96         -         -         8,760           137         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           142         Tank 157         -         -         8,760           300         Tank 158 (Source ID 193)         -         -         8,760           143         Tank 159         -         -         8,760           194         Tank 160         -         -         8,760           194         Tank 161         -         -         8,760           144         Tank 161         -         -         8,760           1445         Tank 162         -         -         8,760           144         Tank 163         -         -         8,760           147         Tank 164         -         -         8,760           148         Tank 165         -         -         8,760           149         Tank 166         -         -         8,760           150         Tank 168         -         -         8,760 </td <td>166</td> <td>Tank 94</td> <td>-</td> <td>-</td> <td>8,760</td>	166	Tank 94	-	-	8,760
137         Tank 152         -         -         8,760           138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           142         Tank 157         -         -         8,760           300         Tank 158 (Source ID 193)         -         -         8,760           143         Tank 159         -         -         8,760           194         Tank 160         -         -         8,760           144         Tank 161         -         -         8,760           144         Tank 162         -         -         8,760           145         Tank 163         -         -         8,760           147         Tank 164         -         -         8,760           148         Tank 165         -         -         8,760           149         Tank 166         -         -         8,760           150         Tank 168         -         -         8,760           155         Tank 170         -         -         8,760           155         Tank 175         -         -         8,760 </td <td>126</td> <td>Tank 95</td> <td>-</td> <td>-</td> <td>8,760</td>	126	Tank 95	-	-	8,760
138         Tank 153         -         -         8,760           140         Tank 155         -         -         8,760           142         Tank 157         -         -         8,760           300         Tank 158 (Source ID 193)         -         -         8,760           143         Tank 159         -         -         8,760           194         Tank 160         -         -         8,760           144         Tank 161         -         -         8,760           145         Tank 162         -         -         8,760           146         Tank 163         -         -         8,760           147         Tank 164         -         -         8,760           148         Tank 165         -         -         8,760           149         Tank 166         -         -         8,760           150         Tank 168         -         -         8,760           152         Tank 170         -         -         8,760           155         Tank 174         -         -         8,760           157         Tank 178         -         -         8,760 </td <td>127</td> <td>Tank 96</td> <td>-</td> <td>-</td> <td>8,760</td>	127	Tank 96	-	-	8,760
140         Tank 155         -         -         8,760           142         Tank 157         -         -         8,760           300         Tank 158 (Source ID 193)         -         -         8,760           143         Tank 159         -         -         8,760           194         Tank 160         -         -         8,760           144         Tank 161         -         -         8,760           145         Tank 162         -         -         8,760           146         Tank 163         -         -         8,760           147         Tank 164         -         -         8,760           148         Tank 165         -         -         8,760           149         Tank 166         -         -         8,760           150         Tank 168         -         -         8,760           152         Tank 170         -         -         8,760           155         Tank 174         -         -         8,760           157         Tank 178         -         -         8,760           157         Tank 181         -         -         8,760 </td <td>137</td> <td>Tank 152</td> <td>-</td> <td>-</td> <td>8,760</td>	137	Tank 152	-	-	8,760
142         Tank 157         -         -         8,760           300         Tank 158 (Source ID 193)         -         -         8,760           143         Tank 159         -         -         8,760           194         Tank 160         -         -         8,760           144         Tank 161         -         -         8,760           145         Tank 162         -         -         8,760           146         Tank 163         -         -         8,760           147         Tank 164         -         -         8,760           148         Tank 165         -         -         8,760           149         Tank 166         -         -         8,760           150         Tank 168         -         -         8,760           152         Tank 170         -         -         8,760           155         Tank 174         -         -         8,760           156         Tank 178         -         -         8,760           157         Tank 181         -         -         8,760           160         Tank 182         -         -         8,760 </td <td>138</td> <td>Tank 153</td> <td>-</td> <td>-</td> <td>8,760</td>	138	Tank 153	-	-	8,760
Tank 158 (Source ID 193)   -	140	Tank 155	-	-	8,760
143       Tank 159       -       -       8,760         194       Tank 160       -       -       8,760         144       Tank 161       -       -       8,760         145       Tank 162       -       -       8,760         146       Tank 163       -       -       8,760         147       Tank 164       -       -       8,760         148       Tank 165       -       -       8,760         149       Tank 166       -       -       8,760         150       Tank 168       -       -       8,760         152       Tank 170       -       -       8,760         155       Tank 174       -       -       8,760         156       Tank 175       -       -       8,760         157       Tank 178       -       -       8,760         160       Tank 181       -       -       8,760         163       Tank 185       -       -       8,760         164       Tank 186       -       -       8,760         New Units       -       Feed Heater 1       99.6       872,496       8,760	142	Tank 157	-	-	8,760
194       Tank 160       -       -       8,760         144       Tank 161       -       -       8,760         145       Tank 162       -       -       8,760         146       Tank 163       -       -       8,760         147       Tank 164       -       -       8,760         148       Tank 165       -       -       8,760         149       Tank 166       -       -       8,760         150       Tank 168       -       -       8,760         152       Tank 170       -       -       8,760         155       Tank 174       -       -       8,760         156       Tank 175       -       -       8,760         157       Tank 178       -       -       8,760         160       Tank 181       -       -       8,760         163       Tank 185       -       -       8,760         164       Tank 186       -       -       8,760         New Units         -       Feed Heater 1       99.6       872,496       8,760         -       Feed Heater 2       44.2       387,192 <t< td=""><td></td><td></td><td>-</td><td>-</td><td>·</td></t<>			-	-	·
144       Tank 161       -       -       8,760         145       Tank 162       -       -       8,760         146       Tank 163       -       -       8,760         147       Tank 164       -       -       8,760         148       Tank 165       -       -       8,760         149       Tank 166       -       -       8,760         150       Tank 168       -       -       8,760         152       Tank 170       -       -       8,760         155       Tank 174       -       -       8,760         156       Tank 175       -       -       8,760         157       Tank 178       -       -       8,760         160       Tank 181       -       -       8,760         161       Tank 182       -       -       8,760         164       Tank 186       -       -       8,760         New Units       -       Feed Heater 1       99.6       872,496       8,760         -       Feed Heater 2       44.2       387,192       8,760			-	-	·
145     Tank 162     -     -     8,760       146     Tank 163     -     -     8,760       147     Tank 164     -     -     8,760       148     Tank 165     -     -     8,760       149     Tank 166     -     -     8,760       150     Tank 168     -     -     8,760       152     Tank 170     -     -     8,760       155     Tank 174     -     -     8,760       156     Tank 175     -     -     8,760       157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760			-	-	·
146     Tank 163     -     -     8,760       147     Tank 164     -     -     8,760       148     Tank 165     -     -     8,760       149     Tank 166     -     -     8,760       150     Tank 168     -     -     8,760       152     Tank 170     -     -     8,760       155     Tank 174     -     -     8,760       156     Tank 175     -     -     8,760       157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760			-		·
147         Tank 164         -         -         8,760           148         Tank 165         -         -         8,760           149         Tank 166         -         -         8,760           150         Tank 168         -         -         8,760           152         Tank 170         -         -         8,760           155         Tank 174         -         -         8,760           156         Tank 175         -         -         8,760           157         Tank 178         -         -         8,760           160         Tank 181         -         -         8,760           161         Tank 182         -         -         8,760           163         Tank 185         -         -         8,760           New Units           -         Feed Heater 1         99.6         872,496         8,760           -         Feed Heater 2         44.2         387,192         8,760					·
148     Tank 165     -     -     8,760       149     Tank 166     -     -     8,760       150     Tank 168     -     -     8,760       152     Tank 170     -     -     8,760       155     Tank 174     -     -     8,760       156     Tank 175     -     -     8,760       157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760					·
149     Tank 166     -     -     8,760       150     Tank 168     -     -     8,760       152     Tank 170     -     -     8,760       155     Tank 174     -     -     8,760       156     Tank 175     -     -     8,760       157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760					· ·
150         Tank 168         -         -         8,760           152         Tank 170         -         -         8,760           155         Tank 174         -         -         8,760           156         Tank 175         -         -         8,760           157         Tank 178         -         -         8,760           160         Tank 181         -         -         8,760           161         Tank 182         -         -         8,760           163         Tank 185         -         -         8,760           164         Tank 186         -         -         8,760           New Units           -         Feed Heater 1         99.6         872,496         8,760           -         Feed Heater 2         44.2         387,192         8,760			-		· · · · · · · · · · · · · · · · · · ·
152     Tank 170     -     -     8,760       155     Tank 174     -     -     8,760       156     Tank 175     -     -     8,760       157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760		ł	-		
155         Tank 174         -         -         8,760           156         Tank 175         -         -         8,760           157         Tank 178         -         -         8,760           160         Tank 181         -         -         8,760           161         Tank 182         -         -         8,760           163         Tank 185         -         -         8,760           164         Tank 186         -         -         8,760           New Units           -         Feed Heater 1         99.6         872,496         8,760           -         Feed Heater 2         44.2         387,192         8,760					
156     Tank 175     -     -     8,760       157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760				1	·
157     Tank 178     -     -     8,760       160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760					·
160     Tank 181     -     -     8,760       161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760					·
161     Tank 182     -     -     8,760       163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760					·
163     Tank 185     -     -     8,760       164     Tank 186     -     -     8,760       New Units       -     Feed Heater 1     99.6     872,496     8,760       -     Feed Heater 2     44.2     387,192     8,760					
164         Tank 186         -         -         8,760           New Units         -         -         8,760           -         Feed Heater 1         99.6         872,496         8,760           -         Feed Heater 2         44.2         387,192         8,760			<del>-</del>		
New Units         -         Feed Heater 1         99.6         872,496         8,760           -         Feed Heater 2         44.2         387,192         8,760			<u>-</u>	1	· ·
-         Feed Heater 1         99.6         872,496         8,760           -         Feed Heater 2         44.2         387,192         8,760		1 and 100	-	<u> </u>	0,700
- Feed Heater 2 44.2 387,192 8,760		Food Hostor 1	00.6	872 406	8 760
				· · · · · · · · · · · · · · · · · · ·	·
- 1.00HIP LOWEL 3.70H					
- Fugitives 8,760		Ŭ			

 $<sup>^{\</sup>rm (a)}$  Based on 195,000 BPD crude rate from 10 year plan.

<sup>(</sup>b) Emissions are based on pounds of coke burned in the catalyst regenerator instead of fuel. Please see table C-4 for more details.

## Table C-4 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the FCC Unit - Source ID 101

Pollutant	Emission	Emission Factor	Notes	Projected Actual Emissions <sup>(a)</sup>		
	Factor	Units		lb/hr	tpy	
Filterable PM	0.45	lb/10 <sup>3</sup> lb coke	Stack test data from 2015	19.32	84.62	
Condensable PM	0.15	lb/10 <sup>3</sup> lb coke	Stack test data from 2013.	6.51	28.52	
Total PM <sub>10</sub>	0.59	lb/10 <sup>3</sup> lb coke	Stack test data from 2013 and Emission Estimation Protocol for Petroleum Refineries Version 2.1.1, May 2011, Table 5-2 Default Size Distribution for Filterable PM from CCU.	25.25	110.60	
Total PM <sub>2.5</sub>	0.52	lb/10 <sup>3</sup> lb coke	Stack test data from 2013 and Emission Estimation Protocol for Petroleum Refineries Version 2.1.1, May 2011, Table 5-2 Default Size Distribution for Filterable PM from CCU.	21.97	96.21	
$SO_2$	0.48	lb/10 <sup>3</sup> lb coke	2015 CEMS data.	20.28	88.82	
$NO_X$	2.32	lb/10 <sup>3</sup> lb coke	2015 CEMS data.	98.75	432.52	
VOC	0.73	lb/hr	Emission factor from historical stack testing.	0.73	3.20	
CO	8.77E-02	lb/10 <sup>3</sup> lb coke	2015 CEMS data.	3.73	16.35	
Lead	N/A	N/A	No available emissions factor.	-	-	
$H_2S$	N/A	N/A	No available emissions factor.	-	-	
TRS	N/A	N/A	No available emissions factor.	-	-	
$CO_2$	102.41	kg/MMBtu	40 CFR Part 98 Subpart Y. Equation Y-6 <sup>(b)</sup>	172,322.68	754,773.34	
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart Y, Equation Y-10	1.01	4.42	
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart Y, Equation Y-9	5.05	22.11	
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	172,328.74	754,800	
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	172,750	756,644	

<sup>(</sup>a) Particle size distributions per the Emission Estimation Protocol for Petroleum Refineries Version 2.1.1, May 2011, Table 5-2 Default Size Distribution for Filterable PM from CCU; CCU with post-regenerator PM control device (tertiary cyclone, wet scrubber, ESP or fabric filter).

Pollutant	Fraction	Units/Notes
Filterable PM <sub>10</sub>	97	%
Filterable PM <sub>2.5</sub>	80	%

(a) Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Projected Future Fuel Usage	42,554	lb coke burned/hr
Operating Hours	8,760	hr/yr
Conversion Factor 1	2,000	lb/ton
Conversion Factor 2	1,000	lb/M lb
Conversion Factor 3	1.10E-03	tons/kg

(b) CO<sub>2</sub> emissions are based upon the following parameters, in accordance with 40 CFR Part 98 Subpart Y, Equation Y-6:

Parameter	Value	Units/Notes
Future Exhaust Flowrate	98,362	dscfm
Future CO <sub>2</sub> Fuel Gas Content	17.24	% by volume
Future CO Fuel Gas Content	7.95	% by volume
Molecular Weight of CO2	44.00	kg/kg-mol
Molar Volume Conversion Factor	836.60	scf/kg-mol at 60 deg and 14.7 psia
Conversion Factor 1	60	min/hr
Conversion Factor 2	2.20	lb/kg

<sup>(</sup>c) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where GHGi = annual mass emissions of greenhouse gas i (short tons/year)

GWPi = global warming potential of greenhouse gas i from the table below

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-5 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from FCCU Feed Heater - Source ID 733

Pollutant	Emission Factor	Emission Factor Units	Notes	_	tual Emissions a)
	Factor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.04	0.18
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.16	0.72
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.16	0.72
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed $H_2S$ content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of $H_2S$ to $SO_2$ .	0.31	0.78
302	50	ppmdv	Based upon TVOP No. 23-00003 limit for $H_2S$ from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of $H_2S$ to $SO_2$ .	0.31	0.76
$NO_X$	0.03	lb/MMBtu	Stack test data from 2013.	0.69	3.02
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.12	0.52
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	1.81	7.93
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.08E-05	4.72E-05
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.96E-03	8.56E-03
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.96E-03	8.56E-03
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	2,992	13,104
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.03	0.13
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.15	0.67
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	2,992	13,104
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	3,005	13,160

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	23	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,068	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{(</sup>b)}$ CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

 $\label{eq:where GHGi} where \ GHGi = annual \ mass \ emissions \ of \ greenhouse \ gas \ i \ (short tons/year)$   $GWPi = global \ warming \ potential \ of \ greenhouse \ gas \ i \ from \ the \ table \ below$ 

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-6 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Kerosene/HCN HTU Feed Heater - Source ID 735

Pollutant	Emission Factor	Emission Factor	Notes	Projected Act	ual Emissions
	ractor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.01	0.06
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.06	0.25
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.06	0.25
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed $H_2S$ content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of $H_2S$ to $SO_2$ .	0.11	0.28
$3O_2$	50	ppmdv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.11	0.28
$NO_X$	0.124	lb/MMBtu	Stack test data from 2005.	1.03	4.51
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.04	0.18
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	0.64	2.81
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	3.82E-06	1.67E-05
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		3.09E-03
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		3.09E-03
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	1,080	4,729
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.01	0.05
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.05	0.24
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .		4,729
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	1,084	4,749

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	8.3	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,086	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-7 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Diesel HTU Heater - Source ID 736

Pollutant	Emission	Emission Factor	Notes	Projected Actual Emissions (a)	
Pollutant	Factor	Units	Notes	lb/hr	tpy
Filterable PM	0.0012	lb/MMBtu	Stack test data from 2013.	0.02	0.11
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.14	0.62
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.14	0.62
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.26	0.67
302	50	ppmdv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.20	0.07
$NO_X$	0.158	lb/MMBtu	Stack test data from 2013.	3.16	13.84
VOC	0.0045	lb/MMBtu	Stack test data from 2013.	0.09	0.39
СО	0.002	lb/MMBtu	Stack test data from 2013.	0.04	0.18
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	9.25E-06	4.05E-05
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.70E-03	7.45E-03
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.70E-03	7.45E-03
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	2,601	11,394
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.03	0.12
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.13	0.58
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	2,602	11,395
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	2,613	11,443

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	20	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,081	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{\</sup>text{(b)}}\text{CO}_2\text{e}$  is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-8 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the D2/VGO Hydrotreater Feed Heater - Source ID 741

Pollutant	Emission		Notes	Projected Actual Emissions (a)	
	Factor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.03	0.15
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.13	0.59
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.13	0.59
SO <sub>2</sub>	0.1	gr/dscf	Based on allowed short-term $H_2S$ content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of $H_2S$ to $SO_2$ .	0.25	0.61
302	48	ppmv	Based upon TVOP No. 23-00003 limit for $H_2S$ from refinery fuel gas fired from the south side fuel supply. Assumed full conversion of $H_2S$ to $SO_2$ .	0.23	0.01
$NO_X$	100	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	1.76	7.71
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.10	0.42
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	1.48	6.48
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	8.80E-06	3.86E-05
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		6.70E-03
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.53E-03	6.70E-03
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	2,341	10,255
$N_2O$	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.02	0.10
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.12	0.52
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .		10,256
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	2,351	10,299

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	18	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,023	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-9 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Naphtha HDS Heater - Source ID 737

Pollutant	Emission	Emission Factor	Notes	Projected Actual Emissic	
	Factor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.14	0.61
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.56	2.43
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.56	2.43
20	0.1	gr/dscf	Based on allowed short-term $H_2S$ content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of $H_2S$ to $SO_2$ .	1.04	2.55
$SO_2$	48	ppmv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the south side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	1.04	2.55
$NO_X$	0.1	lb/MMBtu	Stack Test Data from 1994	7.60	33.29
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.40	1.76
CO	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	6.14	26.88
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	3.65E-05	1.60E-04
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.  6.46E-0		0.03
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.03
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	9,886	43,299
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.10	0.44
$\mathrm{CH}_4$	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.50	2.20
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 9,88		43,301
$CO_2e^{(b)}$	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.		43,485

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	76	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,040	MMBtu/MMSCF
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

## Table C-10 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Platformer Feed Heater - Source ID 738

Pollutant	Emission	Emission Factor	Notes	•	ual Emissions a)
	Factor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.93	4.06
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	3.71	16.23
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	3.71	16.23
SO <sub>2</sub>	0.1	gr/dscf	Based on allowed short-term H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	6.97	17.03
302	48	ppmv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the south side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.97	17.03
$NO_X$	0.086	lb/MMBtu	Stack Testing Data	42.40	185.70
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	2.68	11.75
СО	3.30E-05	lb/MMBtu	Stack Testing Data	0.03	0.15
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	2.44E-04	1.07E-03
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.18
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.04	0.18
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	64,126	280,871
$N_2O$	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.65	2.86
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	3.26	14.28
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 64129.		280,888
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.  64401.63		282,079

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	493	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,011	MMBtu/MMSCF
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-11 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Isocracker 1st Stage Heater - Source ID 739

	Emission	Emission Factor			Actual Emissions	
Pollutant	Factor	Units	Notes		a) 	
				lb/hr	tpy	
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.06	0.26	
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.24	1.03	
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.24	1.03	
SO <sub>2</sub>	0.1	gr/dscf	Based on allowed short-term H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.44	1.08	
302	48	ppmv	Based upon TVOP No. 23-00003 limit for $H_2S$ from refinery fuel gas fired from the south side fuel supply. Assumed full conversion of $H_2S$ to $SO_2$ .	0.44	1.08	
$NO_X$	0.116	lb/MMBtu	Stack test data from 2008.	3.83	16.77	
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.17	0.75	
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	2.61	11.43	
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2 1.55E-05		6.80E-05	
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.01	
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.  2.81E-03		0.01	
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	4,292	18,801	
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.04	0.19	
$\mathrm{CH}_4$	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2		0.96	
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 4292.66		18,802	
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1. 4310.86		18,882	

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	33	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,063	MMBtu/MMSCF
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-12 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Isocracker Splitter Reboiler - Source ID 740

Pollutant	Pollutant Emission Emission Factor		Notes	Projected Actual Emissions	
	Factor	Units	110000	lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.08	0.34
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.31	1.37
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.31	1.37
80	0.1	gr/dscf	Based on allowed short-term H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.59	1.44
$SO_2$	48	ppmv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the south side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.59	1,44
$NO_X$	100	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	4.12	18.05
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.23	0.99
CO	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1	3.46	15.17
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2 2.06E-05		9.03E-05
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.02
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.  3.74E-03		0.02
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	5,723	25,068
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.06	0.25
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.29	1.27
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 5723.54		25,069
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.		25,175

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	44	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,067	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{\</sup>text{(b)}}\text{CO}_2\text{e}$  is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-13 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the VCD 541 VAC Heater - Source ID 742

Pollutant	Emission	Emission Factor	Notes	Projected Actual Emissio		
Factor		Units		lb/hr	tpy	
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.06	0.27	
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.24	1.06	
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.24	1.06	
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.46	1.16	
$3O_2$	50	ppmdv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.40	1.10	
$NO_X$	0.13	lb/MMBtu	Stack test data from 1994.	4.68	20.50	
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.18	0.77	
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1		11.76	
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2		7.00E-0	
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.  3.06E-03		0.01	
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	3.06E-03	0.01	
CO <sub>2</sub>	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	4,683	20,510	
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.05	0.21	
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.24	1.04	
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 468		20,51	
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.		20,598	

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	36	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,127	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-14 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the VCD 542 VAC Heater - Source ID 743

Pollutant	Emission	Emission Factor	Notes	Projected Act	tual Emissi a)
Fact		Units		lb/hr tpy	
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.04	0.15
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.14	0.62
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.14	0.62
$SO_2$	0.1	gr/dscf	Based on short-term allowed H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.26	0.67
$3O_2$	50	ppmdv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.20	0.07
$NO_X$	0.077	lb/MMBtu	Stack test data from 1999.	1.54	6.75
VOC	0.00032	lb/MMBtu	Stack test data from 1999.	6.40E-03	0.03
СО	0.00024	lb/MMBtu	Stack test data from 1999.	4.80E-03	0.02
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	9.27E-06	4.06E-0
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.70E-03	7.45E-0
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	1.70E-03	7.45E-0
CO <sub>2</sub>	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	2,601	11,394
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.03	0.12
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.13	0.58
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	2601.61	11,39
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.		11,443

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	20	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,079	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{(</sup>b)}$ CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-15 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the VCD 544 VAC Heater - Source ID 746

Pollutant	Emission	Emission Factor	Notes	Projected Actual Emissions (a)	
	Factor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.12	0.55
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.50	2.19
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.50	2.19
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.94	2.39
302	50	ppmdv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	0.94	2.39
$NO_X$	0.04	lb/MMBtu	Stack test data from 2013.	2.84	12.44
VOC	0.007	lb/MMBtu	Stack test data from 2007.	0.50	2.18
СО	0.017	lb/MMBtu	Stack test data from 2006.	1.21	5.29
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	3.29E-05	1.44E-04
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.03
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	6.04E-03	0.03
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	9,235	40,450
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.09	0.41
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.47	2.06
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .		40,452
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.  9,275		40,624

 $^{\rm (a)}$  Projected future  $\underline{\rm actual}$  emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	71	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,080	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{\</sup>text{(b)}}\text{CO}_2\text{e}$  is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-16 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the ACD 543 Crude Heater - Source ID 744

Pollutant	Emission	Emission Factor	Notes	_	ual Emissions
	Factor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.46	2.01
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.83	8.02
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.83	8.02
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed H <sub>2</sub> S content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	3.44	8.77
302	50	ppmdv	Based upon TVOP No. 23-00003 limit for H <sub>2</sub> S from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of H <sub>2</sub> S to SO <sub>2</sub> .	3.44	6.77
$NO_X$	0.04	lb/MMBtu	Stack test data from 2003.	10.40	45.55
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.33	5.81
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-1 20		88.66
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2 1.20E-0		5.28E-04
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.10
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.  0.02		0.10
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	33,819	148,127
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.34	1.51
$\mathrm{CH_4}$	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	1.72	7.53
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 33820.93		148,136
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	33964.35	148,764

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	260	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,079	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{(</sup>b)}$ CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

## Table C-17 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the ACD 544 Crude Heater - Source ID 745

Pollutant	Emission Factor	Emission Factor Units	Notes	_	ual Emissions
	ractor	Units		lb/hr	tpy
Filterable PM	1.9	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.46	2.00
Total PM <sub>10</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.83	8.01
Total PM <sub>2.5</sub>	7.6	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.83	8.01
SO <sub>2</sub>	0.1	gr/dscf	Based on short-term allowed $H_2S$ content in refinery fuel gas, found at 40 CFR §§60.104(a)(1). Assumed full conversion of $H_2S$ to $SO_2$ .	3.44	8.75
302	50	ppmdv	Based upon TVOP No. 23-00003 limit for $H_2S$ from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of $H_2S$ to $SO_2$ .	3.44	6.73
$NO_X$	0.04	lb/MMBtu	Stack test data from 2003.	11.44	50.11
VOC	5.5	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.32	5.80
СО	84	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	20.22	88.55
Lead	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2 1.20E-		5.27E-04
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.10
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.		0.10
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	33,819	148,127
$N_2O$	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	0.34	1.51
$\mathrm{CH_4}$	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	1.72	7.53
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> . 33820.93		148,136
CO <sub>2</sub> e <sup>(b)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.  33964.35		148,764

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Projected Heat Duty	260	MMBtu/hr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,080	MMBtu/MMscf
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Conversion Factor 2	2.20	lb/kg
Conversion Factor 3	1,000,000	Btu/MMBtu
Conversion Factor 4	7,000	gr/lb
Gas at Standard Conditions	385.35	scf/lb-mol

 $<sup>^{(</sup>b)}$ CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

# Table C-18 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from Boiler 9

	T	Emission		Projected F	uture Actual	
Pollutant	Emission Factor	Factor	Notes	Emissions <sup>(a),(b)</sup>		
	Factor	Units		lb/hr	tpy	
Filterable PM	7.00E-04	lb/MMBtu	2014 stack test data	0.17	0.72	
Total PM <sub>10</sub>	5.50E-03	lb/MMBtu	2014 stack test data	1.30	5.69	
Total PM <sub>2.5</sub>	4.90E-03	lb/MMBtu	2014 stack test data	1.16	5.07	
$SO_2$	1.00E-03	lb/MMBtu	CEM data and 2009 stack test	0.24	1.04	
$NO_X$	4.26E-03	lb/MMBtu	2014 CEMS data - annual average of hourly data	1.01	4.41	
VOC	2.97E-04	lb/MMBtu	2014 stack test data	0.07	0.31	
СО	1.29E-03	lb/MMBtu	2014 CEMS data - annual average of hourly data	0.31	1.34	
Pb	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.10E-04	4.80E-04	
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.02	0.09	
TRS <sup>(c)</sup>	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.02	0.09	
$CO_2$	120,000	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	26,307.79	115,228.12	
N <sub>2</sub> O	2.2	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.48	2.11	
CH <sub>4</sub>	2.3	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.50	2.21	
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	26,308.78	115,232.44	
CO <sub>2</sub> e <sup>(d)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	26,464.12	115,912.86	

<sup>(</sup>a) Monroe proportionally added the fuel needed to accommodate the additional steam demand based on fuel usages in 2013 and 2014 to the maximum baseline fuel usage of Boilers 9 and 10, as shown below. Fuel additions were based on a total additional steam demand of 18,900 lbs/hr, 8,760 hours of operating per year, and an assumed heat input of 1,350 Btu to generate 1 lb of steam.

Baseline Yea	rs	Fuel Usage + Additional for Steam Demand (MMcf/yr)
2013	2014	1,920.47

(b) Projected future actual emissions were calculated assuming the following:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,078	MMBtu/MMscf

<sup>(</sup>c) Emission factor for TRS is assumed to be equal to the emission factor for H<sub>2</sub>S.

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where  $GHGi = annual\ mass\ emissions\ of\ greenhouse\ gas\ i\ (short\ tons/year)$ 

 $GWPi = global \ warming \ potential \ of \ greenhouse \ gas \ i \ from \ Table \ A-1 \ (below)$ 

Pollutant	GWP (100 year)
CO <sub>2</sub>	1
$N_2O$	298
CH <sub>4</sub>	25

 $<sup>^{(</sup>d)}$  CO $_2$ e is carbon dioxide equivalent, calculated according to 40 CFR Part 98 Equation A-1:

# Table C-19 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from Boiler 10

	T	Emission		Projected F	uture Actual	
Pollutant	Emission Factor	Factor	Notes	Emissions <sup>(a),(b)</sup>		
	Factor	Units		lb/hr	tpy	
Filterable PM	4.00E-04	lb/MMBtu	2014 stack test data	0.09	0.40	
Total PM <sub>10</sub>	3.10E-03	lb/MMBtu	2014 stack test data	0.70	3.07	
Total PM <sub>2.5</sub>	3.00E-03	lb/MMBtu	2014 stack test data	0.68	2.97	
$SO_2$	3.00E-03	lb/MMBtu	CEM data and 2009 stack test	0.68	2.97	
$NO_X$	3.96E-03	lb/MMBtu	2014 CEMS data - annual average of hourly data	0.90	3.93	
VOC	2.69E-04	lb/MMBtu	2014 stack test data	0.06	0.27	
СО	4.97E-03	lb/MMBtu	2014 CEMS data - annual average of hourly data	1.13	4.93	
Pb	5.00E-04	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	1.05E-04	4.60E-04	
$H_2S$	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.02	0.08	
TRS <sup>(c)</sup>	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.02	0.08	
$CO_2$	120,000	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	25,192.19	110,341.81	
$N_2O$	2.2	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.46	2.02	
CH <sub>4</sub>	2.3	lb/MMSCF	AP-42 Chapter 1.4 Natural Gas Combustion Table 1.4-2	0.48	2.11	
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	25,193.14	110,345.95	
CO <sub>2</sub> e <sup>(d)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	25,341.90	110,997.52	

<sup>(</sup>a) Monroe proportionally added the fuel needed to accommodate the additional steam demand based on fuel usages in 2013 and 2014 to the maximum baseline fuel usage of Boilers 9 and 10, as shown below. Fuel additions were based on a total additional steam demand of 18,900 lbs/hr, 8,760 hours of operating per year, and an assumed heat input of 1,350 Btu to generate 1 lb of steam.

Baseline Yea	rs	Fuel Usage + Additional for Steam Demand (MMcf/yr)
2013	2014	1,839.03

<sup>(</sup>b) Projected future actual emissions were calculated assuming the following:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Conversion Factor 1	2,000	lb/ton
Fuel Gas Heating Value	1,078	MMBtu/MMscf

<sup>(</sup>c) Emission factor for TRS is assumed to be equal to the emission factor for H<sub>2</sub>S.

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where  $GHGi = annual\ mass\ emissions\ of\ greenhouse\ gas\ i\ (short\ tons/year)$ 

GWPi = global warming potential of greenhouse gas i from Table A-1 (below)

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

 $<sup>^{(</sup>d)}$  CO $_2$ e is carbon dioxide equivalent, calculated according to 40 CFR Part 98 Equation A-1:

### Table C-20 Monroe Energy, LLC - Trainer, PA Refinery

### Projected Actual Emissions from the Claus SRU - Source ID $102^{(a)}$

Pollutant	Notes	Projected Actual Emissions <sup>(b)</sup>			
		lb/hr	tpy		
Filterable PM	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.03	0.11		
Total PM <sub>10</sub>	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.10	0.44		
Total PM <sub>2.5</sub>	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.10	0.44		
SO <sub>2</sub>	Projected actual emissions are developed based on 2014 production and applying an increase of 2.4 long tons of sulfur per day for future production.	9.21	40.33		
$NO_X$	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	1.33	5.83		
VOC	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.07	0.32		
СО	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	1.12	4.90		
Lead	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	6.66E-06	2.92E-05		
H <sub>2</sub> S	Assumed to be converted to SO <sub>2</sub>	0.00	0.00		
TRS	No available emissions factor.	-	-		
$\mathrm{CO}_2$	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	6,738	29,513		
N <sub>2</sub> O	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.07	0.30		
CH <sub>4</sub>	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	20.34	89.09		
Total GHG	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	6,759	29,603		
CO <sub>2</sub> e <sup>(b)</sup>	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	7,267	31,829		

<sup>(</sup>a) A plan approval application that affects the SRU was submitted to PADEP on May 18, 2015. The expected emissions increase resulting from the modifications proposed in that application have not been incorporated into the project actual emissions for the SRU in this application. The expected emissions increases from the May 18, 2015 plan approval application have been accounted for in the contemporaneous emission increases analysis, shown in Table C-37.

(b) Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Operating Hours	24	hr/day
Maximum Sulfur Loading 2014	50.7	long tons sulfur/day
Future Sulfur Loading Increase	2.4	long tons sulfur/day
Maximum SO <sub>2</sub> Emission Factor 2014	4.16	lb SO2/long ton sulfur
Conversion Factor 1	2,000	lb/ton

 $<sup>^{(</sup>b)}\mathrm{CO}_2\mathrm{e}$  is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where GHGi = annual mass emissions of greenhouse gas i (short tons/year) GWPi = global warming potential of greenhouse gas i from the table below

Pollutant	GWP (100 year)
$CO_2$	1
N <sub>2</sub> O	298
$CH_4$	25

Table C-21

Monroe Energy, LLC - Trainer, PA Refinery

Historical 2013-2014 Monthly Actual Emissions from the Claus SRU - Source ID 102

Date <sup>(a)</sup>	Filterable PM	Total PM <sub>10</sub>	Total PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>x</sub>	voc	со	Lead	H <sub>2</sub> S <sup>(b)</sup>	CO <sub>2</sub>	CH₄	N <sub>2</sub> O
	(tons) <sup>(c)</sup>											
Jan-13	7.09E-03	2.83E-02	2.83E-02	0.82	0.37	2.05E-02	0.31	1.86E-06	N/A	4,581	13.83	0.05
Feb-13	5.91E-03	2.36E-02	2.36E-02	1.20	0.31	1.71E-02	0.26	1.56E-06	N/A	1,611	4.86	0.02
Mar-13	5.99E-03	2.40E-02	2.40E-02	2.29	0.32	1.73E-02	0.26	1.58E-06	N/A	1,186	3.58	0.01
Apr-13	4.40E-03	1.76E-02	1.76E-02	1.34	0.23	1.27E-02	0.19	1.16E-06	N/A	1,606	4.85	0.02
May-13	4.42E-03	1.77E-02	1.77E-02	1.18	0.23	1.28E-02	0.20	1.16E-06	N/A	1,168	3.52	0.01
Jun-13	4.83E-03	1.93E-02	1.93E-02	1.16	0.25	1.40E-02	0.21	1.27E-06	N/A	2,089	6.31	0.02
Jul-13	5.19E-03	2.08E-02	2.08E-02	1.59	0.27	1.50E-02	0.23	1.37E-06	N/A	2,874	8.68	0.03
Aug-13	5.30E-03	2.12E-02	2.12E-02	1.49	0.28	1.53E-02	0.23	1.39E-06	N/A	1,740	5.25	0.02
Sep-13	4.76E-03	1.90E-02	1.90E-02	1.20	0.25	1.38E-02	0.21	1.25E-06	N/A	1,031	3.11	0.01
Oct-13	4.45E-03	1.78E-02	1.78E-02	1.39	0.23	1.29E-02	0.20	1.17E-06	N/A	2,308	6.97	0.02
Nov-13	4.76E-03	1.90E-02	1.90E-02	1.26	0.25	1.38E-02	0.21	1.25E-06	N/A	1,852	5.59	0.02
Dec-13	7.80E-03	1.33E-02	1.33E-02	1.46	0.41	2.26E-02	0.34	2.05E-06	N/A	1,024	3.09	0.01
Jan-14	1.06E-02	4.23E-02	4.23E-02	0.84	0.56	3.06E-02	0.47	2.79E-06	N/A	2,396	7.23	0.02
Feb-14	7.87E-03	3.15E-02	3.15E-02	0.73	0.41	2.28E-02	0.35	2.07E-06	N/A	1,893	5.71	0.02
Mar-14	9.26E-03	3.71E-02	3.71E-02	1.10	0.49	2.68E-02	0.41	2.44E-06	N/A	2,328	7.03	0.02
Apr-14	7.11E-03	2.84E-02	2.84E-02	1.53	0.37	2.06E-02	0.31	1.87E-06	N/A	1,152	3.48	0.01
May-14	7.32E-03	2.93E-02	2.93E-02	1.21	0.39	2.12E-02	0.32	1.93E-06	N/A	1,269	3.83	0.01
Jun-14	6.59E-03	2.63E-02	2.63E-02	1.70	0.35	1.91E-02	0.29	1.73E-06	N/A	870	2.62	0.01
Jul-14	7.83E-03	3.13E-02	3.13E-02	1.56	0.41	2.27E-02	0.35	2.06E-06	N/A	1,169	3.53	0.01
Aug-14	7.10E-03	2.84E-02	2.84E-02	2.03	0.37	2.06E-02	0.31	1.87E-06	N/A	995	3.00	0.01
Sep-14	7.24E-03	2.90E-02	2.90E-02	2.15	0.38	2.10E-02	0.32	1.91E-06	N/A	1,074	3.24	0.01
Oct-14	7.62E-03	3.05E-02	3.05E-02	1.77	0.40	2.21E-02	0.34	2.01E-06	N/A	1,231	3.71	0.01
Nov-14	8.55E-03	3.42E-02	3.42E-02	2.33	0.45	2.47E-02	0.38	2.25E-06	N/A	1,484	4.48	0.01
Dec-14	8.91E-03	3.67E-02	3.67E-02	1.94	0.47	2.68E-02	0.41	2.44E-06	N/A	1,009	3.05	0.01
Maximum Three (3) Month Average Actual Emissions	9.24E-03	3.70E-02	3.70E-02	2.08	0.49	2.67E-02	0.41	2.43E-06	N/A	2,459	7.42	0.02
Three (3) Month Period	Jan-14	Jan-14	Jan-14	Sep-14	Jan-14	Jan-14	Jan-14	Jan-14	N/A	Jan-13	Jan-13	Jan-13
Three (5) William Terloa	Mar-14	Mar-14	Mar-14	Nov-14	Mar-14	Mar-14	Mar-14	Mar-14	N/A	Mar-13	Mar-13	Mar-13

 $<sup>^{(</sup>a)}$  The maximum three (3) month period of actual emissions are shown in bold for each pollutant.

<sup>(</sup>b) Assumed full conversion of H<sub>2</sub>S to SO<sub>2</sub>.

<sup>(</sup>c) Emissions shown here were calculated using the reported emissions and their associated calculation methods by the Trainery Refinery.

## Table C-22 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from the Main Flare - Source ID 103

Pollutant	Notes	Projected Actual Emissions <sup>(a)</sup>				
		lb/hr	tpy			
Filterable PM	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.29	1.25			
Total PM <sub>10</sub>	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.40	1.74			
Total PM <sub>2.5</sub>	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.40	1.74			
$SO_2$	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.95	4.15			
$NO_X$	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.72	3.15			
VOC	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	1.48	6.48			
СО	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	3.91	17.13			
Lead	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	4.89E-05	2.14E-04			
$H_2S$	No emission factors are available.	0.56	2.47			
TRS	Assumed to be converted to SO <sub>2</sub>	-	-			
$CO_2$	No available emissions factor.	1347.65	5,903			
N₂O	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	0.01	5.90E-02			
CH <sub>4</sub>	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	4.07	17.82			
Total GHG	Projected actual emissions are developed by annualizing the average of the three (3) highest emitting months from 2013-2014.	1351.73	5,921			
CO <sub>2</sub> e <sup>(b)</sup>	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	1347.65	6,366			

 $^{\rm (a)}$  Projected future actual emissions are based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Conversion Factor 1	2,000	lb/ton
Control Efficiency from Flare Gas	80	%
Recovery System	80	70

<sup>(</sup>b) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where  $GHGi = annual\ mass\ emissions\ of\ greenhouse\ gas\ i\ (short\ tons/year)$   $GWPi = global\ warming\ potential\ of\ greenhouse\ gas\ i\ from\ the\ table\ below$ 

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

Table C-23

Monroe Energy, LLC - Trainer, PA Refinery

Historical 2013-2014 Monthly Actual Emissions from the Main Flare - Source ID 103

	Filterable	Total	Total	SO <sub>2</sub>	NO <sub>x</sub>	voc	со	Lead	H₂S	CO <sub>2</sub>	СН₄	N <sub>2</sub> O
Date <sup>(a)</sup>	PM	PM <sub>10</sub>	PM <sub>2.5</sub>									
	(tons) <sup>(b)</sup>											
Jan-13	0.97	1.35	1.35	0.44	2.43	5.01	13.23	3.41E-05	0.36	4,581	13.83	0.05
Feb-13	0.34	0.48	0.48	1.53	0.86	1.78	4.70	1.18E-05	1.27	1,611	4.86	0.02
Mar-13	0.25	0.34	0.34	0.75	0.64	1.32	3.49	7.63E-06	0.18	1,186	3.58	0.01
Apr-13	0.35	0.45	0.45	0.72	0.89	1.83	4.84	8.38E-06	0.36	1,606	4.85	0.02
May-13	0.25	0.33	0.33	0.50	0.62	1.28	3.40	7.41E-06	0.33	1,168	3.52	0.01
Jun-13	0.46	0.55	0.55	1.39	1.15	2.37	6.26	8.41E-06	0.71	2,089	6.31	0.02
Jul-13	0.60	0.78	0.78	2.28	1.52	3.13	8.26	1.53E-05	0.98	2,874	8.68	0.03
Aug-13	0.38	0.48	0.48	1.51	0.94	1.95	5.14	8.78E-06	0.84	1,740	5.25	0.02
Sep-13	0.22	0.30	0.30	0.99	0.55	1.14	3.00	6.76E-06	0.54	1,031	3.11	0.01
Oct-13	0.49	0.62	0.62	1.82	1.23	2.53	6.68	1.13E-05	1.30	2,308	6.97	0.02
Nov-13	0.40	0.52	0.52	2.26	1.00	2.05	5.42	1.08E-05	1.25	1,852	5.59	0.02
Dec-13	0.21	0.26	0.26	0.28	0.53	1.10	2.90	3.95E-06	0.15	1,024	3.09	0.01
Jan-14	0.50	0.61	0.61	0.42	1.25	2.58	6.83	9.58E-06	0.24	2,396	7.23	0.02
Feb-14	0.40	0.50	0.50	0.49	1.02	2.10	5.55	8.06E-06	0.29	1,893	5.71	0.02
Mar-14	0.49	0.60	0.60	0.51	1.24	2.55	6.74	9.71E-06	0.30	2,328	7.03	0.02
Apr-14	0.25	0.32	0.32	0.78	0.64	1.32	3.48	5.60E-06	0.41	1,152	3.48	0.01
May-14	0.27	0.33	0.33	0.39	0.67	1.38	3.65	5.68E-06	0.21	1,269	3.83	0.01
Jun-14	0.18	0.23	0.23	0.56	0.46	0.95	2.51	3.99E-06	0.30	870	2.62	0.01
Jul-14	0.25	0.32	0.32	0.48	0.63	1.29	3.41	5.81E-06	0.29	1,169	3.53	0.01
Aug-14	0.21	0.27	0.27	0.85	0.52	1.08	2.84	5.66E-06	0.44	995	3.00	0.01
Sep-14	0.22	0.30	0.30	1.04	0.56	1.15	3.03	6.57E-06	0.55	1,074	3.24	0.01
Oct-14	0.26	0.34	0.34	0.88	0.66	1.36	3.59	6.99E-06	0.48	1,231	3.71	0.01
Nov-14	0.32	0.40	0.40	0.47	0.81	1.66	4.39	6.84E-06	0.25	1,484	4.48	0.01
Dec-14	0.21	0.27	0.27	0.60	0.53	1.09	2.89	4.90E-06	0.32	1,009	3.05	0.01
Maximum Three (3) Month Average Actual Emissions	0.52	0.72	0.72	1.73	1.31	2.70	7.14	1.78E-05	1.03	2,459	7.42	0.02
Three (3) Month Period	Jan-13 Mar-13	Jan-13 Mar-13	Jan-13 Mar-13	Jun-13 Aug-13	Jan-13 Mar-13	Jan-13 Mar-13	Jan-13 Mar-13	Jan-13 Mar-13	Sep-13 Nov-13	Jan-13 Mar-13	Jan-13 Mar-13	Jan-13 Mar-13

<sup>(</sup>a) The maximum three (3) month period of actual emissions are shown in bold for each pollutant.

<sup>(</sup>b) Emissions shown here were calculated using the reported emissions and their associated calculation methods by the Trainery Refinery.

### Table C-24 Monroe Energy, LLC - Trainer, PA Refinery Projected Actual Emissions from Storage Tanks

			Projected Actual VOC			
PADEP ID	Unit	Notes	Emissions (a)(b)			
			lb/hr	tpy		
		Projected actual emissions are developed by annualizing the				
165	Tank 93	average of the three (3) highest emitting months from 2013-	0.44	1.92		
		2014.				
		Projected actual emissions are developed by annualizing the	0.40			
166	Tank 94	average of the three (3) highest emitting months from 2013-	0.63	2.76		
		2014.				
126	Tank 95	Projected actual emissions are developed by annualizing the	0.79	3.46		
120	Talik 93	average of the three (3) highest emitting months from 2013- 2014.	0.79	3.40		
	+	Projected actual emissions are developed by annualizing the				
127	Tank 96	average of the three (3) highest emitting months from 2013-	1.02	4.45		
		2014.	1.02			
		Projected actual emissions are developed by annualizing the				
137	Tank 152	average of the three (3) highest emitting months from 2013-	1.15	5.06		
		2014.				
		Projected actual emissions are developed by annualizing the				
138	Tank 153	average of the three (3) highest emitting months from 2013-	0.04	0.19		
		2014.				
		Projected actual emissions are developed by annualizing the				
140	Tank 155	average of the three (3) highest emitting months from 2013-	0.04	0.18		
		2014.				
1.40	m 1 157	Projected actual emissions are developed by annualizing the		0.21		
142	Tank 157	average of the three (3) highest emitting months from 2013-	0.05	0.21		
	+	2014.		ļ		
200	Toul. 150 (C ID 100)	Projected actual emissions are developed by annualizing the	2.00	12.15		
300	Tank 158 (Source ID 193)	average of the three (3) highest emitting months from 2013-	3.00	13.15		
		2014.  Projected actual emissions are developed by annualizing the				
143	Tank 159		0.91	3.97		
143	Talik 139	average of the three (3) highest emitting months from 2013- 2014.	0.51	3.91		
	+	Projected actual emissions are developed by annualizing the				
194	Tank 160	average of the three (3) highest emitting months from 2013-	0.05	0.22		
.,.	Tunk 100	2014	0.03	0.22		
		Projected actual emissions are developed by annualizing the				
144	Tank 161	average of the three (3) highest emitting months from 2013-	1.38	6.04		
		2014.				
		Projected actual emissions are developed by annualizing the				
145	Tank 162	average of the three (3) highest emitting months from 2013-	0.74	3.25		
		2014.				
		Projected actual emissions are developed by annualizing the				
146	Tank 163	average of the three (3) highest emitting months from 2013-	0.97	4.25		
		2014.				
		Projected actual emissions are developed by annualizing the				
147	Tank 164	average of the three (3) highest emitting months from 2013-	0.87	3.79		
		2014.				
140	m 1 165	Projected actual emissions are developed by annualizing the		0.25		
148	Tank 165	average of the three (3) highest emitting months from 2013-	1.89	8.26		
		2014.				
140	Tank 166	Projected actual emissions are developed by annualizing the	0.01	2.55		
149	1 ank 100	average of the three (3) highest emitting months from 2013-	0.81	3.55		
	1	2014.  Projected actual emissions are developed by annualizing the		1		
150	Tank 168		0.66	2.89		
100	1K 100	average of the three (3) highest emitting months from 2013-	0.00	2.07		
	1	Projected actual emissions are developed by annualizing the				
152	Tank 170	average of the three (3) highest emitting months from 2013-	1.40	6.13		
- <del>-</del>		2014.				
		Projected actual emissions are developed by annualizing the				
155	Tank 174	average of the three (3) highest emitting months from 2013-	2.74	12.01		
		2014.				
		Projected actual emissions are developed by annualizing the				
156	Tank 175	average of the three (3) highest emitting months from 2013-	1.70	7.43		
		2014.				
		Projected actual emissions are developed by annualizing the				
157	Tank 178	average of the three (3) highest emitting months from 2013-	0.74	3.23		
		2014.				
	m	Projected actual emissions are developed by annualizing the				
160	Tank 181	average of the three (3) highest emitting months from 2013-	2.00	8.75		
	+	2014.				
1.51	m 1 102	Projected actual emissions are developed by annualizing the		20.77		
161	Tank 182	average of the three (3) highest emitting months from 2013-	4.69	20.53		
	+	2014.		<del>                                     </del>		
162	Towl- 105	Projected actual emissions are developed by annualizing the	2.57	11.25		
163	Tank 185	average of the three (3) highest emitting months from 2013-	2.57 11.26			
	+	2014. Projected actual emissions are developed by appualizing the		1		
	1	Projected actual emissions are developed by annualizing the				
164	Tank 186	average of the three (3) highest emitting months from 2013-	1.25	5.47		

(a) Projected future actual emissions are based upon the following parameters:

	81										
Parameter	Value	Units/Notes									
Operating Hours	8,760	hr/yr									
Conversion Factor 1	2,000	lb/ton									

<sup>(</sup>b) Monthly emissions were calculated using the methodology laid out in U.S. EPA's Compilation of Air Pollutant Emission Factors - AP-42, Chapter 7.

Table C-25 Monroe Energy, LLC - Trainer, PA Refinery Historical 2013-2014 Monthly Actual VOC Emissions from Storage Tanks

									Tank 158																	
(2)	Tank 93	Tank 94	Tank 95	Tank 96	Tank 152	Tank 153	Tank 155	Tank 157	(Source	Tank 159	Tank 160	Tank 161	Tank 162	Tank 163	Tank 164	Tank 165	Tank 166	Tank 168	Tank 170	Tank 174	Tank 175	Tank 178	Tank 181	Tank 182	Tank 185	Tank 186
Date <sup>(a)</sup>									ID 193)																	
		(tons) <sup>(b)</sup>																								
Jan-13	0.12	0.18	0.20	0.33	0.19	0.01	0.00	0.01	0.06	0.31	0.02	0.46	0.11	0.13	0.15	0.14	0.13	0.28	0.47	0.44	0.67	0.10	0.13	0.40	0.64	0.37
Feb-13	0.12	0.14	0.21	0.36	0.72	0.02	0.01	0.01	0.04	0.32	0.01	0.49	0.09	0.09	0.09	0.07	0.11	0.28	0.50	0.47	0.39	0.06	0.13	0.27	0.39	0.18
Mar-13	0.14	0.24	0.26	0.38	0.35	0.01	0.01	0.01	0.06	0.34	0.02	0.52	0.11	0.11	0.17	0.14	0.09	0.16	0.52	0.54	0.50	0.11	0.09	0.49	0.76	0.46
Apr-13	0.14	0.21	0.29	0.36	0.02	0.01	0.00	0.01	0.10	0.33	0.01	0.50	0.11	0.16	0.11	0.20	0.12	0.14	0.52	0.42	0.43	0.13	0.13	0.22	0.40	0.21
May-13	0.16	0.23	0.28	0.31	0.01	0.01	0.01	0.01	0.21	0.30	0.02	0.44	0.09	0.18	0.14	0.00	0.10	0.18	0.45	0.42	0.63	0.10	0.11	0.32	0.39	0.37
Jun-13	0.13	0.22	0.29	0.28	0.02	0.01	0.00	0.02	0.17	0.29	0.02	0.41	0.11	0.19	0.13	0.60	0.13	0.28	0.43	0.32	0.58	0.09	0.54	0.33	0.37	0.21
Jul-13	0.15	0.21	0.30	0.26	0.01	0.01	0.01	0.00	0.21	0.28	0.02	0.38	0.08	0.20	0.14	0.13	0.12	0.01	0.41	0.35	0.33	0.09	0.00	0.32	0.33	0.21
Aug-13	0.13	0.22	0.27	0.25	0.01	0.01	0.01	0.00	0.14	0.27	0.02	0.37	0.09	0.13	0.12	0.13	0.10	0.02	0.40	0.39	0.32	0.10	0.00	0.43	0.34	0.23
Sep-13	0.12	0.20	0.27	0.26	0.01	0.01	0.01	0.01	0.10	0.27	0.02	0.38	0.09	0.20	0.13	0.15	0.18	0.01	0.39	0.22	0.38	0.10	0.00	0.40	0.27	0.18
Oct-13	0.14	0.20	0.25	0.28	0.01	0.01	0.00	0.01	0.10	0.28	0.01	0.40	0.08	0.11	0.11	0.12	0.12	0.01	0.44	0.33	0.54	0.29	0.98	0.29	0.34	0.19
Nov-13	0.14	0.18	0.23	0.31	0.01	0.01	0.00	0.01	0.05	0.29	0.01	0.43	0.07	0.10	0.08	0.09	0.08	0.00	0.46	0.30	0.39	0.07	0.25	0.91	0.39	0.20
Dec-13	0.12	0.24	0.20	0.32	0.01	0.00	0.01	0.02	0.01	0.30	0.01	0.45	0.08	0.10	0.10	0.10	0.06	0.02	0.46	0.18	0.38	0.27	0.10	0.26	0.29	0.27
Jan-14	0.13	0.14	0.20	0.33	0.01	0.00	0.00	0.01	0.76	0.30	0.01	0.46	0.09	0.05	0.07	0.07	0.05	0.01	0.18	0.19	0.13	0.05	0.06	0.54	0.29	0.21
Feb-14	0.14	0.16	0.20	0.36	0.01	0.01	0.00	0.01	0.77	0.33	0.01	0.49	0.53	0.08	0.65	1.69	0.11	0.01	0.16	1.05	0.66	0.49	1.85	3.29	0.32	0.23
Mar-14	0.13	0.19	0.24	0.38	0.02	0.01	0.01	0.02	0.80	0.34	0.01	0.52	0.14	0.10	0.20	0.26	0.08	0.01	0.19	0.65	0.22	0.06	0.10	0.76	0.77	0.26
Apr-14	0.16	0.21	0.29	0.37	0.01	0.01	0.02	0.02	0.81	0.33	0.02	0.50	0.15	0.11	0.10	0.11	0.09	0.02	0.27	0.34	0.25	0.13	0.23	1.09	0.43	0.25
May-14	0.15	0.16	0.28	0.31	0.02	0.02	0.01	0.02	1.43	0.30	0.02	0.41	0.15	0.10	0.12	0.13	0.12	0.01	0.45	0.30	0.28	0.17	0.23	1.00	0.40	0.21
Jun-14	0.17	0.18	0.30	0.28	0.02	0.01	0.01	0.01	1.04	0.29	0.02	0.42	0.03	0.15	0.17	0.37	0.24	0.02	0.46	0.76	0.66	0.16	0.25	1.13	0.98	0.21
Jul-14	0.14	0.13	0.28	0.26	0.02	0.01	0.00	0.01	0.82	0.27	0.02	0.44	0.12	0.37	0.18	0.34	0.24	0.01	0.51	1.15	0.63	0.25	0.27	1.11	0.90	0.37
Aug-14	0.11	0.17	0.27	0.25	0.01	0.01	0.01	0.02	0.81	0.27	0.01	0.42	0.18	0.35	0.16	0.30	0.34	0.02	0.36	1.10	0.56	0.20	0.25	1.12	0.93	0.34
Sep-14	0.11	0.14	0.26	0.26	0.02	0.01	0.02	0.02	0.80	0.27	0.02	0.40	0.18	0.34	0.22	0.27	0.31	0.02	0.42	0.31	0.52	0.20	0.22	0.95	0.86	0.55
Oct-14	0.09	0.13	0.25	0.27	0.02	0.01	0.01	0.02	0.79	0.28	0.02	0.35	0.15	0.13	0.19	0.27	0.20	0.01	0.27	0.86	0.49	0.10	0.20	0.92	0.81	0.38
Nov-14	0.10	0.14	0.23	0.30	0.02	0.02	0.01	0.02	0.77	0.29	0.02	0.27	0.15	0.21	0.29	0.27	0.17	0.02	0.32	0.49	0.41	0.10	0.12	0.59	0.61	0.44
Dec-14	0.08	0.10	0.18	0.32	0.02	0.02	0.01	0.01	0.01	0.30	0.02	0.22	0.13	0.23	0.22	0.29	0.16	0.01	0.33	0.50	0.40	0.10	0.13	0.59	0.59	0.44
Maximum Three (3) Month Average Actual Emissions	0.16	0.23	0.29	0.37	0.42	0.02	0.01	0.02	1.10	0.33	0.02	0.50	0.27	0.35	0.32	0.69	0.30	0.24	0.51	1.00	0.62	0.27	0.73	1.71	0.94	0.46
Three (3) Month Period	Apr-14	Mar-13	Apr-14	Feb-14	Jan-13	Oct-14	Aug-14	Mar-14	May-14	Feb-14	Oct-14	Feb-14	Feb-14	Jul-14	Feb-14	Feb-14	Jul-14	Jan-13	Feb-13	Jun-14	Jun-14	Dec-13	Feb-14	Feb-14	Jun-14	Sep-14
(,,	Jun-14	May-13	Jun-14	Apr-14	Mar-13	Dec-14	Oct-14	May-14	Jul-14	Apr-14	Dec-14	Apr-14	Apr-14	Sep-14	Apr-14	Apr-14	Sep-14	Mar-13	Apr-13	Aug-14	Aug-14	Feb-14	Apr-14	Apr-14	Aug-14	Nov-14

 $<sup>^{\</sup>mathrm{(a)}}$  The maximum three (3) month period of actual emissions are shown in bold for each tank.

<sup>(</sup>b) Emissions shown here were calculated using the reported emissions and their associated calculation methods by the Trainery Refinery.

## Table C-26 Monroe Energy, LLC - Trainer, PA Refinery Potential to Emit from the New Feed Heaters

Pollutant	Emission	Emission Factor	Notes	Projected Actual Emissions (a)			
	Factor	Units		lb/hr	tpy		
Filterable PM	5.00E-03	lb/MMBtu	Vendor gauranteed emissions.	0.72	3.15		
Total PM <sub>10</sub>	5.00E-03	lb/MMBtu	Vendor gauranteed emissions.	0.72	3.15		
Total PM <sub>2.5</sub>	5.00E-03	lb/MMBtu	Vendor gauranteed emissions.	0.72	3.15		
SO.	162	ppmdv	Emission factor based on the short-term allowable RFG $H_2S$ concentration found at 40 CFR §\$60.102a(g)(1)(ii). Assumed full conversion from $H_2S$ to $SO_2$ .	3.27	4.42		
302	SO <sub>2</sub> 50 ppmdv		Based upon TVOP No. 23-00003 limit for $H_2S$ from refinery fuel gas fired from the north side fuel supply. Assumed full conversion of $H_2S$ to $SO_2$ .	3.21	4.42		
$NO_X$	0.035	lb/MMBtu	Vendor gauranteed emissions.	5.03	22.04		
VOC	5.00E-03	lb/MMBtu	Vendor gauranteed emissions.	0.72	3.15		
CO <sup>(b)</sup>	400	ppmdv @ 3% O <sub>2</sub>	Vendor gauranteed emissions.	31.19	17.08		
Lead	5.00E-04	lb/MMSCF	AP-42 Table 1.4-2	6.08E-05	2.66E-04		
H <sub>2</sub> S	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.01	0.05		
TRS	8.50E-05	lb/MMBtu	U.S. EPA's memo titled "Emission Estimation Protocol for Petroleum Refineries" from May 2011, Table 4-3.	0.01	0.05		
$CO_2$	59.00	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-1	18,704	81,925		
N <sub>2</sub> O	6.00E-04	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	1.90E-01	0.83		
CH <sub>4</sub>	3.00E-03	kg/MMBtu	40 CFR Part 98 Subpart C, Table C-2	9.51E-01	4.17		
Total GHG	N/A	N/A	Emissions are calculated as the sum of CO <sub>2</sub> , N <sub>2</sub> O, and CH <sub>4</sub> .	18,706	81,930		
CO <sub>2</sub> e <sup>(c)</sup>	N/A	N/A	Emissions are calculated according to 40 CFR Part 98 Equation A-1.	18,785	82,278		

 $<sup>^{(</sup>a)}$  The potential to emit is based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Total Heat Input (both heaters)	143.8	MMBtu/hr
Fuel Gas Heating Value	1,182	MMBtu/MMSCF
Conversion Factor 1	2,000	lb/ton
Molecular Weight CO	28.01	lb/lb-mol
Molecular Weight SO <sub>2</sub>	64.00	lb/lb-mol
Natural Gas F-factor	8,710	dscf/MMBtu
Conversion Factor 2	60	min/hour
Conversion Factor 3	1,000,000	Btu/MMBtu
Standard Oxygen	20.9	%
Gas at Standard Conditions	385.35	scf/lb-mol
Conversion Factor 4	2.20	lb/kg

<sup>(</sup>b) Potential annual CO emissions have been calculated to be reflective of future CO emissions anticipated during future normal operations (i.e., an annual average CO concentration of 50 ppmdv @ 3% O<sub>2</sub>).

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where GHGi = annual mass emissions of greenhouse gas i (short tons/year)

 $GWPi = global \ warming \ potential \ of \ greenhouse \ gas \ i \ from \ the \ table \ below$ 

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

 $<sup>^{(</sup>c)}\text{CO}_2\text{e}$  is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

### Table C-27 Monroe Energy, LLC - Trainer, PA Refinery

### Cooling Tower Calculated Potential to Emit PM/PM<sub>10</sub>/PM<sub>2.5</sub> Emission Rates

Pollutant	Air Flow Rate (design) <sup>(b)</sup>	Cooling Water Recirculation Flow Rate	Circulating Water TDS <sup>(c)</sup>	Drift Rate <sup>(d)</sup> (design)	Cooling Water Tower Particulate Emission (drift) Rate	Cooling Water Tower Particulate Emission (drift) Rate	Cooling Water Tower Particulate Emission (drift) Rate	Particulate from Propos Towe	ed Cooling
	(scfm)	(gpm)	(ppmw)	(%)	(lb/hr)	(tons/yr)	(gr/dscf)	lb/hr	(tpy) <sup>(f)</sup>
PM/PM <sub>10</sub> /PM <sub>2.5</sub>	1,568,000	10,200	1,400	0.0005%	0.04	0.16	2.66E-06	0.04	0.16

<sup>(</sup>a) PM is conservatively assumed to be equal to PM2.5 and PM10.

 $<sup>^{\</sup>left( g\right) }$  The potential to emit is based upon the following parameters:

Parameter	Value	Units/Notes
Operating Hours	8,760	hr/yr
Conversion Factor 1	2,000	lb/ton
Conversion Factor 2	1,000	lb/M lb
Conversion Factor 3	1.10E-03	tons/kg
Conversion Factor 4	453.59	g/lb
Conversion Factor 5	3.78	L/gal
Conversion Factor 6	2.21E-06	lb/mg
Conversion Factor 7	60.00	min/hr
Conversion Factor 8	7,000	gr/lb

<sup>(</sup>b) Air flow rate is based on vendor provided specifications.

 $<sup>^{(</sup>c)}$ TDS of city water ranges from 175-280 ppmw. Monroe has assumed five (5) cycles of maximum concentration (280 ppmw  $\times$  5 cycles = 1,400 ppmw).

<sup>(</sup>d) Drift rate is BAT.

<sup>(</sup>e) Emission estimation method from U.S. EPA AP-42 Chapter 13.4.

<sup>&</sup>lt;sup>(f)</sup> Annual emissions for the proposed cooling towers are based on 8,760 hours per year of operation.

### Table C-28 Monroe Energy, LLC - Trainer, PA Refinery Cooling Tower Calculated Potential to Emit VOC Emission Rates

Concentration of Total Hydrocarbons (THCs) in Stripped Air <sup>(a)</sup>	Pressure	Temperature Compound (b)		Mass Flow Rate of the Cooling Water	Potenti Emissio Proposed Towe	ns from I Cooling
(ppmw)	(Hg)	(°C)	(ppmw)	(gal/min)	(lb/hr)	(tpy)
21.00	29.92	32	0.27	10,200	1.37	6.02

<sup>(</sup>a) Concentration of total hydrocarbons (THCs) is one-third the maximum VOC concentration of stripped air allowed before a leaking heat exchanger must be repaired under the heater exchanger system provisions found at 40 CFR §63.654.

 $C = (M*(P*0.03342 \ atm/(in \ Hg))*b*c)/(R*(T+273)*a)$ 

where:

C = Concentration of air strippable compound in water matrix (ppmw)

M = Molecular weight of the compound (g/mol)

P = Pressure in the stripping chamber (in Hg); equivalent to standard atmospheric pressure

b = Stripping air flow rate (ml/min)

 $c = \ Concentration \ of \ compound \ in \ the \ stripped \ air \ (ppmv)$ 

R = 82.054 ml-atm/mol-K

T = Stripping chamber temperature (Celsius)

a = Sample water flow rate (ml/min)

The constants used in Equation 7-1 are as follows:

Parameter from Equation 7-1	Value	Unit
M	16.04	g/mol
b	2500	ml/min
R	82.054	ml-atm/mol-K
a	125	ml/min

<sup>(</sup>c) Concentration of air strippable compound was calculated based on Equation 7-2 from Texas Commission Environmental Quality guidance titled: "Air Stripping Method (Modified El Paso Method) for Determination of Volatile Organic Compound Emissions from Water Sources, Sampling Procedures Manual, Appendix P: Cooling Tower Monitoring Guidance."

$$E=C*F*60 \ min/hr*8.337 \ lb/gal* \ 1/([[10]]^6 \ p \ pm)$$

where:

E = Mass emission rate of VOCs (lb/hr)

 $C = \ Concentration \ of \ air \ strippable \ compound \ in \ the \ water \ matrix \ (ppmw)$ 

F = Water circulation rate of source (gallons/min)

The constants used in Equation 7-2 are as follows:

Parameter	Value	Unit
Operating Hours	8,760	hr/yr
Conversion Factor 1	60	min/hr
Conversion Factor 2	8.34	lb water/gal water
Conversion Factor 3	1,000,000	ppm
Conversion Factor 4	2,000	lb/ton

<sup>(</sup>b) Concentration of air strippable compound was calculated based on Equation 7-1 from Texas Commission Environmental Quality guidance titled: "Air Stripping Method (Modified El Paso Method) for Determination of Volatile Organic Compound Emissions from Water Sources, Sampling Procedures Manual, Appendix P: Cooling Tower Monitoring Guidance."

Table C-29

Monroe Energy, LLC - Trainer, PA Refinery

New Fugitive Components

Fugitive E	Fugitive Equipment Component Counts (total for each)											
Component	Total	Light Liquid	Heavy Liquid	Gas Service								
Valves	1,773	656	60	1,057								
Control Valves	33	33	0	0								
Check Valves	42	42	0	0								
Pressure Relief Valves	28	28	0	0								
Strainers	6	6	0	0								
Flanges	976	282	30	664								
Compressors	1	0	0	1								
Pumps	8	8	0	0								
Connections	62	62	0	0								

Note: Component counts estimated from P&ID drawings.

Table C-30

Monroe Energy, LLC - Trainer, PA Facility

New Fugitive Potential to Emit Rates

			VOC Leal	k Rate <sup>(a)</sup>		
Component	Default 0 ppm	0-500 ppm	500 -10,000 ppm	>10,000 ppm	Total VOC	Total VOC (trus)
	(lbs/year)	(lbs/year)	(lbs/year)	(lbs/year)	(lbs/hr) <sup>(b)</sup>	Total VOC (tpy)
Valves	240.37	646.99	1,398.14	3,287.11	0.64	2.79
Control Valves	4.47	12.04	26.02	61.18	0.01	0.05
Check Valves	5.69	15.33	33.12	77.87	0.02	0.07
Pressure Relief Valves	3.80	10.22	22.08	51.91	0.01	0.04
Strainers	0.42	4.90	6.62	12.69	0.00	0.01
Flanges	5.26	548.85	1,042.69	2,403.22	0.46	2.00
Compressors	0.07	0.82	1.10	2.11	0.00	0.00
Pumps	3.34	27.54	39.60	17.15	0.01	0.04
Connections	4.31	50.65	68.38	131.11	0.03	0.13
Total	267.73	1,317.33	2,637.75	6,044.35	1.17	5.13

 $<sup>^{\</sup>rm (a)}$  Source: "Protocol for Equipment Leak Emission Estimates", EPA-453/R-95-017

<sup>(</sup>b) Short-term emissions rates are determined assuming 8,760 hours of operation per year.

#### Table C-31 Monroe Energy, LLC - Trainer, PA Facility Projected Future Actual Emissions

101	Emission Unit						nission Rate					
101		PM	PM <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NOx	voc	СО	Lead	H <sub>2</sub> S	TRS	CO <sub>2</sub> e <sup>(a)</sup>
	FCC Unit	84.62	110.60	96.21	88.82	432.52	3.20	16.35	-	-	-	756,643.87
733	FCCU Feed Heater	0.18	0.72	0.72	0.78	3.02	0.52	7.93	4.72E-05	8.56E-03	8.56E-03	13,159.88
735	Kerosene/HCN HTU Feed Heater	0.06	0.25	0.25	0.28	4.51	0.18	2.81	1.67E-05	3.09E-03	3.09E-03	4,749.00
736	Diesel HTU Heater	0.11	0.62	0.62	0.67	13.84	0.39	0.18	4.05E-05	7.45E-03	7.45E-03	11,443.37
741	D2/VGO Hydrotreater Feed Heater	0.15	0.59	0.59	0.61	7.71	0.42	6.48	3.86E-05	6.70E-03	6.70E-03	10,299.04
737	Naphtha HDS Heater	0.61	2.43	2.43	2,55	33.29	1.76	26.88	1.60E-04	0.03	0.03	43,484.82
738	Platformer Feed Heater	4.06	16.23	16.23	17.03	185.70	11.75	0.15	1.07E-03	0.18	0.18	282,079,15
739	Isocracker 1st Stage Heater	0.26	1.03	1.03	1.08	16.77	0.75	11.43	6.80E-05	0.01	0.01	18,881.57
740	Isocracker Splitter Reboiler	0.34	1.37	1.37	1.44	18.05	0.99	15.17	9.03E-05	0.02	0.02	25,175.42
742	VCD 541 VAC Heater	0.27	1.06	1.06	1.16	20.50	0.77	11.76	7.00E-05	0.02	0.02	20,598.07
743	VCD 541 VAC Heater	0.15	0.62	0.62	0.67	6.75	0.03	0.02	4.06E-05	7.45E-03	7.45E-03	11.443.37
746	VCD 542 VAC Heater	0.55	2.19	2.19	2.39	12.44	2.18	5.29	1.44E-04	0.03	0.03	40,623,97
744	ACD 543 Crude Heater	2.01	8.02	8.02	8.77	45.55	5.81	88.66	5.28E-04	0.10	0.03	148,763,85
745	ACD 545 Crude Heater ACD 544 Crude Heater	2.00	8.01	8.01	8.75	50.11	5.80	88.55	5.27E-04	0.10	0.10	148,763.85
34			5.69	5.07	1.04	4.41	0.31	1.34	5.27E-04 4.80E-04	0.10	0.10	115,912.86
	Boiler 9	0.72										
35	Boiler 10	0.40	3.07	2.97	2.97	3.93	0.27	4.93	4.60E-04	0.08	0.08	110,997.52
102	SRU	0.11	0.44	0.44	40.33	5.83	0.32	4.90	2.92E-05	0.00	-	31,828.54
103	Main Flare	1.25	1.74	1.74	4.15	3.15	6.48	17.13	2.14E-04	2.47	-	6,365.71
165	Tank 93	-	-	-	-	-	1.92	-	-	-	-	-
166	Tank 94	-	-	-	-	-	2.76	-	-	-	-	-
126	Tank 95	-	-	-	-	=	3.46	-	-	-	-	-
127	Tank 96	-	-	-	-	-	4.45	-	-	-	-	-
137	Tank 152	-	-	-	-	-	5.06	-	-	-	-	-
138	Tank 153	-	-	-	-	-	0.19	-	-	-	-	-
140	Tank 155	-	-	-	-	-	0.18	-	-	-	-	-
142	Tank 157	-	-	-	-	-	0.21	-	-	-	-	-
300	Tank 158 (Source ID 193)	-	-	-	-	-	13.15	-	-	-	-	-
143	Tank 159	-	-	-	-	-	3.97	-	-	-	-	-
194	Tank 160	-	-	-	-	-	0.22	-	-	-	-	-
144	Tank 161	-	-	-	=	=	6.04	-	-	-	-	-
145	Tank 162	-	-	-	-	-	3.25	-	-	-	-	-
146	Tank 163	-	-	-	-	-	4.25	-	-	-	-	-
147	Tank 164	-	-	-	-	-	3.79	-	-	-	-	-
148	Tank 165	-	-	-	-	-	8.26	-	-	-	-	-
149	Tank 166	-	-	-	-	-	3.55	-	-	-	-	-
150	Tank 168	-	-	-	-	-	2.89	-	-	-	-	-
152	Tank 170	-	-	-	-	-	6.13	-	-	-	-	-
155	Tank 174	-	-	-	-	-	12.01	-	-	-	-	-
156	Tank 175	-	-	-	-	-	7.43	-	-	-	-	-
157	Tank 178	-	-	-	-	-	3.23	-	-	-	-	-
160	Tank 181	-	-	-	-	-	8.75	-	-	-	-	-
161	Tank 182	-	-	-	-	=.	20.53	-	-	-	-	-
163	Tank 185	-	-	-	-	=.	11.26	-	-	-	-	-
164	Tank 186	-	-	-	-	-	5.47	-	-	-	-	-
N/A	New Feed Heaters	3.15	3.15	3.15	4.42	22.04	3.15	17.08	2.66E-04	-	_	-
N/A	New Cooling Tower	0.16	0.16	0.16	-	-	6.02	-	-	-	_	_
N/A	Additional Fugitive Emissions	-	-	-	_	-	5.13	-	-	-	-	<u> </u>
	jected Future Actual Emissions	16.53	57.40	56.68	99.11	457.60	195.44	310.66	4.29E-03	3.15	0.68	1,044,569.99

 $<sup>^{(</sup>a)}$  CO $_2$ e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

where GHGi = annual mass emissions of greenhouse gas i (short tons/year) GWPi = global warming potential of greenhouse gas i from the table below

Pollutant	GWP (100 year)
$CO_2$	1
N <sub>2</sub> O	298
CH <sub>4</sub>	25

### Table C-32 Monroe Energy, LLC - Trainer, PA Refinery Emissions Which Could Have Been Accomodated (CHA)

	Emission Unit	·			_				sion Rate (t						
			PM	PM <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>X</sub>	voc	СО	Lead	H <sub>2</sub> S	TRS	CO2	N <sub>2</sub> O	CH <sub>4</sub>
101	ECC II-it	Highest Emitting Month	Mar-15	Mar-15	Mar-15	Jun-15	Dec-14	Mar-13	May-13	Jan-14			Jul-10	Jul-10	Jul-10
101	FCC Unit	Monthly Emissions Annualized Emissions (CHA)	9.79	11.73 140.78	10.07 120.81	8.06 96.67	37.87 454.41	0.27 3.26	2.95 35.45	3.48E-05 4.18E-04	0.00	0.00	46,689.55 560,274.64	0.27 3.28	1.37
		Highest Emitting Month	Jun-14	Jun-14	Jun-14	Jun-14	Jun-14	Jun-14	Mar-13	Jun-14	Jul-09	Jul-09	Jul-09	Jul-09	Jul-09
733	FCCU Feed Heater	Monthly Emissions	0.03	0.13	0.13	0.14	0.54	0.09	0.94	8.32E-06	1.85E-03	1.85E-03	2,833.44	0.03	0.14
		Annualized Emissions (CHA) Highest Emitting Month	0.38 Dec-14	1.52 Jul-15	1.52 Jul-15	1.66 Jul-15	6.44 May-15	1.10 Jul-15	11.29 Dec-14	9.99E-05 Aug-14	0.02 Jan-09	0.02 Jan-11	34,001.33 Jan-11	0.35 Jan-11	1.73 Jan-11
735	Kerosene/HCN HTU Feed	Monthly Emissions	0.04	0.04	0.04	0.05	0.77	0.03	0.44	2.38E-06	3.12E-04	3.63E-04	555.94	5.65E-03	0.03
	Heater	Annualized Emissions (CHA)	0.47	0.50	0.50	0.55	9.20	0.36	5.23	2.85E-05	3.74E-03	4.36E-03	6,671.34	0.07	0.34
736	Diesel HTU Heater	Highest Emitting Month Monthly Emissions	Apr-14 0.05	Jul-15 0.06	Jul-15 0.06	Jul-15 0.07	Jul-15 1.37	Oct-13 0.03	Jan-13 0.91	Jan-13 5.39E-06	Mar-10 1.00E-03	Mar-10 1.00E-03	Mar-10 1,529.58	Mar-10 0.02	Mar-10 0.08
750	Diesei III o Heater	Annualized Emissions (CHA)	0.63	0.68	0.68	0.07	16.45	0.03	10.87	6.47E-05	0.01	0.01	18,354.99	0.02	0.08
	D2/VGO Hydrotreater Feed	Highest Emitting Month	Jul-14	Jun-15	Jun-15	Jun-15	Jun-15	Jun-15	May-13	May-13	Jan-09	Mar-11	May-11	May-11	May-11
741	Heater	Monthly Emissions Annualized Emissions (CHA)	0.07	0.10 1.14	0.10 1.14	0.10 1.20	1.26 15.06	0.07 0.83	1.28 15.41	7.64E-06 9.17E-05	1.46E-03 0.02	1.85E-03 0.02	2,879.96 34,559.53	0.03	0.15 1.76
		Highest Emitting Month	Oct-14	Oct-14	Oct-14	Oct-14	Oct-14	Oct-14	Oct-14	Oct-14	Oct-10	Oct-10	Oct-10	Oct-10	Oct-10
737	Naphtha HDS Heater	Monthly Emissions	0.20	0.20	0.20	0.21	3.09	0.14	2.19	1.30E-05	2.43E-03	2.43E-03	3,714.73	0.04	0.19
		Annualized Emissions (CHA) Highest Emitting Month	2.37 Mar-14	2.37 Jul-15	2.37 Jul-15	2.49 Jul-15	37.04 Jul-15	1.72 Jul-15	26.25 Mar-13	1.56E-04 Mar-13	0.03 Mar-10	0.03 Mar-10	44,576.75 Mar-10	0.45 Mar-10	2.27 Mar-10
738	Platformer Feed Heater	Monthly Emissions	1.26	1.29	1.29	1.35	14.51	0.93	0.59	9.20E-05	0.02	0.02	26,617.95	0.27	1.35
		Annualized Emissions (CHA)	15.12	15.46	15.46	16.21	174.17	11.19	7.11	1.10E-03	0.21	0.21	319,415.38	3.25	16.24
739	Isocracker 1st Stage Heater	Highest Emitting Month Monthly Emissions	Dec-14 0.09	Aug-13 0.12	Aug-13 0.12	Aug-13 0.12	Jan-15 1.81	Aug-13 0.08	May-13 1.37	May-13 8.13E-06	Jan-10 1.27E-03	Jan-10 1.27E-03	Jan-10 1,937,43	Jan-10 0.02	Jan-10 0.10
137	Isocracker 1st Stage Teater	Annualized Emissions (CHA)	1.07	1.39	1.39	1.46	21.75	1.01	16.45	9.76E-05	0.02	0.02	23,249.17	0.02	1.18
		Highest Emitting Month	May-14	May-14	May-14	May-14	May-14	May-14	Jul-13	Jul-13	May-10	Mar-11	Mar-11	Mar-11	Mar-11
740	Isocracker Splitter Reboiler	Monthly Emissions	0.13	0.13	0.13	0.13	1.65	0.09	1.46	8.72E-06	1.26E-03	1.30E-03	1,986.38	0.02	0.10
		Annualized Emissions (CHA) Highest Emitting Month	1.50 Jul-15	1.50 Jul-15	1.50 Jul-15	1.58 Jul-15	19.76 Apr-15	1.09 Jul-15	17.58 Aug-14	1.05E-04 Aug-14	0.02 Jan-09	0.02 Apr-10	23,836.53 Apr-10	0.24 Apr-10	1.21 Apr-10
742	VCD 541 VAC Heater	Monthly Emissions	0.02	0.10	0.10	0.11	1.82	0.07	0.95	5.63E-06	1.03E-03	9.72E-04	1,487.03	0.02	0.08
		Annualized Emissions (CHA)	0.29	1.17	1.17	1.28	21.87	0.85	11.34	6.75E-05	0.01	0.01	17,844.39	0.18	0.91
743	VCD 542 VAC Heater	Highest Emitting Month Monthly Emissions	Apr-14 0.11	Apr-14 0.11	Apr-14 0.11	Apr-14 0.06	Apr-14 0.63	Apr-14 2.57E-03	Apr-14 1.95E-03	Apr-14 3.83E-06	Jan-09 1.20E-03	Jul-10 1.12E-03	Jul-10 1,719.25	Jul-10 0.02	Jul-10 0.09
, , , ,	100 312 1110 1111111	Annualized Emissions (CHA)	1.32	1.32	1.32	0.76	7.52	0.03	0.02	4.60E-05	0.01	0.01	20,631.05	0.02	1.05
		Highest Emitting Month	Mar-14	Aug-13	Aug-13	Aug-13	Aug-13	Aug-13	Jan-13	Aug-13	Jan-10	Jan-10	Jan-10	Jan-10	Jan-10
746	VCD 544 VAC Heater	Monthly Emissions Annualized Emissions (CHA)	0.27 3.20	0.28 3.36	0.28 3.36	0.24 2.88	1.22	0.21 2.56	0.45 5.41	1.45E-05 1.74E-04	2.50E-03 0.03	2.50E-03 0.03	3,819.02 45,828.20	0.04	0.19 2.33
		Highest Emitting Month	3.20 Apr-14	3.30 Sep-13	5.36 Sep-13	2.88 Sep-13	Oct-13	2.56 Sep-13	5.41 Sep-13	Sep-13	0.03 Mar-10	0.03 Mar-10	45,828.20 May-11	0.47 May-11	2.33 May-11
744	ACD 543 Crude Heater	Monthly Emissions	0.72	0.73	0.73	0.80	4.14	0.53	8.07	4.80E-05	8.80E-03	8.80E-03	13,850.21	0.14	0.70
		Annualized Emissions (CHA)	8.66	8.76	8.76	9.57	49.71	6.34	96.84	5.76E-04	0.11	0.11	166,202.49	1.69	8.45
745	ACD 544 Crude Heater	Highest Emitting Month Monthly Emissions	Jan-14 0.77	Jan-14 0.77	Jan-14 0.77	Jan-14 0.84	Jan-14 4.68	Jan-14 0.56	Jan-14 8.50	Jan-14 5.06E-05	Mar-10 8.58E-03	Mar-10 8.58E-03	Mar-10 13,123.53	Mar-10 0.13	Mar-10 0.67
, ,,,	Tieb 511 crude ficates	Annualized Emissions (CHA)	9.23	9.23	9.23	10.08	56.20	6.68	102.01	6.07E-04	0.10	0.10	157,482.30	1.60	8.01
		Highest Emitting Month	Jan-15	Jan-15	Jan-15	Jun-15	Dec-13	Jan-15	Jan-14	Mar-13	-		Aug-10	Aug-10	Aug-10
34	Boiler 9	Monthly Emissions	0.07	0.47 5.62	0.44 5.29	0.27 3.24	0.41 4.91	0.03	0.12	4.66E-05 5.60E-04	7.19E-03 0.09	7.19E-03 0.09	9,097.35 109,168.22	0.02	2.06
		Annualized Emissions (CHA) Highest Emitting Month	Dec-13	3.62 Jan-15	3.29 Jan-15	3.24 Jul-15	4.91 Dec-13	Jan-15	1.41 Dec-13	5.60E-04 Dec-13	0.09	0.09	Aug-10	0.21 Aug-10	2.06 Aug-10
35	Boiler 10	Monthly Emissions	0.05	0.26	0.26	0.28	0.42	0.03	1.39	4.54E-05	7.48E-03	7.48E-03	9,469.05	0.02	0.18
		Annualized Emissions (CHA)	0.58	3.14	3.07	3.35	5.09	0.31	16.67	5.45E-04	0.09	0.09	113,628.58	0.21	2.14
102	SRU	Highest Emitting Month Monthly Emissions	Mar-15 0.01	Mar-15 0.05	Mar-15 0.05	Nov-14 2.33	Mar-15 0.69	Jan-14 0.03	Jan-14 0.47	Jan-14 2.79E-06	0.00	0.00	May-11 295.23	May-11 6.09E-03	May-11 6.09E-04
		Annualized Emissions (CHA)	0.14	0.58	0.58	27.98	8.23	0.37	5.62	3.34E-05	0.00	0.00	3,542.78	0.07	7.31E-03
102	M. i. Fl.	Highest Emitting Month	Feb-15	Feb-15	Feb-15	Nov-13	Feb-15	Jun-15	Jan-13	Jan-13	Jan-10	-	Jan-10	Jan-10	Jan-10
103	Main Flare	Monthly Emissions Annualized Emissions (CHA)	0.57 6.83	0.68 8.11	0.68 8.11	2.26 25.00	1.43	10.89 130.71	13.23 158.82	3.41E-05 4.09E-04	1.52 18.26	0.00	6,024.93 72,299.13	0.11 1.30	1.14
		Highest Emitting Month	-	-	-	-	-	Jun-14	-	-	-	-	-	-	-
165	Tank 93	Monthly Emissions		-	-	-	-	0.17	-		-	-	-	-	-
		Annualized Emissions (CHA)				-	-	2.03	-		-		-	-	-
		Highest Emitting Month	-	-	-	-	-	Dec-13	-	-	-	-	-	-	-
166	Tank 94	Monthly Emissions	-	-		-	-	0.24	-		-	-			-
		Annualized Emissions (CHA)													
126	T1.05		-	-	-	-	-	2.87	-	-	-			-	-
126	Tank 95	Highest Emitting Month		-	-	-	-	Jun-14	-		-			- - -	-
		Monthly Emissions		- - -			-	Jun-14 0.30				- - -	- - - -	- - - -	•
		Monthly Emissions Annualized Emissions (CHA)			- - - -	- - -	- - -	Jun-14 0.30 3.54						- - - -	- - - -
127	Tank 96	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month		- - - -	- - - - -	- - - -		Jun-14 0.30 3.54 Mar-14	- - - -			- - - -		- - - - -	-
127	Tank 96	Monthly Emissions Annualized Emissions (CHA)		- - - - - -	- - - - - -	- - - - - -	- - -	Jun-14 0.30 3.54			- - - - -	- - - - - -	-	- - - - - -	- - - - - - -
127	Tank 96	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions		- - - - - - -	- - - - - - -			Jun-14 0.30 3.54 Mar-14 0.38				- - - - - - -	- - - - - - - -	-	
127	Tank 96 Tank 152	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)		- - - - - - - -	- - - - - - -	-		Jun-14 0.30 3.54 Mar-14 0.38 4.61	-		- - - - - - -	- - - - - - - - - -			
		Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15							
137	Tank 152	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15					-	-	
		Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15							
137	Tank 152	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02							
137	Tank 152  Tank 153	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emisting Month						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15							
137	Tank 152	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions (CHA) Highest Emitting Month Monthly Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02							- - - -
137	Tank 152  Tank 153	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.21 0.21							
137 138 140	Tank 152  Tank 153  Tank 155	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14							- - - -
137	Tank 152  Tank 153	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 Mar-14 0.02							- - - -
137 138 140	Tank 152  Tank 153  Tank 155	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.22 0.22							- - - -
137 138 140	Tank 152  Tank 153  Tank 155	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 Mar-14 0.02							
137 138 140	Tank 152  Tank 153  Tank 155  Tank 157	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.24 Jun-15							
137 138 140 142 300	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.22 Jun-15 0.02							
137 138 140	Tank 152  Tank 153  Tank 155  Tank 157	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Jun-14 0.02 0.22 Jun-15 0.02 0.23 Mar-14 0.02 0.24 Jun-15 0.02							
137 138 140 142 300	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.23 Mar-14 0.04 0.05 0.05 0.05 0.05 0.05 0.07 0.07 0.08 0.08 0.09 0.09 0.09 0.09 0.09 0.09							
137 138 140 142 300	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-14 0.38 4.01 Jun-15 0.02 0.21 Mar-14 0.34 4.06 Jan-15							
137 138 140 142 300	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.24 Jun-15 2.33 28.01 Mar-14 0.34 4.06							
137 138 140 142 300	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA)						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.24 Jun-15 2.33 28.01 Mar-14 0.34 4.06 Jan-15 0.02 0.24 0.24 0.25 0.26							
137 138 140 142 300 143	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159  Tank 160	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emisting Month						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.38 2.8.01 Mar-14 0.34 4.60 Jan-15 0.02 0.26 Mar-14							
137 138 140 142 300	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-14 0.02 0.22 Mar-14 0.02 0.24 Jun-15 2.33 28.01 Mar-14 0.34 4.06 Jan-15 0.02 0.20 Mar-14 0.34 4.06 Mar-14 0.34 4.06 Jan-15 0.02 0.26 Mar-14 0.34 4.06 Mar-14 0.35							
137 138 140 142 300 143	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159  Tank 160	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.24 Jun-15 2.33 28.01 Mar-14 0.34 4.06 Jan-15 0.02 0.26 Mar-14 0.05 0.02 0.26 Mar-14 0.05							
137  138  140  142  300  143  194  144	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159  Tank 160  Tank 161	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-14 0.02 0.22 Mar-14 0.02 0.24 Jun-15 28.01 Mar-14 0.34 0.34 0.34 0.34 0.34 0.34 0.34 0.3							
137 138 140 142 300 143	Tank 152  Tank 153  Tank 155  Tank 157  Tank 158 (Source ID 193)  Tank 159  Tank 160	Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions Annualized Emissions (CHA) Highest Emitting Month Monthly Emissions						Jun-14 0.30 3.54 Mar-14 0.38 4.61 May-15 0.02 0.23 Apr-15 0.02 0.21 Mar-15 0.02 0.22 Mar-14 0.02 0.24 Jun-15 2.33 28.01 Mar-14 0.34 4.06 Jan-15 0.02 0.26 Mar-14 0.02 0.26 Mar-14 0.05 0.02							

### Table C-32 Monroe Energy, LLC - Trainer, PA Refinery Emissions Which Could Have Been Accomodated (CHA)

								Foots	sion Rate (	41					
	Emission Un	nit	PM	PM <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>x</sub>	VOC	CO CO	tpy) Lead	H <sub>2</sub> S	TRS	CO,	N <sub>2</sub> O	CH₄
		Highest Emitting Month		11110	11112.5	302	i ii o x	Jun-15	-		1120			1120	04
146	Tank 163	Monthly Emissions						0.38							
		Annualized Emissions (CHA)						4.57							
		Highest Emitting Month						Feb-14							
147	Tank 164	Monthly Emissions	_	_	_	_		0.65	_	_		_	_		
		Annualized Emissions (CHA)	-					7.79	_				-		
		Highest Emitting Month	-	-				Feb-14	-	-					
148	Tank 165	Monthly Emissions	-	-		-		1.69	-	-					
		Annualized Emissions (CHA)	-	-		-		20.33	-	-					
		Highest Emitting Month	-	-		-		Jun-15	-	-					
149	Tank 166	Monthly Emissions	-	-		-		0.41	-	-					
		Annualized Emissions (CHA)	-	-		-		4.91	-	-					
		Highest Emitting Month	-	-	-	-		Apr-14	-	-					
150	Tank 168	Monthly Emissions	-	-	-	-		0.02	-	-					
		Annualized Emissions (CHA)	-	-	-	-		0.24	-	-		-	-		
		Highest Emitting Month	-	-	-	-		Jul-14	-	-					
152	Tank 170	Monthly Emissions	-	-	-	-		0.51	-	-		-	-		
		Annualized Emissions (CHA)	-	-	-	-		6.16	-	-		-	-		
		Highest Emitting Month	-	-	-	-	-	Jul-14	-	-		-	-		
155	Tank 174	Monthly Emissions	-	-	-	-		1.15	-	-		-	-		
		Annualized Emissions (CHA)	_	-			-	13.79	-	-					
		Highest Emitting Month	-	-	-	-	-	Jun-15	-	-		-	-		
156	Tank 175	Monthly Emissions	-	-	-	-		1.05	-	-		-	-		
		Annualized Emissions (CHA)	-	-	-	-		12.61	-	-		-	-		-
		Highest Emitting Month	-	-	-	-		Feb-14	-	-		-	-		-
157	Tank 178	Monthly Emissions	-	-	-	-	-	0.49	-	-	-	-	-	-	-
		Annualized Emissions (CHA)	-	-	-	-		5.85	-	-		-	-		-
		Highest Emitting Month	-	-	-	-		Feb-14	-	-	-	-	-	-	-
160	Tank 181	Monthly Emissions	-	-	-	-	-	1.85	-	-	-	-	-	-	-
		Annualized Emissions (CHA)	-	-	-	-		22.24	-	-	-	-	-	-	-
		Highest Emitting Month	-	-	-	-		Feb-14	-	-	-	-	-	-	-
161	Tank 182	Monthly Emissions	-	-	-	-		3.29	-	-	-	-	-	-	-
		Annualized Emissions (CHA)	-	-	-	-		39.43	-	-	-	-	-	-	-
		Highest Emitting Month	-	-	-	-		Jun-14	-	-	-	-	-	-	-
163	Tank 185	Monthly Emissions	-	-	-	-	-	0.98	-	-	-	-	-		-
		Annualized Emissions (CHA)	-	-	-	-	-	11.81	-	-	-	-	-	-	-
		Highest Emitting Month	-	-	-	-	-	Sep-14	-	-	-	-	-	-	-
164	Tank 186	Monthly Emissions	-	-	-	-	-	0.55	-	-	-	-		-	-
		Annualized Emissions (CHA)	-	-	-		-	6.60	-	-	-		-	-	-
	Total Capable of Accommode	ating Emissions	53.48	65.85	65.45	110.09	485.22	381.04	508.31	0.00	19.03	0.77	1,211,292	11.08	64.23
	Baseline Perio	d	Aug-13	Aug-13	Aug-13	Aug-13	Aug-13	Aug-13	Jan-13	Nov-12	Jan-09	Apr-09	Jun-09	Jun-09	Jun-09
	Duscinic 1 crio	-	Jul-15	Jul-15	Jul-15	Jul-15	Jul-15	Jul-15	Dec-14	Oct-14	Dec-10	Mar-11	May-11	May-11	May-11

### Table C-33 Monroe Energy, LLC - Trainer, PA Refinery Project Emission Increases Summary

So	ource	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable BAE)
						ns/vr		1
	<del> </del>	PM PM <sub>10</sub>	84.62 110.60	43.06 63.93	41.56 46.66	93.30 140.78	50.24 76.84	0.00
	1	PM <sub>2.5</sub>	96.21	56.61	39.60	120.81	64.20	0.00
		SO <sub>2</sub>	88.82	46.18	42.64	96.67	50.49	0.00
		$NO_X$	432.52	297.01	135.51	454.41	157.40	0.00
		VOC	3.20	3.18	0.02	3.26	0.08	0.00
101	FCC Unit	CO Lead	16.35	15.63 2.47E-04	0.71	35.45 4.18E-04	19.82 1.71E-04	0.00
101	1	Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		$H_2SO_4$	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	-	-		0.00	-	-
		TRS	-	- 400 255 51		0.00		-
		CO <sub>2</sub> N <sub>2</sub> O	754,773.34 4.42	499,375.51 2.93	255,397.83 1.50	560,274.64 3.28	60,899.13 0.36	194,498.70 1.14
		CH <sub>4</sub>	22.11	14.67	7.44	16.46	1.79	5.65
		PM	0.18	0.10	0.08	0.38	0.28	0.00
		$PM_{10}$	0.72	0.42	0.30	1.52	1.10	0.00
		PM <sub>2.5</sub>	0.72	0.42	0.30	1.52	1.10	0.00
		$SO_2$	0.78	0.44	0.34	1.66	1.22	0.00
		$NO_X$	3.02	1.76	1.26	6.44	4.67	0.00
		VOC	0.52	0.30	0.22	1.10	0.80	0.00
700	FOCUE. 111	CO	7.93	0.93	7.00	11.29	10.36	0.00
733	FCCU Feed Heater	Lead	4.72E-05	3.73E-05	9.89E-06	9.99E-05	6.26E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub> H <sub>2</sub> S	0.00 8.56E-03	0.00	0.00	0.00 0.02	0.00 8.85E-03	0.00
		H <sub>2</sub> S TRS	8.56E-03 8.56E-03	0.01	0.00	0.02	8.85E-03 0.01	0.00
		CO <sub>2</sub>	13,103.51	16,695.75	0.00	34,001.33	17,305.58	0.00
	-	N <sub>2</sub> O	0.13	0.17	0.00	0.35	0.18	0.00
	1	CH <sub>4</sub>	0.67	0.85	0.00	1.73	0.88	0.00
		PM	0.06	0.22	0.00	0.47	0.25	0.00
		$PM_{10}$	0.25	0.36	0.00	0.50	0.15	0.00
		PM <sub>2.5</sub>	0.25	0.36	0.00	0.50	0.15	0.00
		$SO_2$	0.28	0.39	0.00	0.55	0.16	0.00
		$NO_X$	4.51	6.41	0.00	9.20	2.79	0.00
		VOC	0.18	0.26	0.00	0.36	0.11	0.00
	l	СО	2.81	3.23	0.00	5.23	2.00	0.00
735	Kerosene/HCN HTU Feed Heater	Lead	1.67E-05 0.00	1.82E-05 0.00	0.00	2.85E-05	1.03E-05	0.00
	<del> </del>	Fluorides H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	3.09E-03	2.74E-03	3.54E-04	3.74E-03	1.00E-03	0.00
		TRS	3.09E-03	2.77E-03	3.22E-04	4.36E-03	1.59E-03	0.00
		CO <sub>2</sub>	4,728.66	4,319.92	408.74	6,671.34	2,351.42	0.00
		N <sub>2</sub> O	0.05	0.04	4.16E-03	0.07	0.02	0.00
		CH <sub>4</sub>	0.24	0.22	0.02	0.34	0.12	0.00
		PM	0.11	0.24	0.00	0.63	0.39	0.00
		$PM_{10}$	0.62	0.42	0.19	0.68	0.26	0.00
		PM <sub>2.5</sub>	0.62	0.42	0.19	0.68	0.26	0.00
		SO <sub>2</sub>	0.67	0.49	0.18	0.81	0.31	0.00
		NO <sub>X</sub>	13.84	10.39	3.45	16.45	6.07	0.00
		VOC	0.39	0.06	0.34	0.39	0.33	7.36E-03
736	Diesel HTU Heater	CO Lead	0.18 4.05E-05	3.49 3.35E-05	0.00 6.98E-06	10.87 6.47E-05	7.38 3.12E-05	0.00
7.50	Diesel III O Heater	Fluorides	4.05E-05 0.00	0.00	0.98E-06	0.4/E-05 0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S 4	7.45E-03	9.06E-03	0.00	0.01	2.93E-03	0.00
		TRS	7.45E-03	9.24E-03	0.00	0.01	2.75E-03	0.00
		CO <sub>2</sub>	11,394.36	13,802.45	0.00	18,354.99	4,552.54	0.00
		N <sub>2</sub> O	0.12	0.14	0.00	0.19	0.05	0.00
		$CH_4$	0.58	0.70	0.00	0.93	0.23	0.00
		PM	0.15	0.43	0.00	0.79	0.36	0.00
		$PM_{10}$	0.59	0.33	0.26	1.14	0.81	0.00
		PM <sub>2.5</sub>	0.59	0.33	0.26	1.14	0.81	0.00
		$SO_2$	0.61	0.64	0.00	1.20	0.56	0.00
		$NO_X$	7.71	8.01	0.00	15.06	7.05	0.00
	Ι Γ	VOC	0.42	0.44	0.00	0.83	0.39	0.00
		CO	6.48	7.44	0.00	15.41	7.97	0.00
741	D2/VGO Hydrotreater Feed Heater	Lead	3.86E-05	4.78E-05	0.00	9.17E-05	4.39E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		$H_2SO_4$	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	6.70E-03	0.01	0.00	0.02	4.27E-03	0.00
		TRS	6.70E-03	0.01	0.00	0.02	7.79E-03	0.00
		CO <sub>2</sub>	10,254.92	23,209.06	0.00	34,559.53	11,350.47	0.00
	1	N <sub>2</sub> O	0.10	0.24	0.00	0.35	0.12	0.00

### Table C-33 Monroe Energy, LLC - Trainer, PA Refinery Project Emission Increases Summary

		Pollutant	Emissions (PAE)	Emissions (BAE)	Increases (PAE - BAE)	Could Have Been Accomodated (CHA)	Emissions (CHA - BAE)	Increases (PAE - Excludable BAE)
<u> </u>			1			ns/vr		
	-	PM	0.61	1.19	0.00	2.37	1.18	0.00
	-	PM <sub>10</sub>	2.43	1.87	0.56	2.37	0.50	0.06
	-	PM <sub>2.5</sub>	2.43	1.87	0.56	2.37	0.50	0.06
	-	SO <sub>2</sub>	2.55	1.96	0.59	2.49	0.53	0.06
	-	NO <sub>X</sub>	33.29	26.07	7.22	37.04	10.97	0.00
	-	VOC	1.76	1.35	0.41	1.72	0.36	0.04
737	Nonhaho HDC Hoston	СО	26.88	20.86	6.01	26.25	5.38	0.63
757	Naphtha HDS Heater	Lead	1.60E-04	1.22E-04	3.83E-05	1.56E-04	3.45E-05	3.75E-06
	<b>-</b>	Fluorides H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
	ŀ	H <sub>2</sub> SO <sub>4</sub>	0.03	0.02	6.14E-03	0.03	6.98E-03	0.00
	ŀ	TRS	0.03	0.02	6.68E-03	0.03	7.52E-03	0.00
	ŀ	CO <sub>2</sub>	43,298.56	33,037.72	10,260.84	44,576.75	11,539.03	0.00
	H	N <sub>2</sub> O	0.44	0.34	0.10	0.45	0.12	0.00
	ŀ	CH <sub>4</sub>	2.20	1.68	0.52	2.27	0.59	0.00
+		PM	4.06	8.45	0.00	15.12	6.67	0.00
	<u> </u>	PM <sub>10</sub>	16.23	13.44	2.79	15.46	2.01	0.78
	ļ	PM <sub>2.5</sub>	16.23	13.44	2.79	15.46	2.01	0.78
	Ţ	$SO_2$	17.03	14.10	2.92	16.21	2.11	0.81
	Ţ.	$NO_X$	185.70	147.14	38.57	174.17	27.04	11.53
		VOC	11.75	9.73	2.02	11.19	1.46	0.56
		CO	0.15	1.57	0.00	7.11	5.54	0.00
738	Platformer Feed Heater	Lead	1.07E-03 0.00	9.42E-04 0.00	1.26E-04 0.00	1.10E-03 0.00	1.61E-04 0.00	0.00
		Fluorides H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
	<u> </u>	H <sub>2</sub> S	0.18	0.19	0.00	0.21	0.02	0.00
		TRS	0.18	0.19	0.00	0.21	0.02	0.00
		CO <sub>2</sub>	280,870.92	284,157.46	0.00	319,415.38	35,257.92	0.00
	Ī	N <sub>2</sub> O	2.86	2.89	0.00	3.25	0.36	0.00
		CH <sub>4</sub>	14.28	14.45	0.00	16.24	1.79	0.00
		PM	0.26	0.55	0.00	1.07	0.52	0.00
	-	$PM_{10}$	1.03	0.96	0.07	1.39	0.43	0.00
		PM <sub>2.5</sub>	1.03	0.96	0.07	1.39	0.43	0.00
		SO <sub>2</sub> NO <sub>X</sub>	1.08 16.77	1.01 15.65	0.07 1.12	1.46 21.75	0.45 6.10	0.00
		VOC	0.75	0.70	0.05	1.01	0.31	0.00
	<del> </del>	CO	11.43	11.21	0.22	16.45	5.24	0.00
739	Isocracker 1st Stage Heater	Lead	6.80E-05	6.49E-05	3.08E-06	9.76E-05	3.27E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		$H_2SO_4$	0.00	0.00	0.00	0.00	0.00	0.00
	_	H <sub>2</sub> S	0.01	9.24E-03	3.04E-03	0.02	5.95E-03	0.00
	-	TRS	0.01	9.38E-03	2.90E-03	0.02	5.81E-03	0.00
	-	CO <sub>2</sub> N <sub>2</sub> O	18,800.69 0.19	14,711.55 0.15	4,089.14 0.04	23,249.17 0.24	8,537.61 0.09	0.00
	-	CH <sub>4</sub>	0.19	0.75	0.04	1.18	0.43	0.00
		PM	0.34	0.69	0.00	1.50	0.81	0.00
	ļ.	PM <sub>10</sub>	1.37	1.19	0.18	1.50	0.31	0.00
	ļ	PM <sub>2.5</sub>	1.37	1.19	0.18	1.50	0.31	0.00
	Į	$SO_2$	1.44	1.25	0.19	1.58	0.32	0.00
		$NO_X$	18.05	15.70	2.36	19.76	4.07	0.00
	<u> </u>	VOC	0.99	0.86	0.13	1.09	0.22	0.00
740	Isocracker Splitter Reboiler	CO Lead	15.17 9.03E-05	13.38 7.83E-05	1.78 1.20E-05	17.58 1.05E-04	4.19 2.64E-05	0.00
740	250cracker Spiriter Reporter	Lead Fluorides	9.03E-05 0.00	7.83E-05 0.00	1.20E-05 0.00	1.05E-04 0.00	2.64E-05 0.00	0.00
	ŀ	H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
	ļ-	H <sub>2</sub> S 0 <sub>4</sub>	0.02	0.01	5.29E-03	0.02	4.02E-03	1.27E-03
	ļ	TRS	0.02	0.01	4.70E-03	0.02	3.90E-03	8.04E-04
	Ţ	CO <sub>2</sub>	25,067.59	18,382.52	6,685.07	23,836.53	5,454.01	1,231.06
	Ţ	$N_2O$	0.25	0.19	0.07	0.24	0.06	0.01
		CH <sub>4</sub>	1.27	0.93	0.34	1.21	0.28	0.06
	ļ.	PM	0.27	0.18	0.09	0.29	0.12	0.00
	<u> </u>	PM <sub>10</sub>	1.06	0.71	0.36	1.17	0.46	0.00
	Ļ	PM <sub>2.5</sub>	1.06	0.71	0.36	1.17	0.46	0.00
	ļ	SO <sub>2</sub>	1.16	0.77	0.39	1.28	0.50	0.00
	ļ	NO <sub>X</sub>	20.50	13.38	7.12	21.87	8.49	0.00
	Ļ	VOC	0.77	0.51	0.26	0.85	0.33	0.00
	Trop 5 · · · · · ·	СО	11.76	7.34	4.41	11.34	4.00	0.41
742	VCD 541 VAC Heater	Lead	7.00E-05	4.31E-05	2.69E-05	6.75E-05	2.45E-05	2.46E-06
742 VCD 541 VAC	ļ	Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
			0.01	9.43E-03	3.97E-03	0.01	2.88E-03	1.10E-03
		H <sub>2</sub> S						
	-	TRS	0.01	9.09E-03	4.31E-03	0.01	2.57E-03	1.74E-03
							2.57E-03 4,050.79 0.04	1.74E-03 2,665.46 0.03

### Table C-33 Monroe Energy, LLC - Trainer, PA Refinery Project Emission Increases Summary

Sc	ource	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable BAE)
		PM	0.15	0.44	0.00	1.32	0.88	0.00
		PM <sub>10</sub>	0.62	0.78	0.00	1.32	0.53	0.00
		PM <sub>2.5</sub>	0.62	0.78	0.00	1.32	0.53	0.00
		SO <sub>2</sub>	0.67	0.44	0.24	0.76	0.32	0.00
		NO <sub>X</sub>	6.75	4.48	2.27	7.52	3.04	0.00
		VOC	0.03	0.02	9.65E-03	0.03	0.01	0.00
		CO	0.02	0.01	8.67E-03	0.02	0.01	0.00
743	VCD 542 VAC Heater	Lead	4.06E-05	2.38E-05	1.68E-05	4.60E-05	2.22E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	7.45E-03	0.01	0.00	0.01	2.44E-03	0.00
		TRS	7.45E-03	0.01	0.00	0.01	1.78E-03	0.00
		CO <sub>2</sub>	11,394.36	17,771.31	0.00	20,631.05	2,859.74	0.00
		N <sub>2</sub> O	0.12	0.18	0.00	0.21	0.03	0.00
		CH <sub>4</sub>	0.58	0.90	0.00	1.05	0.15	0.00
		PM	0.55	1.35	0.00	3.20	1.85	0.00
		$PM_{10}$	2.19	2.88	0.00	3.36	0.48	0.00
		PM <sub>2.5</sub>	2.19	2.88	0.00	3.36	0.48	0.00
		SO <sub>2</sub>	2.39 12.44	2.37 12.53	0.02	2.88 14.63	0.52 2.10	0.00
		NO <sub>X</sub> VOC	2.18	12.53	0.00	14.63 2.56	2.10 0.37	0.00
		CO	5.29	1.34	3.95	5.41	4.07	0.00
746	VCD 544 VAC Heater	Lead	1.44E-04	1.40E-04	4.35E-06	1.74E-04	3.41E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		$H_2SO_4$	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	0.03	0.02	2.82E-03	0.03	6.33E-03	0.00
		TRS	0.03	0.02	3.19E-03	0.03	6.71E-03	0.00
		CO <sub>2</sub>	40,449.97	35,464.65	4,985.32	45,828.20	10,363.55	0.00
		N <sub>2</sub> O	0.41	0.36	0.05	0.47	0.11	0.00
		CH <sub>4</sub> PM	2.06 2.01	1.80 4.32	0.25	2.33 8.66	0.53 4.35	0.00
		PM <sub>10</sub>	8.02	7.22	0.80	8.76	1.54	0.00
		PM <sub>2.5</sub>	8.02	7.22	0.80	8.76	1.54	0.00
		SO <sub>2</sub>	8.77	7.89	0.87	9.57	1.68	0.00
		$NO_X$	45.55	28.30	17.25	49.71	21.41	0.00
		VOC	5.81	5.23	0.58	6.34	1.11	0.00
		CO	88.66	81.32	7.34	96.84	15.52	0.00
744	ACD 543 Crude Heater	Lead	5.28E-04	4.82E-04	4.59E-05	5.76E-04	9.45E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		$H_2SO_4$ $H_2S$	0.00	0.00	0.00 3.83E-03	0.00 0.11	0.00	0.00
		TRS	0.10	0.09	3.21E-03	0.11	0.01	0.00
		CO <sub>2</sub>	148,126.65	143,860.54	4,266.12	166,202.49	22,341.96	0.00
		N <sub>2</sub> O	1.51	1.46	0.04	1.69	0.23	0.00
		CH <sub>4</sub>	7.53	7.31	0.22	8.45	1.14	0.00
		PM	2.00	4.68	0.00	9.23	4.55	0.00
		PM <sub>10</sub>	8.01	7.59	0.43	9.23	1.64	0.00
		PM <sub>2.5</sub>	8.01	7.59	0.43	9.23	1.64	0.00
		SO <sub>2</sub> NO <sub>x</sub>	8.75 50.11	8.29 32.82	0.47 17.28	10.08 56.20	1.80 23.37	0.00
		VOC	5.80	5.49	0.31	6.68	1.19	0.00
		CO	88.55	83.63	4.93	102.01	18.38	0.00
745	ACD 544 Crude Heater	Lead	5.27E-04	4.91E-04	3.59E-05	6.07E-04	1.16E-04	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	0.10	0.09	3.40E-03	0.10	9.51E-03	0.00
		TRS CO <sub>2</sub>	0.10	0.09	1.93E-03	0.10 157,482.30	8.04E-03	0.00
		N <sub>2</sub> O	148,126.65 1.51	145,398.35 1.48	2,728.31 0.03	157,482.30	12,083.95 0.12	0.00
		CH <sub>4</sub>	7.53	7.39	0.03	8.01	0.61	0.00
	1	PM	0.72	0.53	0.20	0.89	0.36	0.00
		$PM_{10}$	5.69	1.69	4.01	5.62	3.93	0.07
		PM <sub>2.5</sub>	5.07	1.51	3.57	5.29	3.79	0.00
		SO <sub>2</sub>	1.04	1.93	0.00	3.24	1.31	0.00
		NO <sub>X</sub>	4.41	4.14	0.27	4.91	0.77	0.00
		VOC	0.31	0.11	0.20	0.35	0.25	0.00
		CO	1.34	1.17	0.17	1.41	0.25	0.00
34	Boiler 9	Lead	4.80E-04	4.51E-04	2.91E-05	5.60E-04	1.09E-04	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> S	0.09	0.06	0.03	0.09	0.03	1.70E-03
		TRS	0.09	0.06	0.03	0.09	0.03	1.70E-03
		CO <sub>2</sub>	115,228.12	72,880.82	42,347.30	109,168.22	36,287.41	6,059.89
	1	N <sub>2</sub> O	2.11	0.14	1.98	0.21	0.07	1.91
				1.37	0.83	2.06	0.68	0.15

So	urce	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable BAE)
		PM	0.40	0.38	0.02	0.58	0.20	0.00
		$PM_{10}$	3.07	1.06	2.01	3.14	2.08	0.00
		PM <sub>2.5</sub>	2.97	1.01	1.97	3.07	2.06	0.00
		SO <sub>2</sub>	2.97	1.91	1.06	3.35	1.44	
		NO <sub>X</sub>	3.93	3.89	0.04	5.09	1.20	
		VOC	0.27	0.10	0.17	0.31	0.22	
		СО	4.93	8.72	0.00	16.67		
35	Boiler 10	Lead	4.60E-04	4.32E-04	2.76E-05	5.45E-04		
		Fluorides	0.00	0.00	0.00	0.00		
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00		
		H <sub>2</sub> S	0.08	0.06	0.02	0.09		
		TRS	0.08	0.06	0.02	0.09		
		CO <sub>2</sub>	110,341.81	83,481.92	26,859.89	113,628.58		
		N <sub>2</sub> O	2.02	0.16	1.87	0.21		
		CH <sub>4</sub>	2.11	1.57	0.54	2.14		1
		PM	0.11	0.10	0.01	0.14		1
		PM <sub>10</sub>	0.44	0.38	0.07	0.58		
		PM <sub>2.5</sub>	0.44	0.38	0.07	0.58	0.20	0.00
		SO <sub>2</sub>	40.33	19.27	21.06	27.98	8.70	12.36
		NO <sub>X</sub>	5.83	5.22	0.62	8.23	3.02	0.00
		VOC	0.32	0.24	0.08	0.37	0.13	0.00
		CO	4.90	3.56	1.34	5.62	2.05	0.00
102	SRU	Lead	2.92E-05	2.04E-05	8.78E-06	3.34E-05	1.30E-05	0.00
		Fluorides	0.00	0.00	0.00	0.00	0.00	0.00
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00		
		H <sub>2</sub> S	0.00	0.00	0.00	0.00		
		TRS	-	-	-	0.00		
		CO <sub>2</sub> N <sub>2</sub> O	29,513.46 0.30	2,852.70 0.06	26,660.76 0.24	3,542.78 0.07		
		N <sub>2</sub> O CH <sub>4</sub>	89.09	5.88E-03	89.08	7.31E-03		
		PM	1.25	4.05	0.00	6.83		
		PM <sub>10</sub>	1.74	5.04	0.00	8.11		
		PM <sub>2.5</sub>	1.74	5.04	0.00	8.11	8.70 12.36 3.02 0.00 0.13 0.00 2.05 0.00 1.30E-05 0.00 0.00 0.00 0.00 0.00 0.00 0.00	
		SO <sub>2</sub>	4.15	10.04	0.00	25.00	14.96	1.44         0.00           1.20         0.00           0.22         0.00           0.94         0.00           0.05         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.02         0.00           0.06         1.81           0.57         0.00           0.05         0.00           0.20         0.00           0.20         0.00           0.20         0.00           0.20         0.00           0.20         0.00           0.21         0.00           0.22         0.00           0.03         0.00           0.04         0.00           0.05         0.00           0.01         12.36           0.02         0.00           0.03         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00 </td
		$NO_X$	3.15	10.19	0.00	17.20	0.20         0.00           0.20         0.00           8.70         12.36           3.02         0.00           0.13         0.00           2.05         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.00         0.00           -         -           690.08         25,970.68           0.01         0.22           1.42E-03         89.08           2.78         0.00           3.07         0.00           3.07         0.00           7.00         0.00           97.59         0.00           100.71         0.00           2.95E-04         0.00           0.00         0.00           0.00         0.00           0.00         0.00           0.34         0.00           0.34         0.00           4.87         4.19           -         -           -         -           -         -           -         -           - <t< td=""><td>0.00</td></t<>	0.00
		VOC	6.48	33.12	0.00	130.71		0.00
		CO	17.13	58.11	0.00	158.82		
103	Main Flare	Lead	2.14E-04	1.14E-04	9.96E-05	4.09E-04		
		Fluorides	0.00	0.00	0.00	0.00		
		H <sub>2</sub> SO <sub>4</sub>	0.00	0.00	0.00	0.00		
		H <sub>2</sub> S	2.47	14.23	0.00	18.26		
		TRS CO <sub>2</sub>	5,902.69	51,382.53	0.00	0.00 72,299.13		
		N <sub>2</sub> O	0.06	0.96	0.00	1.30		
		CH <sub>4</sub>	17.82	8.75	9.07	13.62		
		PM	-	-	-	-		-
		PM <sub>10</sub>	-	-	-	-		-
		PM <sub>2.5</sub>	-	-	-	-		
		SO <sub>2</sub>	-	-	-	-	-	-
		$NO_X$	-	-	-	-		
		VOC	1.92	2.46	0.00	2.03		
165	Toute 02	CO	-	-	-	-		
165	Tank 93	Lead	-	-	-	-		
		Fluorides H <sub>2</sub> SO <sub>4</sub>	-	-	-	-		
		H <sub>2</sub> SO <sub>4</sub> H <sub>2</sub> S	-	-	-	-		
		TRS	-	-	-	-		
		CO <sub>2</sub>	-	-	-	-		+
		N <sub>2</sub> O	-	-	-	-		
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		$NO_X$	-	-	-	-	-	-
		VOC	2.76	1.61	1.15	2.87	1.26	0.00
		CO	-	-	-	-	-	-
166	Tank 94	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub>	-	-	-	-	-	-
	ĺ	N <sub>2</sub> O	-	-	-	-	-	-

Sou	irce	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable BAE)
					tor	ns/vr		_
[		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		$SO_2$	-	-	-	-	-	-
		$NO_X$	-		-	-		-
		VOC	3.46	2.13	1.33	3.54	1.42	0.00
		CO	-	-	-	-	-	-
126	Tank 95	Lead	-	-	-	-	-	-
		Fluorides	-		-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	
		CO <sub>2</sub>	-	-	-	-	-	-
		N <sub>2</sub> O	-	-	-	-	-	-
		CH <sub>4</sub>	-		-	-	-	-
<del></del>		PM	-	-	-	-	-	-
[		PM <sub>10</sub>	-	-	-	-	-	-
[		PM <sub>10</sub> PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub>	-	-	-	-	-	-
		VOC	4.45	3.27	1.19	4.61	1.34	0.00
		CO	-	-	-	-	-	-
127	Tank 96	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-		-
		$H_2SO_4$	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		$CO_2$	-		-	-		-
		$N_2O$	-	-	-	-	-	-
		$CH_4$	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub>	-		-		-	
		VOC	5.06	1.38	3.68	0.23	-1.15E+00	4.83
127	Tank 152	СО	-	-	-	-	-	-
137	1 alik 132	Lead	-	-	-	-	-	-
		Fluorides H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub>	-	-	-	-	-	-
		N <sub>2</sub> O	-	-	-	_	-	-
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-		-
		$SO_2$	-	-	-	-	-	-
		$NO_X$	-	-	-	-	-	-
		VOC	0.19	0.15	0.03	0.21	0.06	0.00
		CO	-	-	-	-	-	-
138	Tank 153	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
[		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub> N <sub>2</sub> O	-	-	-	-	-	-
		N <sub>2</sub> O CH <sub>4</sub>	-	-	-	-	-	
		PM	-	-	-	-	-	-
		PM <sub>10</sub>	-	-	-	-	-	-
		PM <sub>10</sub> PM <sub>2.5</sub>	-	-	-	-		-
		PM <sub>2.5</sub> SO <sub>2</sub>					-	
			-	-	-	-	-	-
		NO <sub>X</sub>	-	-	-	- 0.00	-	-
		VOC	0.18	0.13	0.05	0.22	0.09	0.00
	m 1	CO	-	-	-	-	-	-
140	Tank 155	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		$H_2SO_4$	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
[		CO <sub>2</sub>	-	-	-	-	-	-
II .		N <sub>2</sub> O	-		-	-	-	-
			1	-	-	-	-	-

Sou	irce	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable
					1	ns/vr		
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		$SO_2$	-	-	-	-	-	-
		$NO_X$	-		-	-		-
		VOC	0.21	0.15	0.06	0.24	0.09	0.00
		CO	-	-	-	-	-	-
142	Tank 157	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub>	-	-	-	-	-	-
		N <sub>2</sub> O	-	-	-	-	-	
il l		N <sub>2</sub> O CH <sub>4</sub>	-	-	-	-	-	-
il l		PM PM <sub>10</sub>	-	-	-	-	-	-
il l		PM <sub>10</sub> PM <sub>2.5</sub>	-	-	-	-	-	-
		PM <sub>2.5</sub> SO <sub>2</sub>	-	-	-	-	-	-
il l		NO <sub>X</sub>	-	-	-	-	-	-
		VOC	13.15	3.50	9.66	28.01	24.51	0.00
il l		CO	13.13	3.30	9.00	28.01	24.51	- 0.00
300	Tank 158 (Source ID 193)	Lead	-	-	-	-	-	-
200	(Source ID 175)	Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	_	-	-	_	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub>	-	-	-	-	-	-
		N <sub>2</sub> O	-	-	-	-	-	-
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		$NO_X$	-		-	-		-
		VOC	3.97	3.32	0.65	4.06	0.74	0.00
		СО	-	-	-	-	-	-
143	Tank 159	Lead	-		-	-		-
		Fluorides	-	-	-	-	-	-
		$H_2SO_4$	-		-	-		-
		$H_2S$	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		$CO_2$	-	-	-	-	-	-
		$N_2O$	-	-	-	-	-	-
		$CH_4$	-	-	-	-	-	-
<u> </u>		PM	-		-	-	ı	-
		$PM_{10}$	-	-	-	-	-	-
(I		PM <sub>2.5</sub>	-		-	-	-	-
il l		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub>	-	-	-	-		
il l		VOC	0.22	4.86	0.00	0.26	-4.61E+00	0.00
104	Tank 160	CO	-	-	-	-	-	-
194	1 ank 160	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-		t		-
il l		H <sub>2</sub> S	-	-	-	-	-	-
		TRS			-	t		+
(I		CO <sub>2</sub> N <sub>2</sub> O	-	-	-	-	-	-
il l		N <sub>2</sub> O CH <sub>4</sub>	-		-	-	-	
( <del>                                     </del>		PM	-	-	-	-	-	-
1		PM PM <sub>10</sub>	-	-	-	-	-	-
						t		+
1		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
1		NO <sub>X</sub>	-	-	-	-	-	-
		VOC	6.04	2.70	3.34	6.21	3.51	0.00
		CO	-	-	-	-	-	-
144	Tank 161	Lead	-		-	-	1	-
144		Fluorides	-		-	-	1	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
								1
		H <sub>2</sub> S	-	-	-	-	-	-
			-	-	-	-	-	-
		H <sub>2</sub> S		-				
		H <sub>2</sub> S TRS	-		-	-	-	-

Sou	urce	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable BAE)
		PM	-	-	-	-	-	-
		PM <sub>10</sub>	-	-	-	-	-	-
	'	PM <sub>2.5</sub>	-	-	-	-	-	-
	<u>'</u>	SO <sub>2</sub>	-	-	-	-	-	-
	<u>'</u>	$NO_X$	-	-	-	-	-	-
	'	VOC	3.25	0.87	2.39	6.36	5.49	0.00
	'	CO	-	-	-	-	-	-
145	Tank 162	Lead	-	-	-	-	-	-
	'	Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-		
	'	H <sub>2</sub> S	-	-	-	-		+
	'	TRS CO <sub>2</sub>	-	-	-	-		
	'	N <sub>2</sub> O	-	-	-	-		
	'	CH <sub>4</sub>	-	-	-	-		
		PM	-	-	-	-		
		PM <sub>10</sub>	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub>	-	-	-	-	-	-
		VOC CO	4.25	1.60	2.64	4.57		
146	Tank 163	Lead	-	-	-	-		
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub> N <sub>2</sub> O	-	-	-	-		
		N <sub>2</sub> O CH <sub>4</sub>	-	-	-	-		
		PM	-	-	-	-	-	-
		PM <sub>10</sub>	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-		
		SO <sub>2</sub>	-	-	-	-		+
		NO <sub>X</sub>	2.70	2.52	- 1.26	7.70		1
		VOC CO	3.79	2.53	1.26	7.79		
147	Tank 164	Lead	-	-	-	-		
	1	Fluorides	-	-	-	-		+
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-		
		H <sub>2</sub> S	-	-	-	-		
		TRS	-	-	-	-		+
		CO <sub>2</sub> N <sub>2</sub> O	-	-	-	-		
		N <sub>2</sub> O CH <sub>4</sub>	-	-	-	-		
		PM	-	-	-	-		
		$PM_{10}$	-	-	-	-		
		PM <sub>2.5</sub>	-	-	-	-		
		SO <sub>2</sub>	-	-	-	-		
		NO <sub>X</sub> VOC	8.26	3.09	5.17	20.33		
		CO	8.20	3.09	5.17	-		
148	Tank 165	Lead	-	-	-	-		
		Fluorides	-	-	-	-		
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-		
		H <sub>2</sub> S	-	-	-	-		
		TRS CO <sub>2</sub>	-	-	-	-		+
		N <sub>2</sub> O	-	-	-	-		
	<u>                                     </u>	CH <sub>4</sub>	-	-	-	-		+
		PM	-	-	-	-		
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-		+
		SO <sub>2</sub>	-	-	-	-		
		NO <sub>X</sub>	-	-	-	-		
		VOC	3.55	2.16	1.40	4.91		
140	mode tee	CO	-	-	-	-		
149	Tank 166	Lead	-	-	-	-		
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub> H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub>	-	-	-	-	-	-
	1							
l i		$N_2O$	-	-	-	-	-	-

Sou	irce	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable BAE)
		DM	1		1	ns/vr		1
		PM	-	-	-	-		
		PM <sub>10</sub>	-	-	-	-		+
		PM <sub>2.5</sub>	-	-	-	-		
		$SO_2$	-	-	-	-	-	-
		$NO_X$	-	-	-	-	-	-
		VOC	2.89	1.53	1.36	0.24		
		CO	-	-	-	-		
150	Tank 168	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		$H_2SO_4$	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-		-
		TRS	-	-	-	-	-	-
		$CO_2$	-	-	-	-	-	-
		$N_2O$	-	-	-	-	-	-
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		$NO_X$	-	-	-	-	-	-
		VOC	6.13	3.02	3.11	6.16	3.15	0.00
		CO	-	-	-	-	-	-
152	Tank 170	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-		
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-		
		H <sub>2</sub> S	-	-	-	-		
		TRS CO <sub>2</sub>	-	-	-	-		
	•	N <sub>2</sub> O	-	-	-	-		+
		CH <sub>4</sub>	-	-	-	-		
		PM	-	-	-	-		
		PM <sub>10</sub>	-	-	-	-		
		PM <sub>2.5</sub>	-	-	-	-		
		SO <sub>2</sub>	-	-	-	-		
		NO <sub>X</sub>	-	-	-	-	-	-
		VOC	12.01	4.09	7.92	13.79	9.70	0.00
		CO	-	-	-	-	-	-
155	Tank 174	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		$H_2SO_4$	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-		-
		CO <sub>2</sub>	-	-	-	-		
		N <sub>2</sub> O	-	-	-	-		
		CH <sub>4</sub> PM	-	-	-	-		
		PM PM <sub>10</sub>	-	-	-	-		
		PM <sub>2.5</sub>	-	-	-	-		
		SO <sub>2</sub>	-	-	-	-		
		NO <sub>X</sub>	-	-	-	-	-	-
		VOC	7.43	5.35	2.07	12.61	7.25	0.00
		CO	-	-	-	-	-	-
156	Tank 175	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-1.29E+00 -1.29E	-
		$H_2SO_4$	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-		-
		TRS	-	-	-	-		-
	l l	CO <sub>2</sub>	-	-	-	-		-
		N <sub>2</sub> O	-	-	-	-		-
		CH <sub>4</sub>	-	-	-	-		
		PM	-	-	-	-		
		PM <sub>10</sub>	-	-	-	-		
		PM <sub>2.5</sub>	-	-	-	-	BAE)	
	l l	SO <sub>2</sub>	-	-	-	-		
		$NO_X$	-	-	-	-		
		VOC	3.23	4.53	0.00	5.85	1.32	0.00
	[	CO	-	-	-	-		-
157	Tank 178	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		$H_2SO_4$	-	-	-	-		-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-		
		CO <sub>2</sub>	-	-	-	-		+
				-	-	-		
	l l	$N_2O$	-	-				

Sou	ırce	Pollutant	Projected Actual Emissions (PAE)	Baseline Actual Emissions (BAE)	Emission Increases (PAE - BAE)	Emissions Which Could Have Been Accomodated (CHA)	Excludable Emissions (CHA - BAE)	Total Project Emission Increases (PAE - Excludable
					to	ns/vr		
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub>	-	-	-	-	-	-
		VOC	8.75	3.03	5.72	22.24	19.21	0.00
1.50	T 1 101	СО	-	-	-	-	-	-
160	Tank 181	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub> H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-		-	-	-	-
		CO <sub>2</sub>	-	-	-	-	-	<u> </u>
		N <sub>2</sub> O	-	-	-	-	-	-
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub> VOC	20.52	- 6.52	-	- 20.42	- 22.01	- 0.00
		CO	20.53	6.52	14.01	39.43	32.91	0.00
161	Tank 182	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS	-	-	-	-	-	-
		CO <sub>2</sub> N <sub>2</sub> O	-	-	-	-	-	-
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
	Tank 185	PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub>	-	-	-	-	-	-
		NO <sub>X</sub> VOC	11.26	7.02	4.23	11.81	4.78	0.00
		co	- 11.20	7.02	4.23	-	4.78	- 0.00
163		Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-		-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS CO <sub>2</sub>	-	-	-	-	-	-
		N <sub>2</sub> O	-	-	-	-	-	-
		CH <sub>4</sub>	-	-	-	-	-	-
		PM	-	-	-	-	-	-
		$PM_{10}$	-	-	-	-	-	-
		PM <sub>2.5</sub>	-	-	-	-	-	-
		SO <sub>2</sub> NO <sub>V</sub>	-	-	-	-	-	-
		VOC	5.47	4.75	0.72	6.60	1.85	0.00
		co	-	4.73	- 0.72	-	-	-
164	Tank 186	Lead	-	-	-	-	-	-
		Fluorides	-	-	-	-	-	-
		H <sub>2</sub> SO <sub>4</sub>	-	-	-	-	-	-
		H <sub>2</sub> S	-	-	-	-	-	-
		TRS CO <sub>2</sub>	-	-	-	-	-	-
		N <sub>2</sub> O	-	-	-	-	-	-
		CH <sub>4</sub>	-	-	-	-	_	-

#### Table C-34 Monroe Energy, LLC - Trainer, PA Refinery PSD Applicability Assessment Summary

					Pi	roject Rela	ted Emissio	ns Increas	e (tpy)			
	Emission Unit	PM	PM <sub>10</sub>	PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>X</sub>	VOC	co	Lead	H <sub>2</sub> S	TRS	CO <sub>2</sub> e <sup>(a),(b)</sup>
101	FCC Unit	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-	-	-	194,979.46
733	FCCU Feed Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
735	Kerosene/HCN HTU Feed Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
736	Diesel HTU Heater	0.00	0.00	0.00	0.00	0.00	7.36E-03	0.00	0.00	0.00	0.00	0.00
741	D2/VGO Hydrotreater Feed Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
737	Naphtha HDS Heater	0.00	0.06	0.06	0.06	0.00	0.04	0.63	3.75E-06	0.00	0.00	0.00
738	Platformer Feed Heater	0.00	0.78	0.78	0.81	11.53	0.56	0.00	0.00	0.00	0.00	0.00
739	Isocracker 1st Stage Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
740	Isocracker Splitter Reboiler	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	1.27E-03	8.04E-04	1,236.35
742	VCD 541 VAC Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.41	2.46E-06	1.10E-03	1.74E-03	2,676.92
743	VCD 542 VAC Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
746	VCD 544 VAC Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
744	ACD 543 Crude Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
745	ACD 544 Crude Heater	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
34	Boiler 9	0.00	0.07	0.00	0.00	0.00	0.00	0.00	0.00	1.70E-03	1.70E-03	6,631.89
35	Boiler 10	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	539.02
102	SRU	0.00	0.00	0.00	12.36	0.00	0.00	0.00	0.00	0.00	-	28,263.81
103	Main Flare	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	-	104.87
165	Tank 93	-	-	-	-	-	0.00	-	-	-	-	-
166	Tank 94	_	_	-	-	-	0.00	_	-	-	-	-
126	Tank 95	_	_	-	-	-	0.00	_	-	-	-	-
127	Tank 96	-	_	_	_	_	0.00	_	_	_	_	_
137	Tank 152	_	_	_	-	_	4.83	_	_	_	_	_
138	Tank 152	-	-	-	-	_	0.00	-	-	-	-	-
140	Tank 155	-	-	-	-	_	0.00	-	-	_	-	-
142	Tank 157	-	_	_		_	0.00	_	_	-	_	_
300	Tank 158 (Source ID 193)	-	_	_		_	0.00	_	_	-	_	_
143	Tank 159	-	-	-	-	_	0.00	-	-	-	-	_
194	Tank 160	-	_	-	-	_	0.00	-	_	-	-	_
144	Tank 161	_	_	_	-	_	0.00	-	_	-	-	_
145	Tank 162	-		_		_	0.00	_	† <u> </u>	_		
146	Tank 163	_	_	-	-	_	0.00	-		_	-	
147	Tank 164	_	-	-	-		0.00	-	-	-	-	-
148	Tank 165	-	_			_	0.00			_		
149	Tank 166						0.00			_		
150	Tank 168	-	-	-	-	_	2.65	-	-	_	-	_
152	Tank 170	_	_		-	_	0.00		-	_	-	
155	Tank 170	-		<u> </u>	-	<u> </u>	0.00			-		
156	Tank 174 Tank 175	-	-	-	-	-	0.00	-	-	-	-	-
157	Tank 178	-		-	-	-	0.00	-	-	-	-	-
160	Tank 176	-	-	-	-	-	0.00	-	-	-	-	
161	Tank 182	-		<del></del>	-	<del></del>	0.00	-	<del> </del>			<del></del>
163	Tank 185				-	-	0.00		-	-	-	
164	Tank 186		-	-	-	-	0.00	-	-	-	-	-
N/A	New Feed Heaters	3.15	3.15	3.15	4.42	22.04	3.15	17.08	2.66E-04	-	-	81,935.43
N/A	New Cooling Tower	0.16	0.16	0.16	4.42	22.04	6.02	- 17.06	2.00E-04		<del></del>	01,733.43
N/A N/A	Additional Fugitive Emissions	0.16	0.10	0.16		-	5.13	-	-	-	-	<del>-</del>
	al Project Emissions Increases	3.31	4.21	4.14	17.65	33.57	22.38	18.12	2.73E-04	4.06E-03	4.25E-03	316,367.75
		25	15	10	40	40	40	18.12	2./3E-04 0.6	4.06E-03		
r	PSD Significance Threshold										10	75,000
	PSD Significant?	No	No	No	No	No	No	No	No	No	No	No

<sup>(</sup>a) CO<sub>2</sub>e is carbon dioxide equivalent, calculated according to 40 CFR 98 Equation A-1:

$$CO_2e = \sum_{i=1}^n GHG_i \times GWP_i$$

 $\label{eq:where GHGi} where GHGi = annual mass emissions of greenhouse gas i (short tons/year)$   $GWPi = global \ warming \ potential \ of \ greenhouse \ gas \ i \ from \ the \ table \ below$ 

Pollutant	GWP (100 year)
$CO_2$	1
$N_2O$	298
CH <sub>4</sub>	25

<sup>(</sup>b) A June 23, 2014 decision by the U.S. Supreme Court, in Utility Air Regulatory Group v. EPA , rules that PSD for greenhouse gas (GHG) emissions need only be considered when permitting already triggers PSD permitting for one of the convention PSD pollutants.

ULSG PAA Emissions Inventory (9-14-15).xlsx

# Table C-35 Monroe Energy, LLC - Trainer, PA Refinery NNSR Applicability Assessment Summary

		Proj	ject Relate	d Emissions	s Increase (	(tpy)
	Emission Unit		PM <sub>2.5</sub> NNSR	Ozone NNSR		
	-	PM <sub>2.5</sub>	SO <sub>2</sub>	NO <sub>X</sub>	NO <sub>x</sub>	VOC
101	FCC Unit	0.00	0.00	0.00	0.00	0.00
733	FCCU Feed Heater	0.00	0.00	0.00	0.00	0.00
735	Kerosene/HCN HTU Feed Heater	0.00	0.00	0.00	0.00	0.00
736	Diesel HTU Heater	0.00	0.00	0.00	0.00	0.01
741	D2/VGO Hydrotreater Feed Heater	0.00	0.00	0.00	0.00	0.00
737	Naphtha HDS Heater	0.06	0.06	0.00	0.00	0.04
738	Platformer Feed Heater	0.78	0.81	11.53	11.53	0.56
739	Isocracker 1st Stage Heater	0.00	0.00	0.00	0.00	0.00
740	Isocracker Splitter Reboiler	0.00	0.00	0.00	0.00	0.00
742	VCD 541 VAC Heater	0.00	0.00	0.00	0.00	0.00
743	VCD 542 VAC Heater	0.00	0.00	0.00	0.00	0.00
746	VCD 544 VAC Heater	0.00	0.00	0.00	0.00	0.00
744	ACD 543 Crude Heater	0.00	0.00	0.00	0.00	0.00
745	ACD 544 Crude Heater	0.00	0.00	0.00	0.00	0.00
34	Boiler 9	0.00	0.00	0.00	0.00	0.00
35	Boiler 10	0.00	0.00	0.00	0.00	0.00
102	SRU	0.00	12.36	0.00	0.00	0.00
103	Main Flare	0.00	0.00	0.00	0.00	0.00
165	Tank 93	-	-	-	-	0.00
166	Tank 94	-	-	-	-	0.00
126	Tank 95	-	-	-	-	0.00
127	Tank 96	-	-	-	-	0.00
137	Tank 152	-	-	-	-	4.83
138	Tank 153	-	-	-	-	0.00
140	Tank 155	-	-	-	-	0.00
142	Tank 157	-	-	-	-	0.00
300	Tank 158 (Source ID 193)	-	-	-	-	0.00
143	Tank 159	-	-	-	-	0.00
194	Tank 160	-	-	-	-	0.00
144	Tank 161	-	-	-	-	0.00
145	Tank 162	-	-	-	-	0.00
146	Tank 163		-	-	-	0.00
147 148	Tank 164 Tank 165	-	-	-	-	0.00
149		<u> </u>				
150	Tank 166 Tank 168		-	-	-	0.00 2.65
150	Tank 108					0.00
155	Tank 170  Tank 174	-	-	-	<u>-</u>	0.00
156	Tank 174  Tank 175	<u> </u>	-	-		0.00
157	Tank 173					0.00
160	Tank 181		<u> </u>			0.00
161	Tank 182		_	_	_	0.00
163	Tank 185	_	_	_	_	0.00
164	Tank 186	-	_	_	_	0.00
N/A	New Feed Heaters	3.15	4.42	22.04	22.04	3.15
N/A	New Cooling Tower	0.16	-	-	-	6.02
N/A	Additional Fugitive Emissions	-	-	-	-	5.13
	Project Emissions Increases	4.14	17.65	33.57	33.57	22.38
	SR Significance Threshold	10	40	40	25	25
	NNSR Significant?	No	No	No	Yes	No

# Table C-36 Monroe Energy, LLC - Trainer, PA Refinery Contemporaneous Emission Increases/Decreases

	Plan Approval/			Emission Incr	ease/Decrease
Date <sup>(a)</sup>	RFD	Description	Note	NO <sub>x</sub>	voc
	KFD			(t <sub>l</sub>	py)
10/03/2006	23-0003I	Two New Boilers		23.70	2.60
05/04/2007	23-0003J	Clean Fuel Project	(b)	39.00	0.00
10/19/2007	23-0003K	Modification to PA 23-0003G		21.89	0.00
10/23/2008	23-0003M	Cooling Tower		0.00	0.74
12/08/2008	23-0003N	FCCU Feed Heater Modification		0.00	(1.10)
02/09/2009	23-0003O	ReVAP	(c)		
04/10/2009	23-0003P	2010 Turnaround		1.59	0.26
09/28/2009	23-0003Q	Boiler MACT Phase II Application		0.00	0.00
12/04/2009	RFD	Light Components Loading		0.07	0.14
12/23/2009	23-0003R	Aromatic Saturation Unit Project	(c)		
10/01/2010	23-0003S	Flare Gas Recovery Project		0.00	3.58
10/01/2010	23-0003T	Amended Alky ReVAP Project	(c)		
11/09/2011	23-0003U	Two New Boilers (Replace Boiler 8)(withdrawn)			
04/12/2012	23-0003V	Diesel Heater Project	(c)		
08/09/2012	RFD	Main Flare - Turnaround		0.00	0.09
01/10/2013	RFD #3418	Propane Loading into Trucks		0.00	0.00
04/04/2013	RFD #3561	Peabody Heater Modifications		0.00	0.00
04/23/2013	RFD #3596	Max Jet		0.00	0.21
05/17/2013	23-0003W	D2 Project	(d)	0.00	3.44
03/13/2014	23-0003X	400 kW Emergency Generator	(e)	1.19	0.01
10/14/2014	23-0003Y	Proposed Boiler 13 (Replace Boiler 8)		11.70	1.98
Tota	l Contemporaneous Emi	ssion Increases with Proposed Boiler 13		117.14	0.00
Т	otal Contemporaneous E	Emission Reduction Credits Required	(f)	152.28	0.00
Total E	Emission Reduction Cred	its Previously Provided with PA 23-0003X	(g)	(146.20)	N/A
Net E	mission Reduction Cred	its Required/Provided with PA 23-0003Y	(h)	6.08	0.00
TBD	23-0003Z	Proposed Cooling Tower Project	(i)	1.44	67.38
TBD	TBD	Proposed Flare PAA		1.60	0.09
TBD	TBD	Proposed ULSG PAA		33.57	22.38
		5-	year Aggregation	36.62	22.47
		10-	year Aggregation	36.62	22.47
		S	ignificance Level	25	25
		Total Emission Reduction Ci	redits Required (f)	48	N/A

#### Notes

<sup>&</sup>lt;sup>(a)</sup> Based on net emission increases occurring over a 10-year period.

<sup>(</sup>b) This application modified an existing Plan Approval No. 23-0003E.

<sup>(</sup>c) Application/Plan Approval was withdrawn.

<sup>(</sup>d) Project triggered NNSR for VOC, 40 tons of VOC ERCs were purchased, cumulative contemporaneous emissions increase reset back to zero.

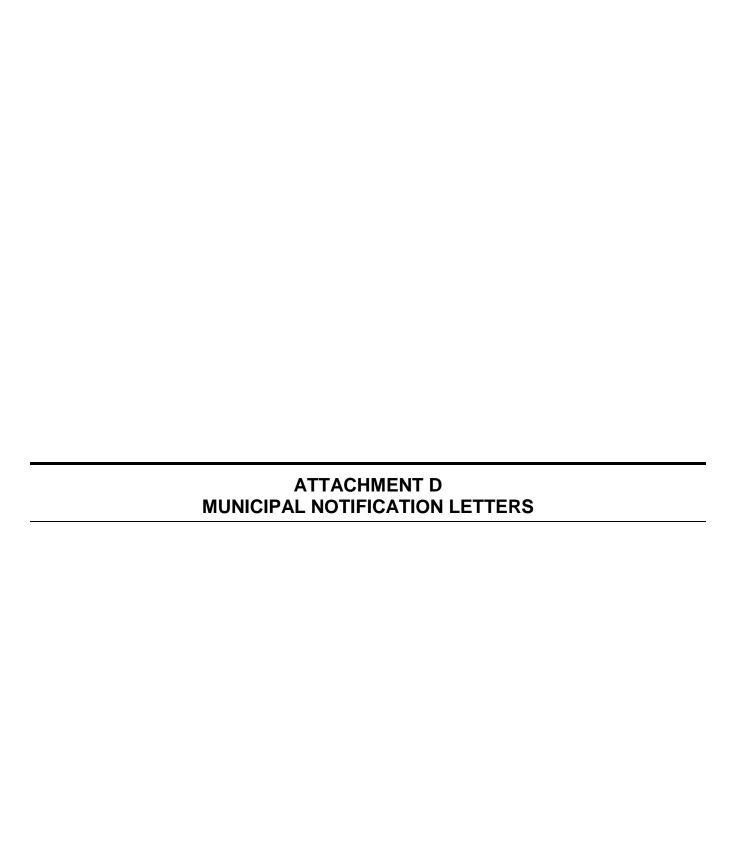
 $<sup>^{(</sup>e)}$  Project triggered NNSR for NO<sub>X</sub>, 147.6 tons of NO<sub>X</sub> ERCs were purchased, cumulative contemporaneous emissions increase reset back to zero with an additional 1.4 tons available for future use.

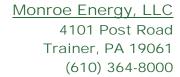
<sup>(</sup>f) At an offset ratio of 1.3:1 per 25 Pa. Code § 127.210.

<sup>(</sup>g) Application/Plan Approval 23-0003U was withdrawn and desired back-up capacity now being replaced with proposed Boiler 13. Aggregate NO<sub>X</sub> ERCs required is reduced accordingly for those already provided under PA 23-0003X, per conversations with Virendra Trivedi (PADEP) on July 10, 2014.

<sup>(</sup>h) Project triggered NNSR for NO<sub>x</sub>, 6.08 tons of NO<sub>x</sub> ERCs were purchased, cumulative contemporaneous emission increase reset back to zero.

<sup>(</sup>i) Project triggered NNSR for VOC, 69.39 tons of VOC ERCs were purchased, cumulative contemporaneous emission increase reset back to zero.







September 1, 2015

#### CERTIFIED MAIL 7009 2820 0002 5399 2534

Principal Planner
Delaware County Planning Department
Court House/Government Center
201 W. Front Street
Media, PA 19063

RE: PADEP Required County Notification – Plan Approval Application

Dear Sir or Madam:

Pursuant to the Commonwealth of Pennsylvania's Administrative Code (Section 1905-A), Cooperation with Municipalities, which became effective April 17, 1984, Monroe Energy, LLC (Monroe) hereby notifies Delaware County of its submittal of a Plan Approval Application to Construct, Modify, or Reactivate an Air Contamination Source and/or Air Cleaning Device to the Pennsylvania Department of Environmental Protection (PADEP). Monroe operates a petroleum refinery located in Trainer, Pennsylvania (Trainer Refinery), and is submitting a Plan Approval Application for the installation of new sources needed to meet gasoline sulfur level requirements of the U.S. Environmental Protection Agency (U.S. EPA) Tier 3 Motor Vehicle Emission and Fuel Standards rule.

PADEP will accept comments on the Plan Approval Application during a 30-day period which begins upon your receipt of this notification. A copy of the Plan Approval Application is available for your review at PADEP's Southeast Regional Office in Norristown, Pennsylvania. Any comments concerning the application should be transmitted to PADEP within 30 days of your receipt of this letter. If you have any questions or concerns regarding the above information, please contact me at 610-364-8528 or david.chetkowski@monroe-energy.com.

Sincerely,

MONROE ENERGY, LLC

David M. Chetkowski, P.E.

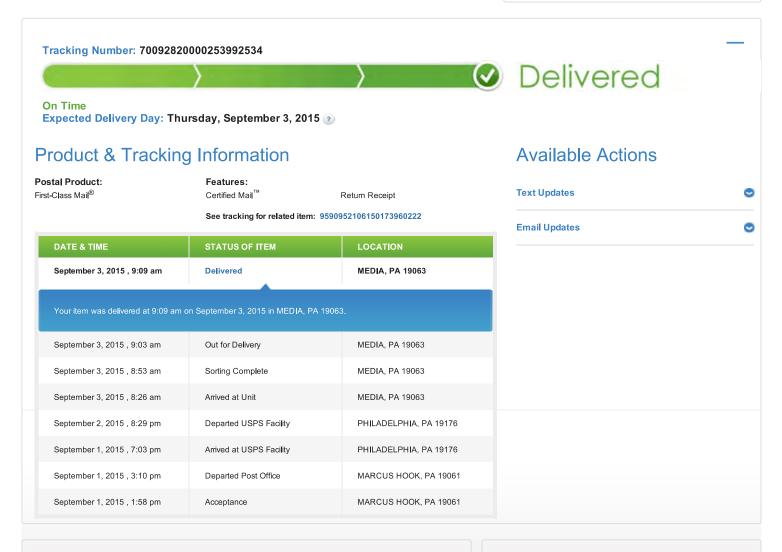
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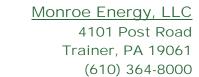
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September 1, 2015

#### CERTIFIED MAIL 7009 2820 0002 5399 2527

VP Council and Public Safety Trainer Borough 824 Main Street Trainer, PA 19061

RE: PADEP Required Borough Notification – Plan Approval Application

Dear Sir or Madam:

Pursuant to the Commonwealth of Pennsylvania's Administrative Code (Section 1905-A), Cooperation with Municipalities, which became effective April 17, 1984, Monroe Energy, LLC (Monroe) hereby notifies Trainer Borough of its submittal of a Plan Approval Application to Construct, Modify, or Reactivate an Air Contamination Source and/or Air Cleaning Device to the Pennsylvania Department of Environmental Protection (PADEP). Monroe operates a petroleum refinery located in Trainer, Pennsylvania (Trainer Refinery), and is submitting a Plan Approval Application for the installation of new sources needed to meet gasoline sulfur level requirements of the U.S. Environmental Protection Agency (U.S. EPA) Tier 3 Motor Vehicle Emission and Fuel Standards rule.

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Sincerely,

Monroe Energy, LLC

David M. Chetkowski, P.E.

Air Program Lead



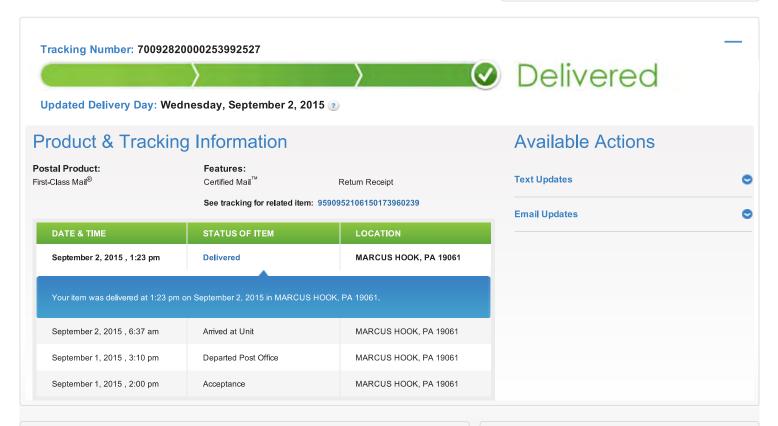




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### ATTACHMENT E ALL4 INC. QUALITY SEAL



Den Dine

Digitally signed by Kevin J. Hickey DN: cn=Kevin J. Hickey, o=All4 Inc., ou, email=khickey@all4inc.com, c=US Date: 2015.09.11 19:28:25 -04'00'